

3D modeling and measurement of coupling AC loss in soldered tapes and striated coated conductors

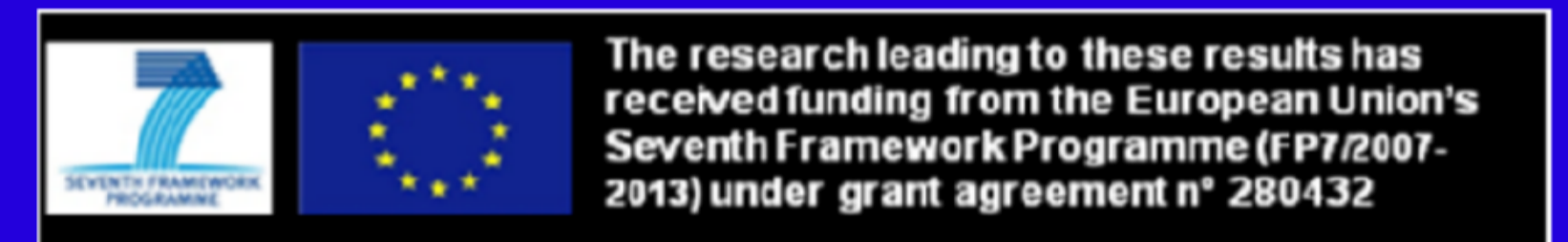
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3A-LS-O1.8

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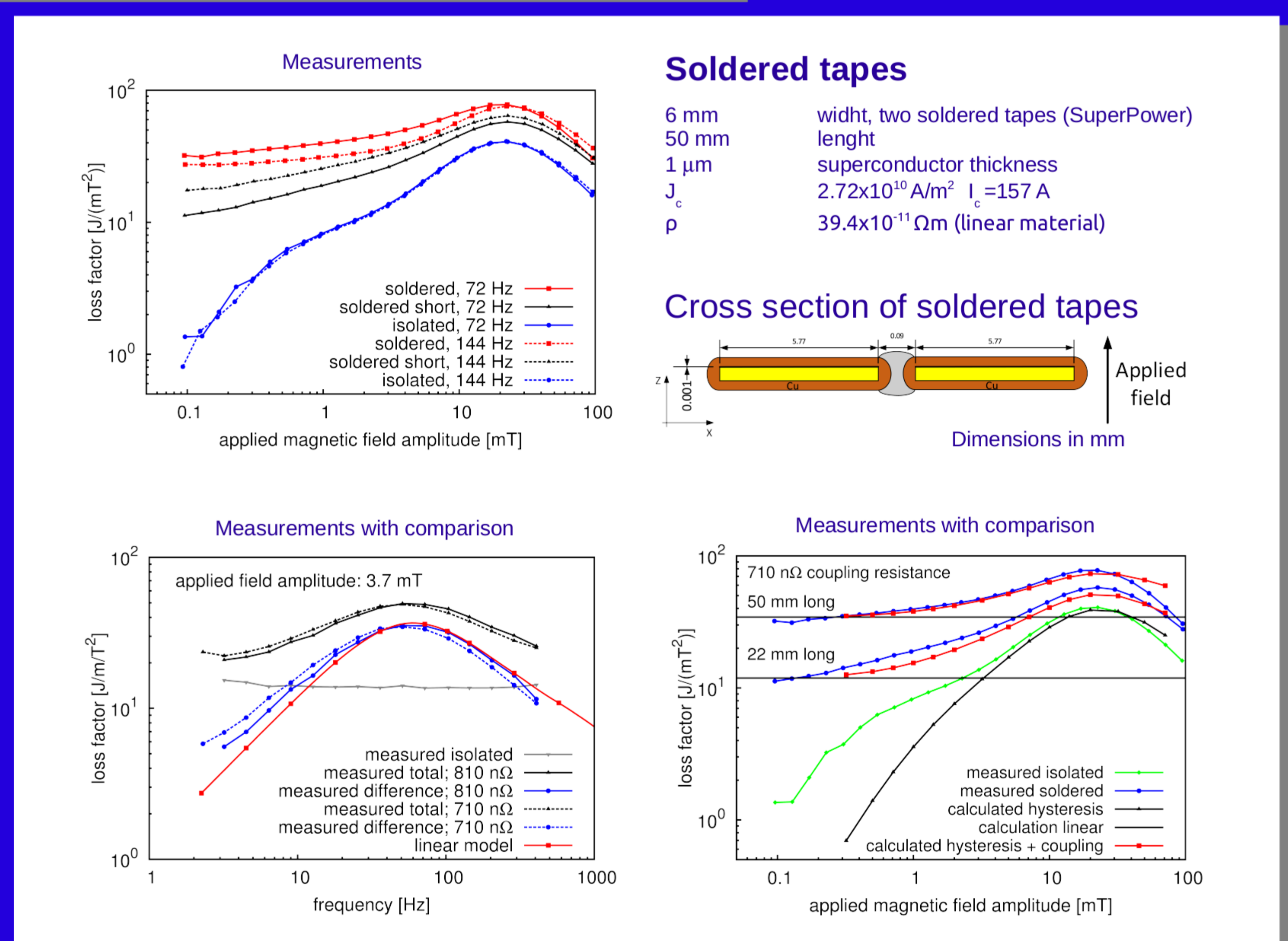
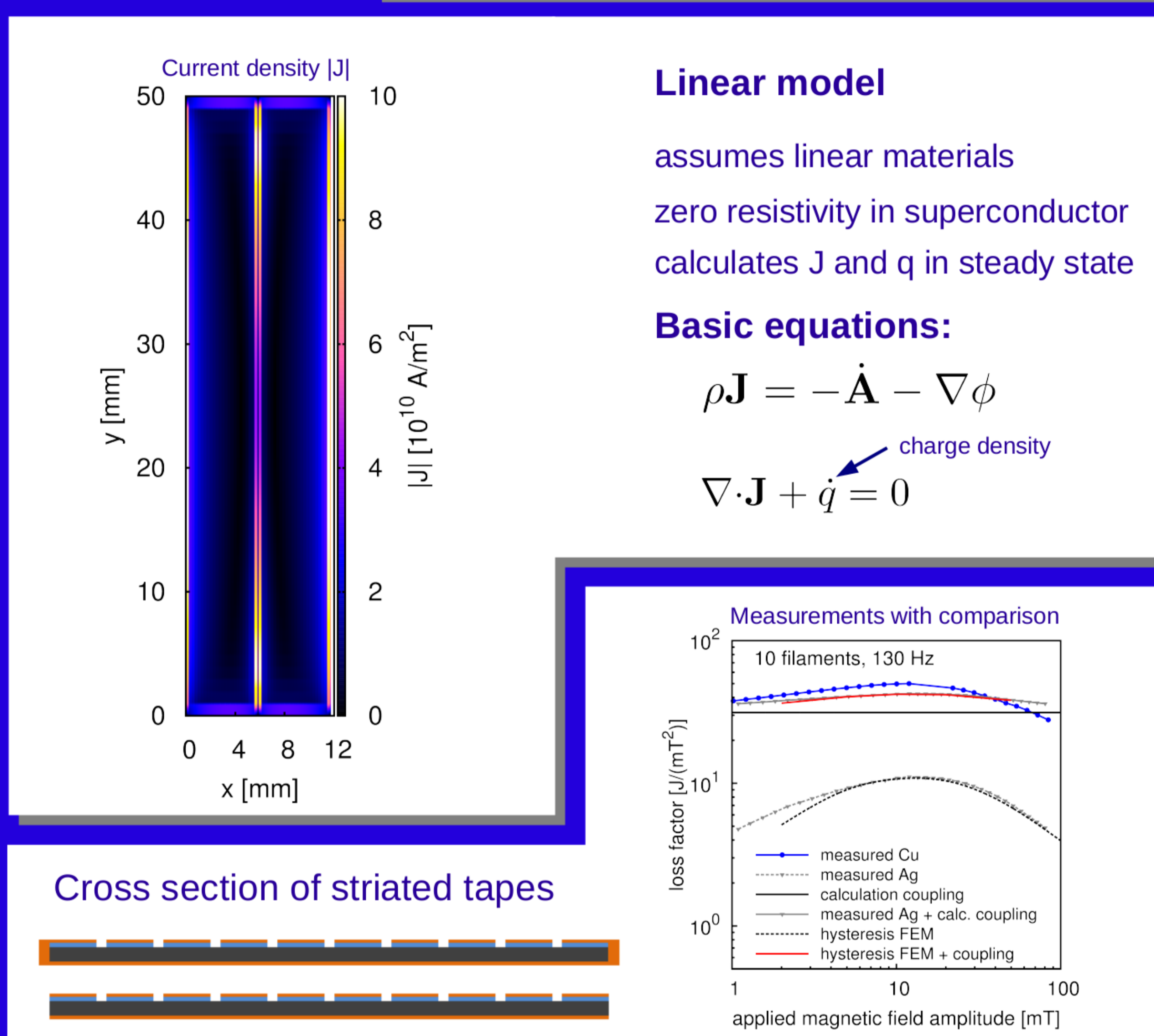
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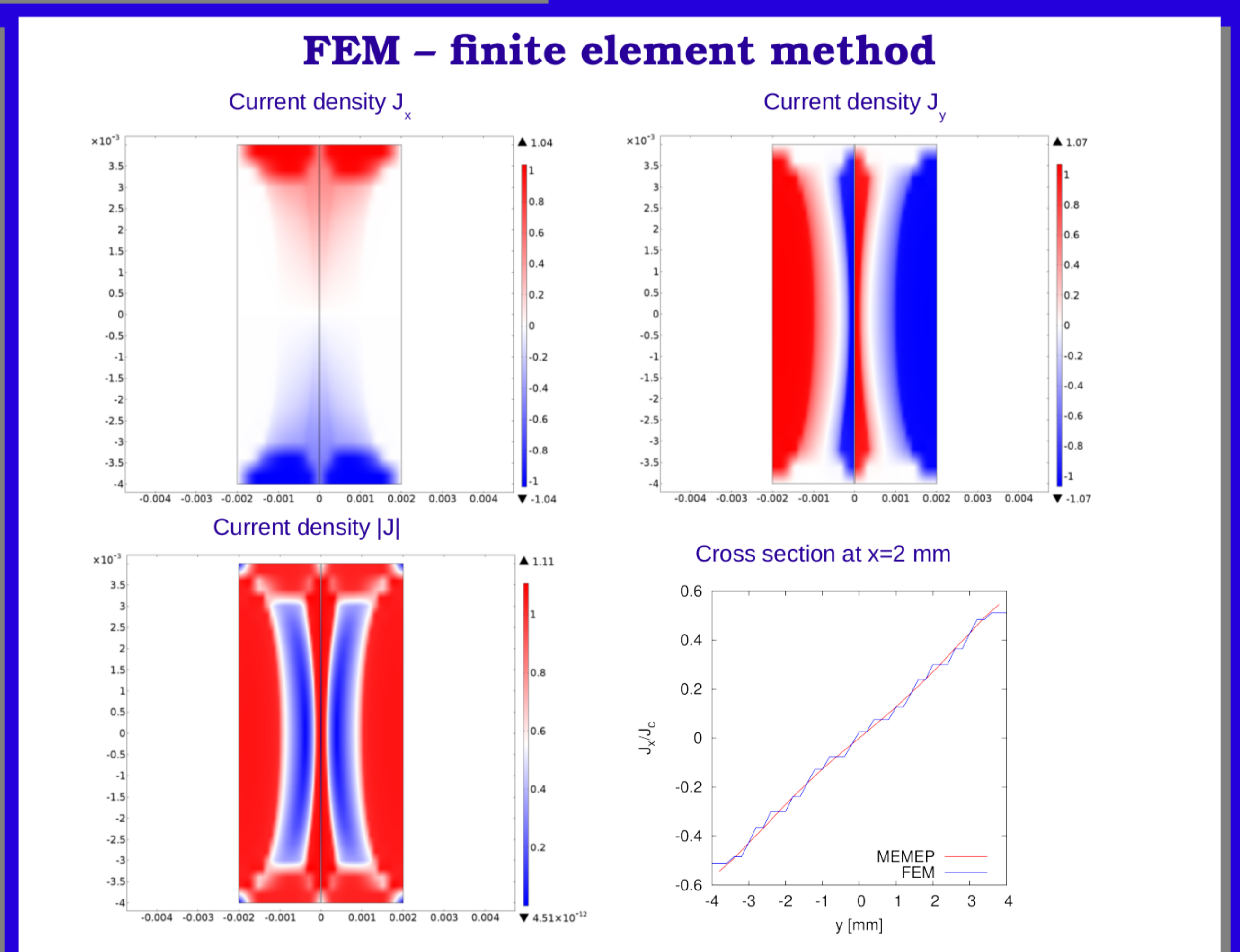
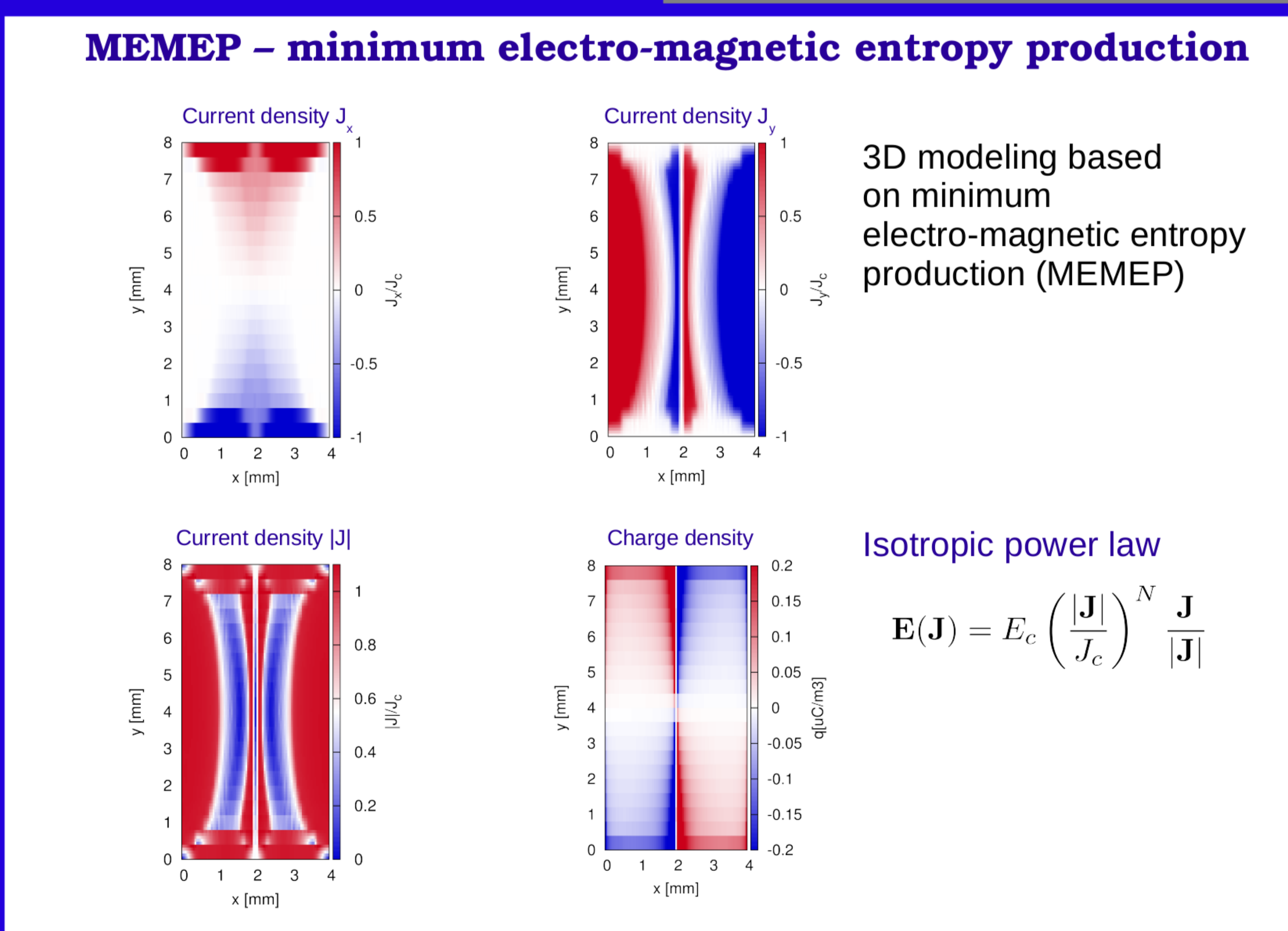
Introduction

Coated conductors experience high AC loss
 Striation reduces hysteresis loss
 There appear coupling loss

Measurements of AC loss in striated and soldered tapes



Comparison of two calculation methods



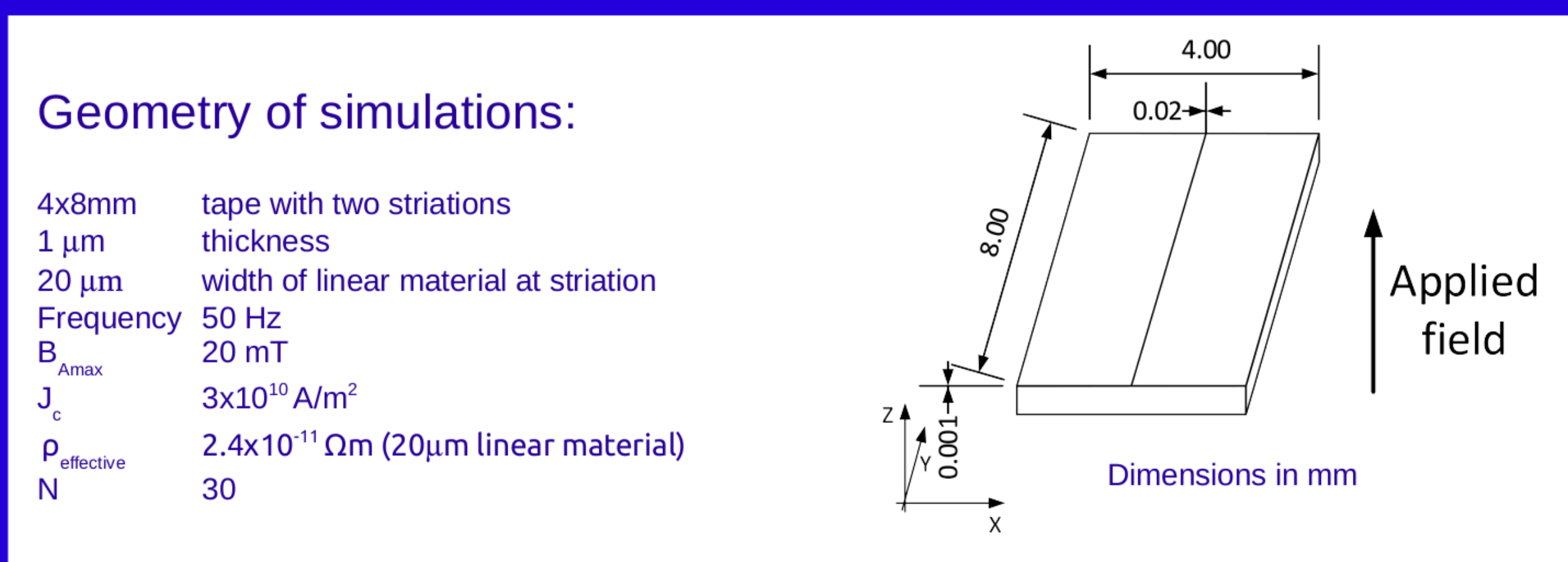
CONCLUSION

Model for linear materials agrees with measurements at low amplitudes

At low frequencies (few Hz) soldered tapes present low coupling losses: important for magnets

MEMEP simulations agree with FEM

MEMEP requires further development for long samples



3D electromagnetic modeling of practical superconductors for power applications

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Introduction

Current has 3D behavior
Computation volume restricted to superconductor volume

3D formulation

Vector and scalar potential

Coulomb's gauge $\nabla \cdot \mathbf{A} = 0$

$$\mathbf{E} = -\dot{\mathbf{A}} - \nabla\phi$$

charge density \uparrow

$$\nabla \cdot \mathbf{E} = \frac{q}{\epsilon_0}$$

$$\Phi(\mathbf{r}) = \frac{1}{4\pi\epsilon_0} \int_{V'} \frac{q(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} dV'$$

\uparrow $\mathbf{A}_s(\mathbf{r})$

$$\nabla \times \mathbf{B} = \mu_0 \mathbf{J} + \frac{\dot{\mathbf{E}}}{c^2}$$

$$\mathbf{A}(\mathbf{r}) = \frac{\mu_0}{4\pi} \int_{V'} \frac{\mathbf{J}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} dV' + \frac{1}{4\pi c^2} \int_{V'} \frac{\dot{\mathbf{E}}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} dV'$$

Low frequencies: Neglect terms with second derivatives of E and B (no electromagnetic radiation)

$$(1) \quad \mathbf{E} = -\dot{\mathbf{A}} - \nabla\phi \approx -\dot{\mathbf{A}}_S - \nabla\phi$$

$$\mathbf{B} = \nabla \times \mathbf{A} \approx \nabla \times \mathbf{A}_S$$

Continuity equation \uparrow

$$(2) \quad 0 = \nabla \cdot \mathbf{A} = \nabla \cdot \mathbf{A}_S + \frac{\dot{\phi}}{c^2} \Leftrightarrow \nabla \cdot \mathbf{J} + \dot{q} = 0$$

For given E(J) relation, solving equations (1) and (2) same as minimizing (3) and (4)

\uparrow \mathbf{A}_s due to $\Delta \mathbf{J}$ \uparrow change in applied vector potential \uparrow $\mathbf{J} = (\mathbf{J}_0 + \Delta \mathbf{J})$ \uparrow \mathbf{J}_0 : \mathbf{J} at the beginning of time step

$$(3) \quad \mathbf{L}_J = \int_V \left(\frac{1}{2} \Delta \mathbf{J} \cdot \frac{\Delta \mathbf{A}_{SJ}}{\Delta t} + \Delta \mathbf{J} \cdot \frac{\Delta \mathbf{A}_a}{\Delta t} + U(\mathbf{J}) + \nabla\phi \cdot \Delta \mathbf{J} \right) dV$$

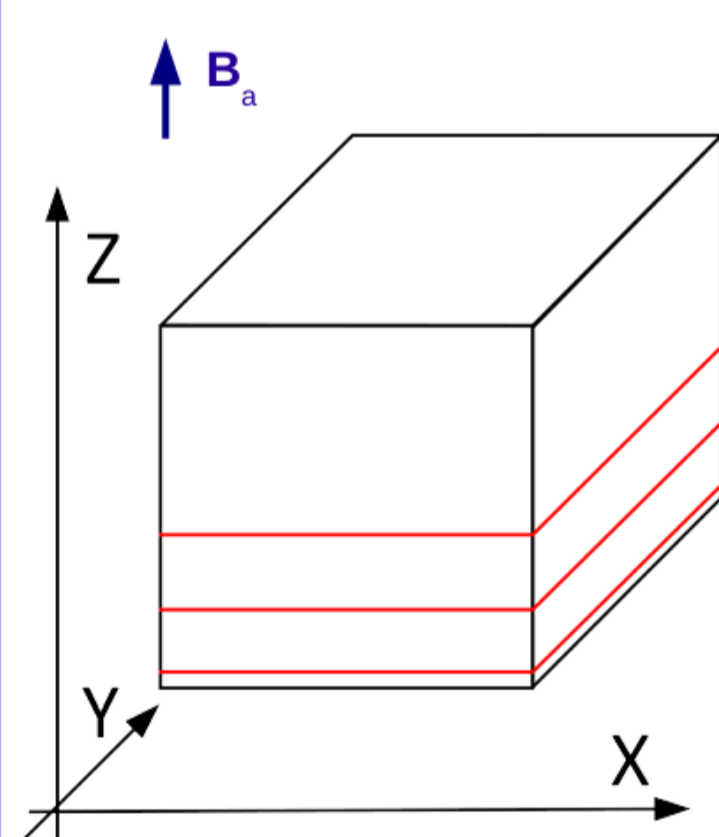
\downarrow $\Delta \mathbf{J}$ change in \mathbf{J} in 1 time step \downarrow $U(\mathbf{J}) = \int_0^{\mathbf{J}} \mathbf{E}(\mathbf{J}') \cdot d\mathbf{J}'$

\downarrow change in q in 1 time step \downarrow $\phi = (\phi_0 + \Delta\phi)$ \downarrow ϕ_0 : ϕ at the beginning of time step

$$(4) \quad \mathbf{L}_q = \int_V \left(\frac{1}{2\Delta t} \Delta q \cdot \Delta\phi - \nabla\phi \cdot (\mathbf{J}_0 + \Delta \mathbf{J}) \right) dV$$

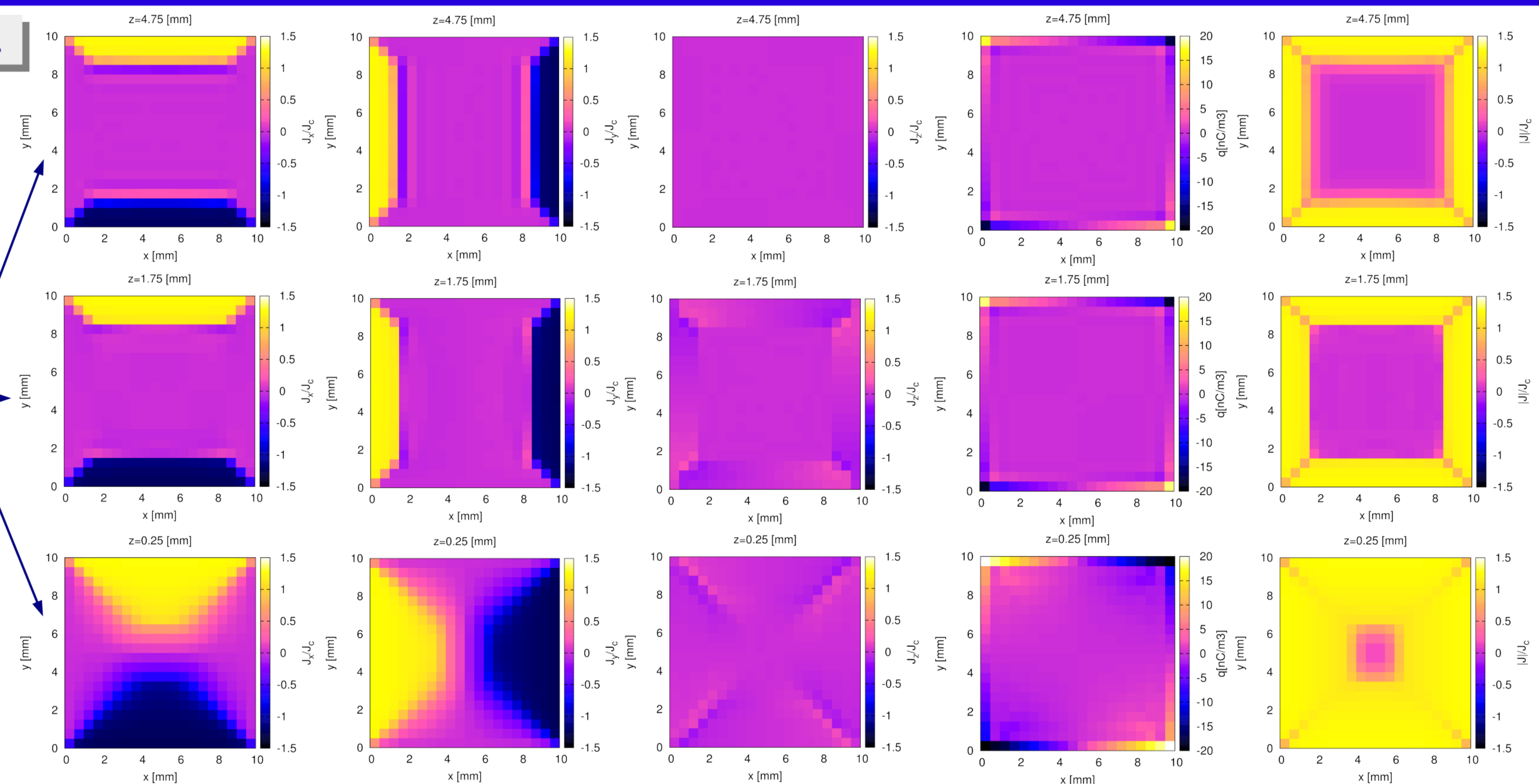
3D solution

10x10x10 mm
Frequency 50 Hz
 B_a 161 mT
 J_c 10^9 A/m²
N 30



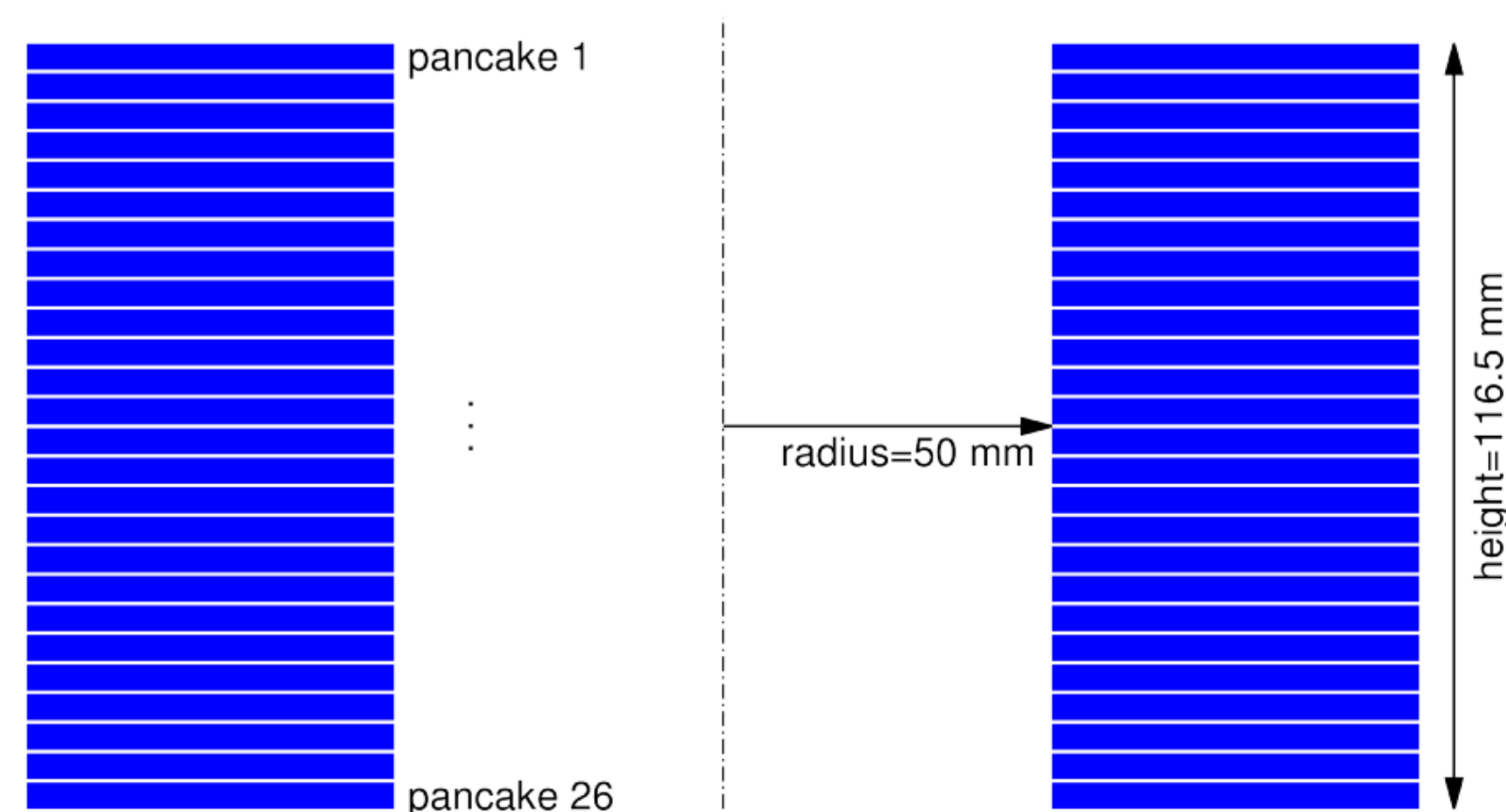
Isotropic power law

$$\mathbf{E}(\mathbf{J}) = E_c \left(\frac{|\mathbf{J}|}{J_c} \right)^N \frac{\mathbf{J}}{|\mathbf{J}|}$$



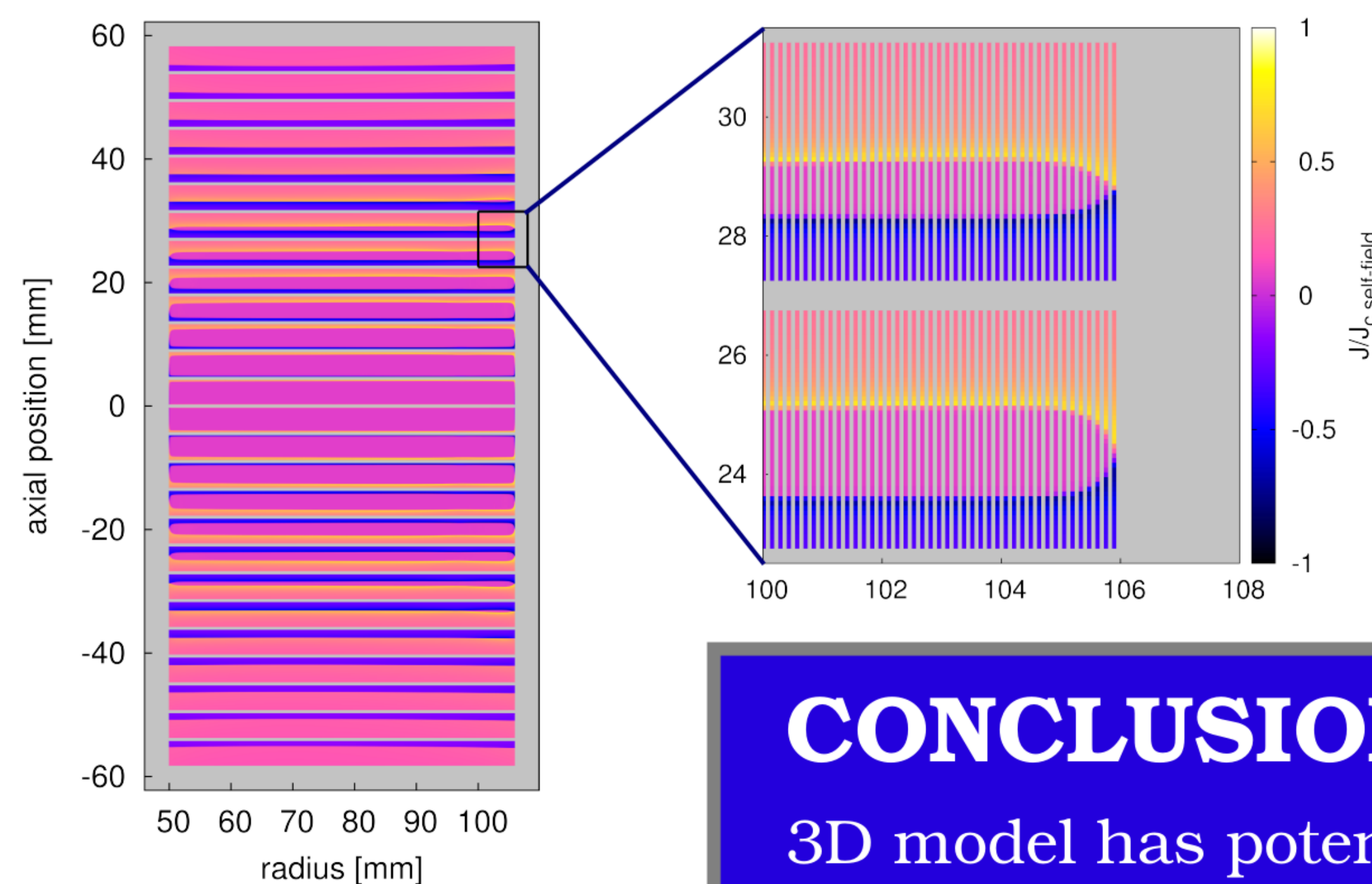
2D solution for coils

More than 10000 turns
Cross section of coil

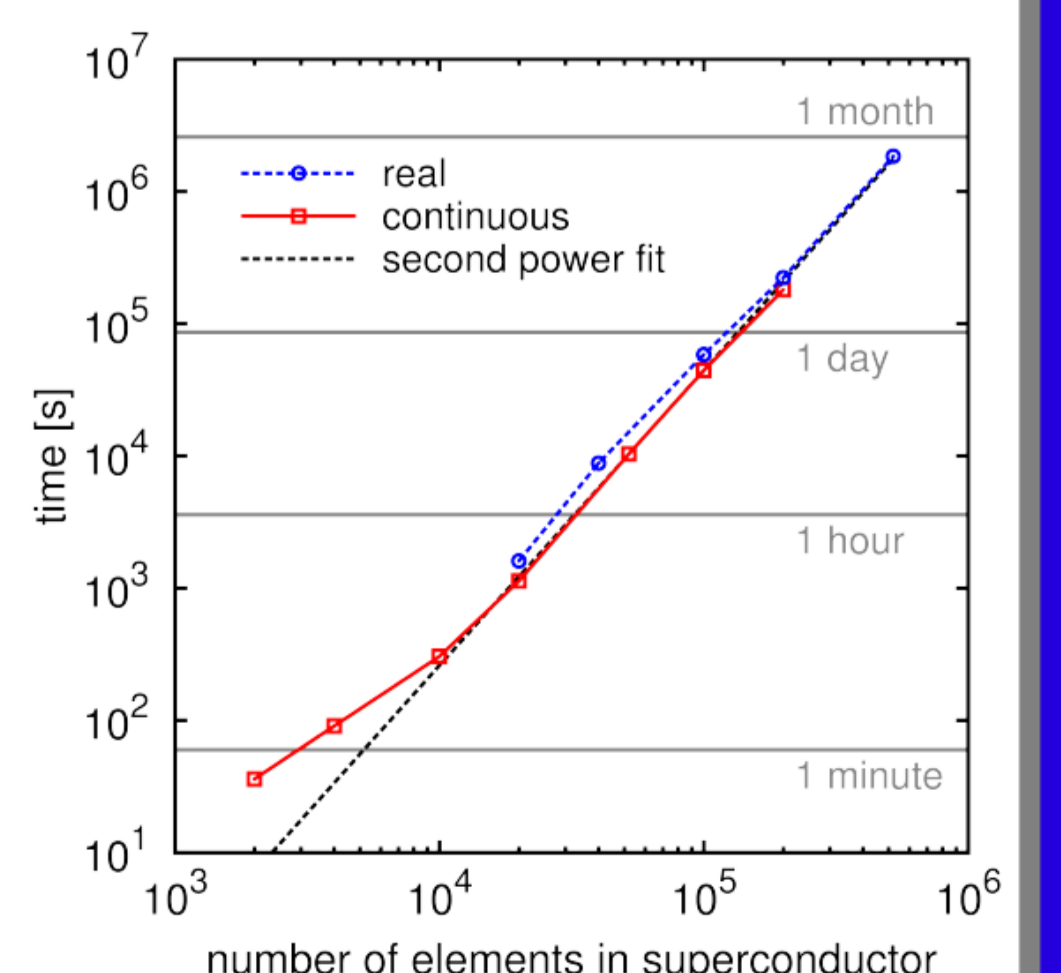


Up to 40000 turns with continuous approximation

Detailed modeling



Calculation time



CONCLUSION

3D model has potential for fast calculations