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2021 Virtual Coated Conductors for Applications
(Virtual CCA 2021)
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Robust REBCO Coil Structure for High Field Cryogen-free Superconducting Magnet

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High Field Magnet Development at HFLSM - Load map -

2015

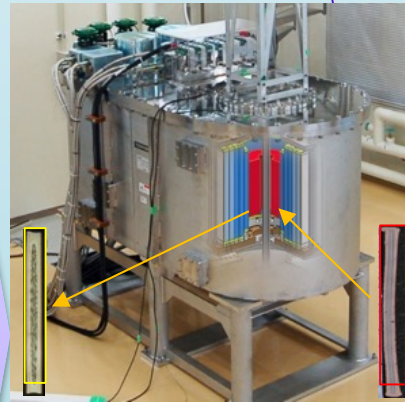
25 T cryogen-free
Superconducting Magnet
(25T-CSM)



- 24.6 T in a 52 mm RT bore with 1 hour ramping
- Advanced high strength Nb₃Sn technologies and high strength Bi2223 (Type HT-Nx (SEI))
- World highest field in CSM
- Open for users since 2016 (250 days operation in 2018)
- 25.1 T achieved in 2020
- Long time, high precision experiments
- J_c - B - T - θ of HTS, transport, NMR, high pressure, etc.

2018-2022

Upgrade to
30T-CSM
(JSPS project)



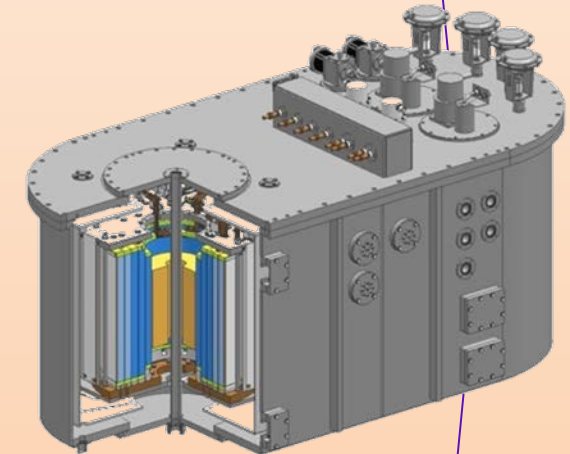
- Replace from Bi2223 insert to REBCO one.
- R&D toward to 33T

S. Awaji IEEE TAS
31 (2021) 4300105

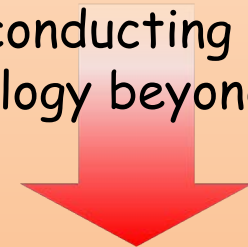
2022-

NEW 33T-CSM

- High strength Nb₃Sn
- REBCO conductors
- Adv. HTS coil technol.



Superconducting magnet
technology beyond 40 T



50T Superconducting magnet

Under "High Magnetic Field Collaboratory Japan" project



Summary and issues of commercial REBCO CC tapes

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- ✓ **Excellent in-field J_c and electromechanical properties.**
 - ✓ Stress tolerance decreases with decreasing volume fraction of Hastelloy
- ✓ APC is effective to improve in-field J_c properties.
 - ✓ Angular dependence of J_c is not complicated below 20 K even for REBCO with APC.

Issues

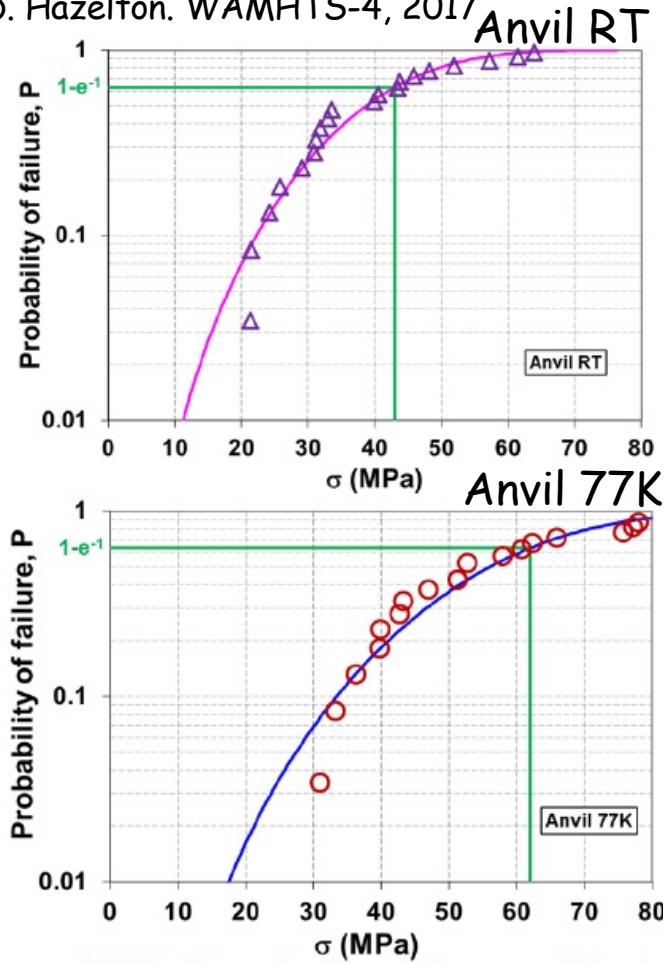
- ✓ **Delamination** and the local degradation.
 - ✓ Current share is a key to overcome the hotspot.
- ✓ **Screening current induced field and stress**
- ✓ **Piece length**: typically 100m, 2-300m (high cost), Is 1km possible?,
- ✓ **Cost**: \approx \$50/m (4mm-width), Need less than \$10/m?
- ✓ **Protection** from the hot-spot is critical.
 - ✓ No-insulation (self-protection) \rightarrow delay of magnetic field and heating are issues.
 - ✓ Quench heater (Active protection) \rightarrow need huge power in quench heater with short time.
 - ✓ Dump resistor (Passive protection) \rightarrow need detection and quick dump before burn-out



Issues of REBCO coated conductors for high field magnets

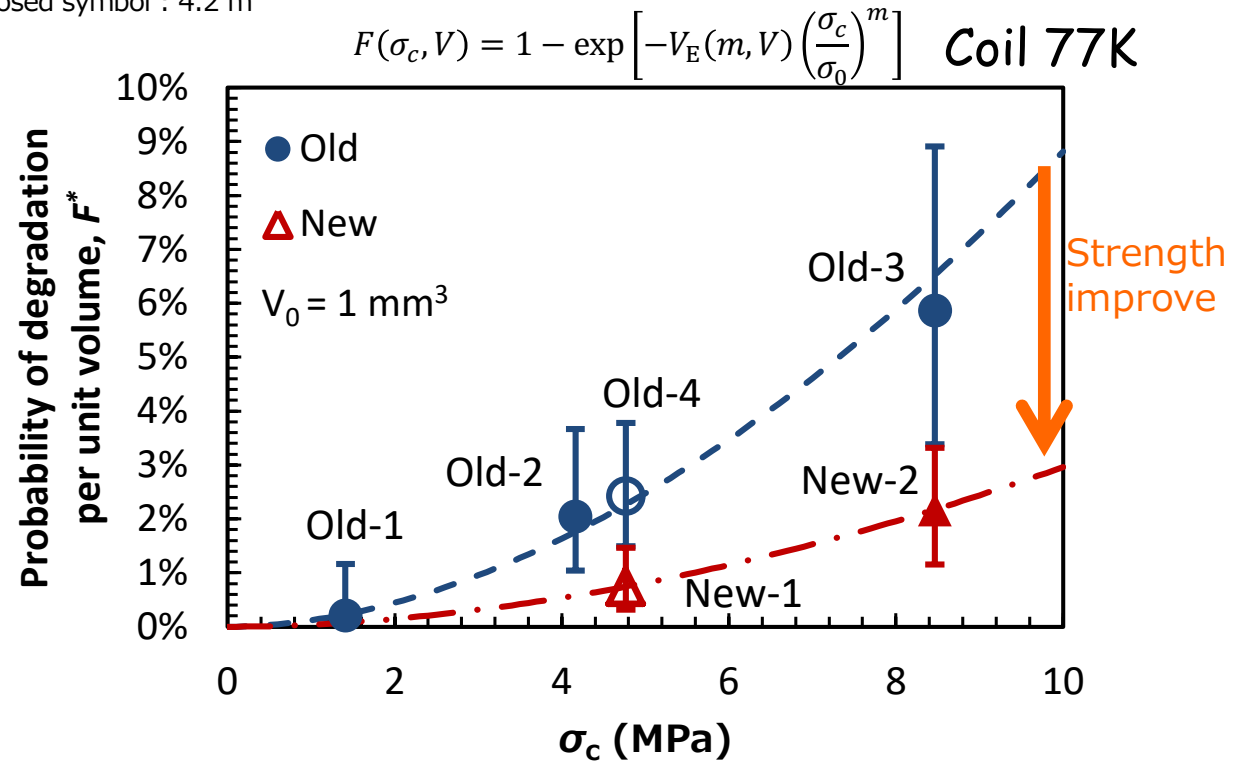
✓ Delamination and local degradation

D. Hazelton. WAMHTS-4, 2017



Open symbol : 2.6 m
 Closed symbol : 4.2 m

Muto et al., IEEE TAS 28 (2018) 6601004.

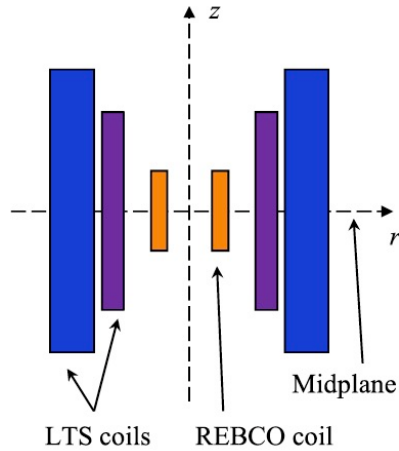


σ_c is estimated for R/in/Rout ratio.

It may be impossible to avoid the local degradation statistically, although its possibility can be reduced so much.



Issues of REBCO coated conductors for high field magnets



REBCO insert for 32T-SM
 $(B_{LTS}=15T, B_{HTS}=10.7T)$

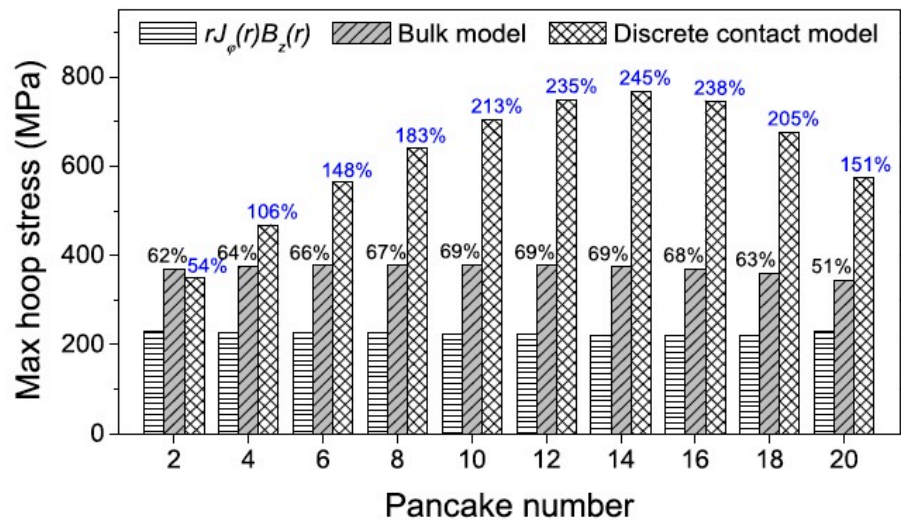
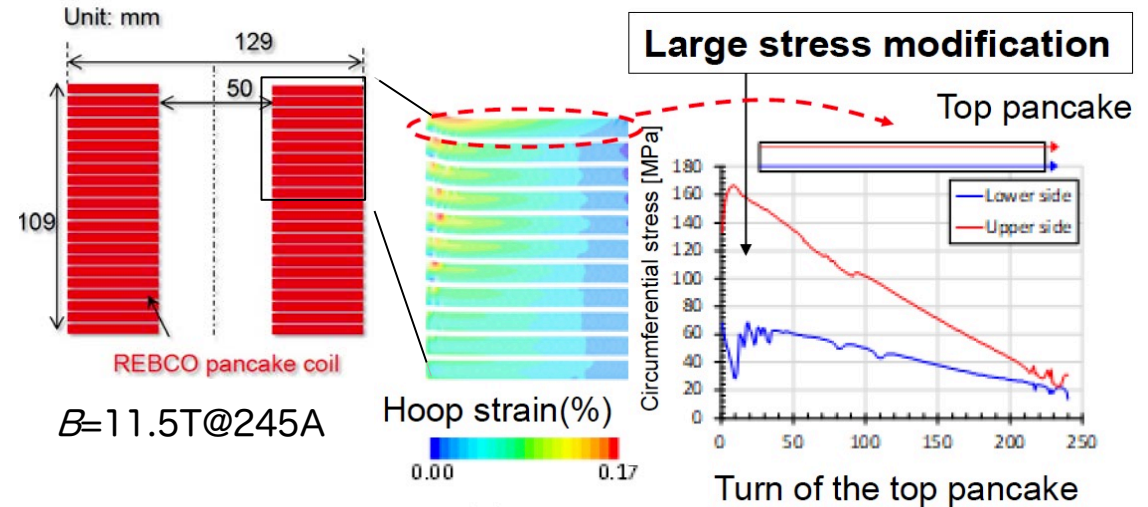
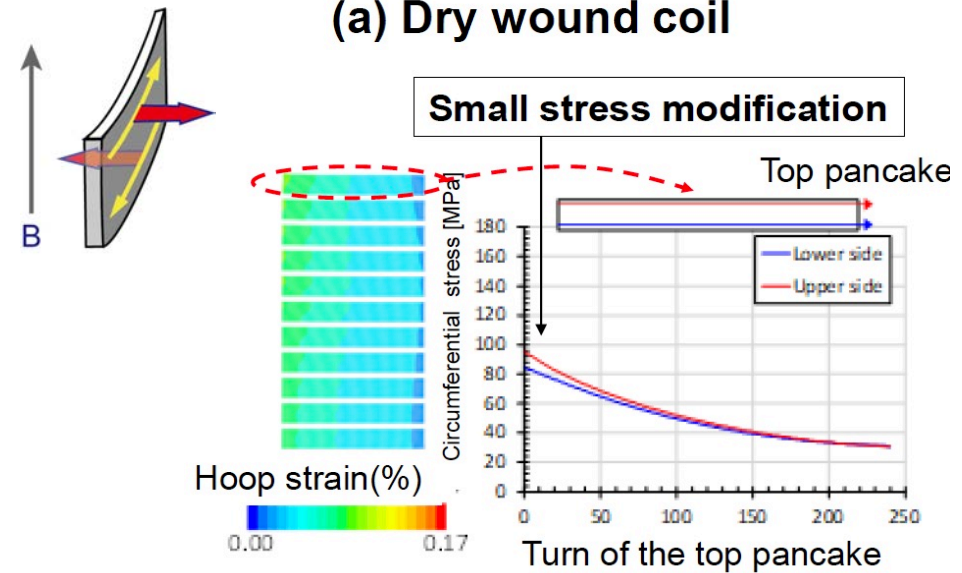


Figure 15. Maximum local hoop stresses in pancakes based on the classic formula (without SC), bulk model (with SC) and discrete contact model (with SC), respectively.

Xia et al, SuST, 32 (2019) 095005



(a) Dry wound coil



(b) Epoxy impregnated coil

H. Maeda, ASC2020 Wk2Lor2A-2, Ueda et al, to be published.

Impregnation → Improve coil stiffness



Concept of Robust REBCO coil

- Robust against local degradation: Two bundle winding
- Robust against mechanical stress: Edge impregnation

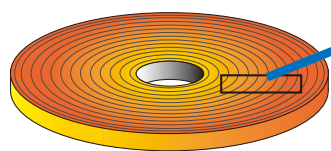
Two tape bundle winding with a face-to-back configuration

Current share at local damaged area.

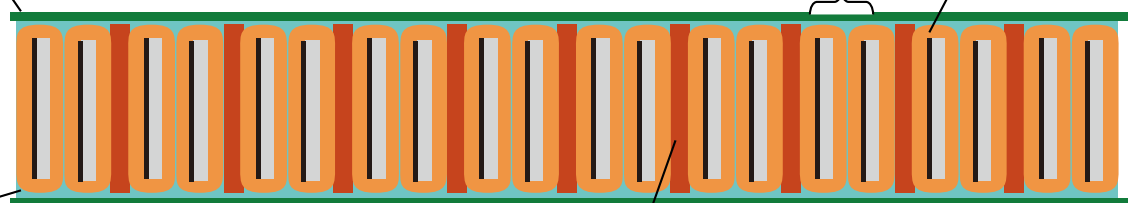
Reduce amount of insulation (Increase J_{space}).

Edge impregnation
Thin FRP plate glued on coil & Impregnation
(Improve coil stiffness)

40 μm Cu stabilizer
(Reduce hot-spot temp.)



Epoxy



REBCO tape
(SC inside)
Polyimide
(F coated)

All turn separation with F-coated polyimide
(Reduce delamination force on REBCO tape)



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Robust against local degradation: Two bundle winding



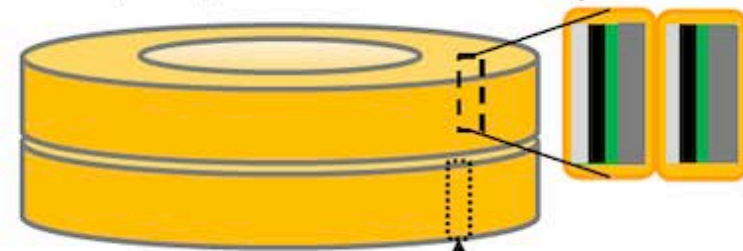


Robust against local degradation: Two bundle insulated double pancake coil with a damaged area

EuBCO tape with BHO

Width	4 mm
full thickness	0.11 mm
REBCO thickness	2.5 μm
Hastelloy [®] thickness	50 μm
Cu thickness	20 μm
I_c (4mm, 77 K, s.f.)	213.5 A

$\phi 40 \times \phi 94$, 101 x 2 turns/pc



Damaged part
 in 55th/101 turn of bottom PC

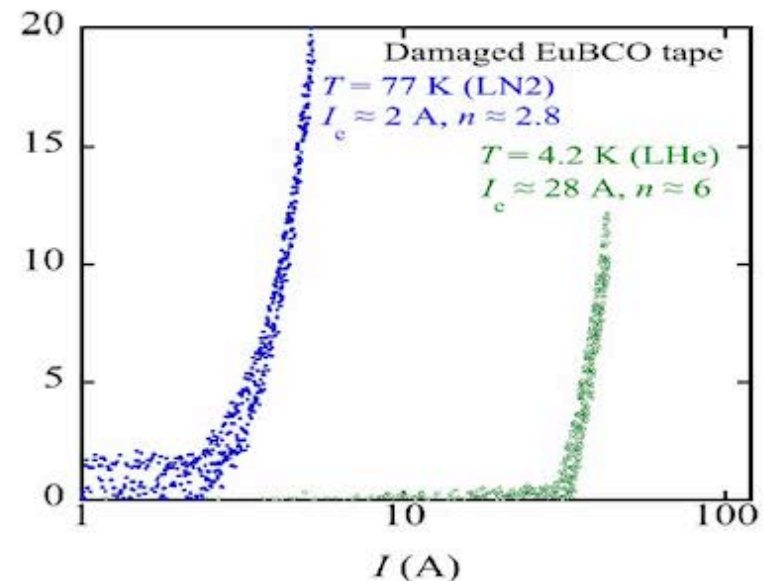
Double pancake coil

tape	EuBCO+BHO
Turn number	101 turn x 2 layer
Inner diameter	40.0 mm
Outer diameter	94.0 mm
Position of damage*	55 turn of bottom coil, outer tape
Coil constant	3.87×10^{-3} T/A

*Damage was introduced by double bending with $\phi 12$ mm bending dia.

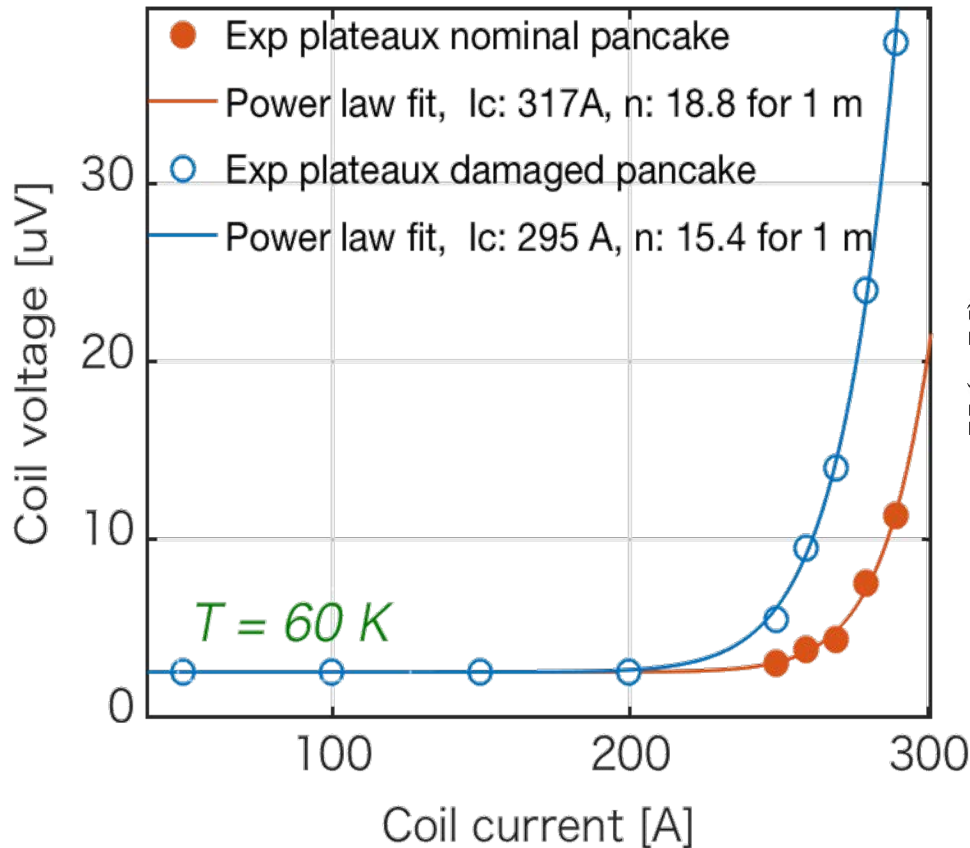


IV property of damaged EuBCO

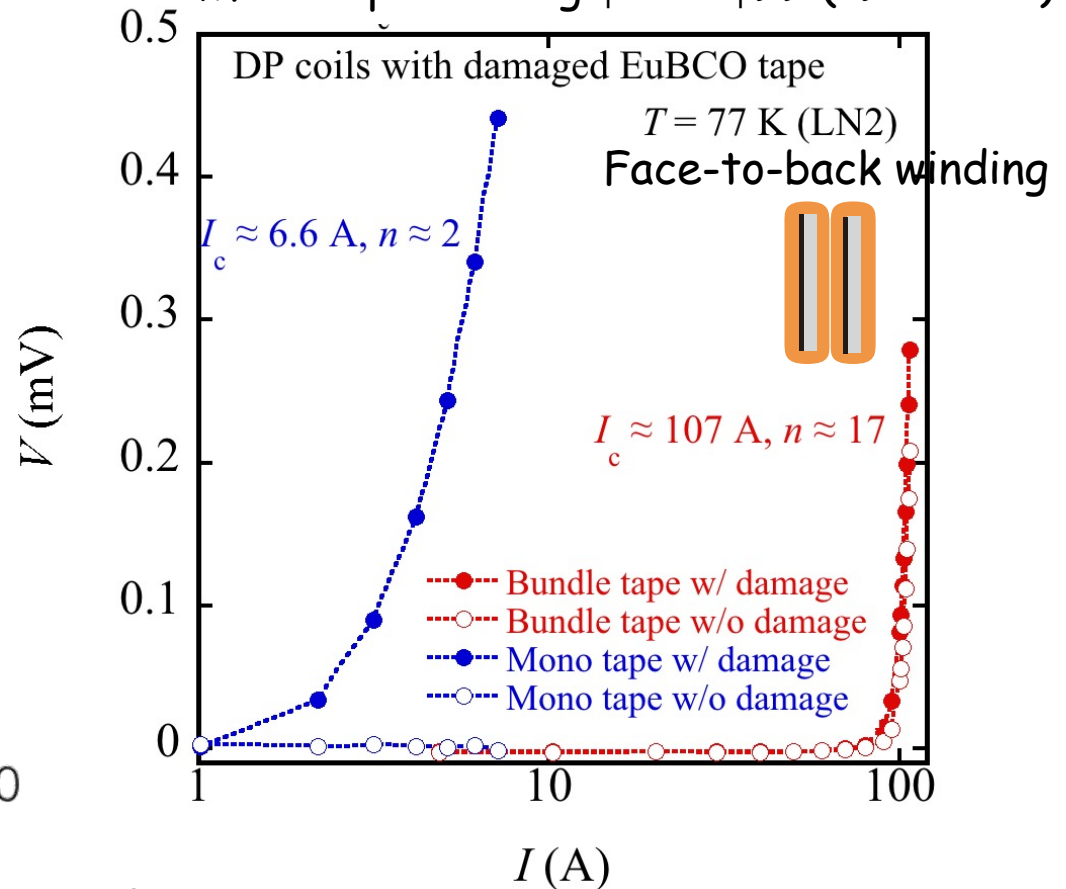




Robust against local degradation: Two bundle insulated double pancake coil with a damaged area



Bundle winding $\phi 40 \times \phi 94$ (101 turns \times 2)
 Mono tape winding $\phi 40 \times \phi 99$ (198 turns)



- Monotape coil with a damage shows low performance.
- Bundle tape coil with damage shows similar performance to that without a damage at 77K and slightly lower with decreasing temperature.
- I_c difference may be related to I_c distribution in the coil.

➔ Bundle winding is effective!



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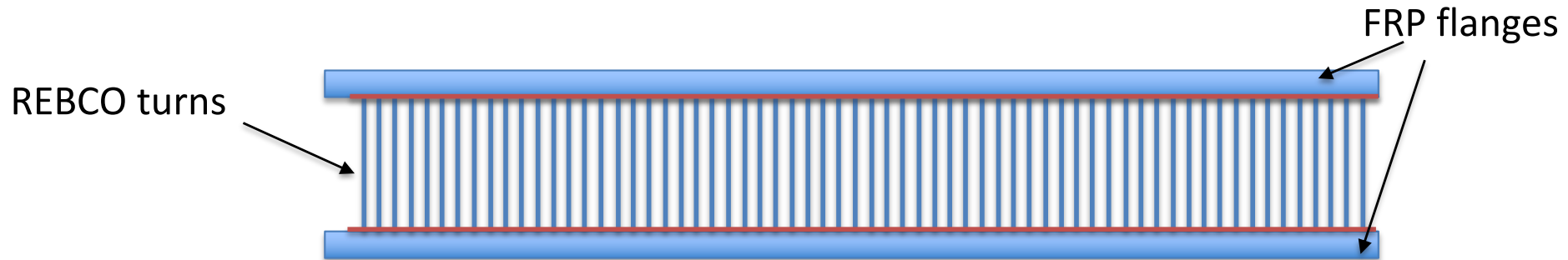
Robust against mechanical stress: Edge impregnation





Robust against mechanical stress: Edge impregnation

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Turns are not glued only to the flanges (in red), not to each other
Radial stiffness is defined by ratio between flange thickness and tape width : can be made very low

⇒ Radial tensile stress only in the flange : no delamination risk

⇒ Hoop stress profile can be adjusted to be more homogenous

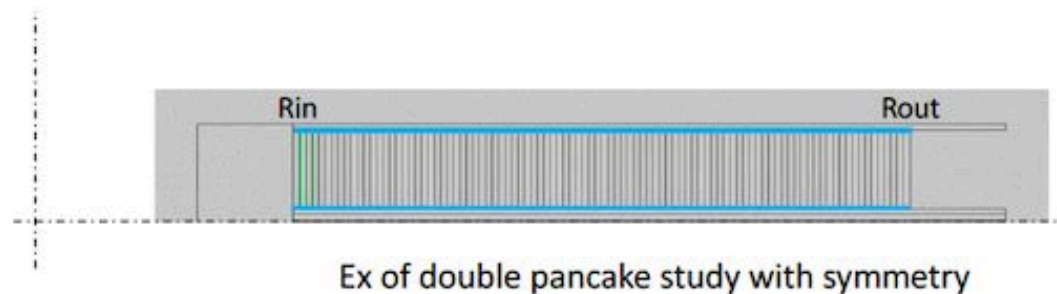
Edge impregnation can be obtained :

- Impregnation + non-stick material for isolation between turns (fluorine-coated polyimide)
- Only gluing the flanges on the pancake after winding



Edge impregnation modelling approach

- 2D axisymmetrical Magnetostatic / Mechanics coupled using Comsol®

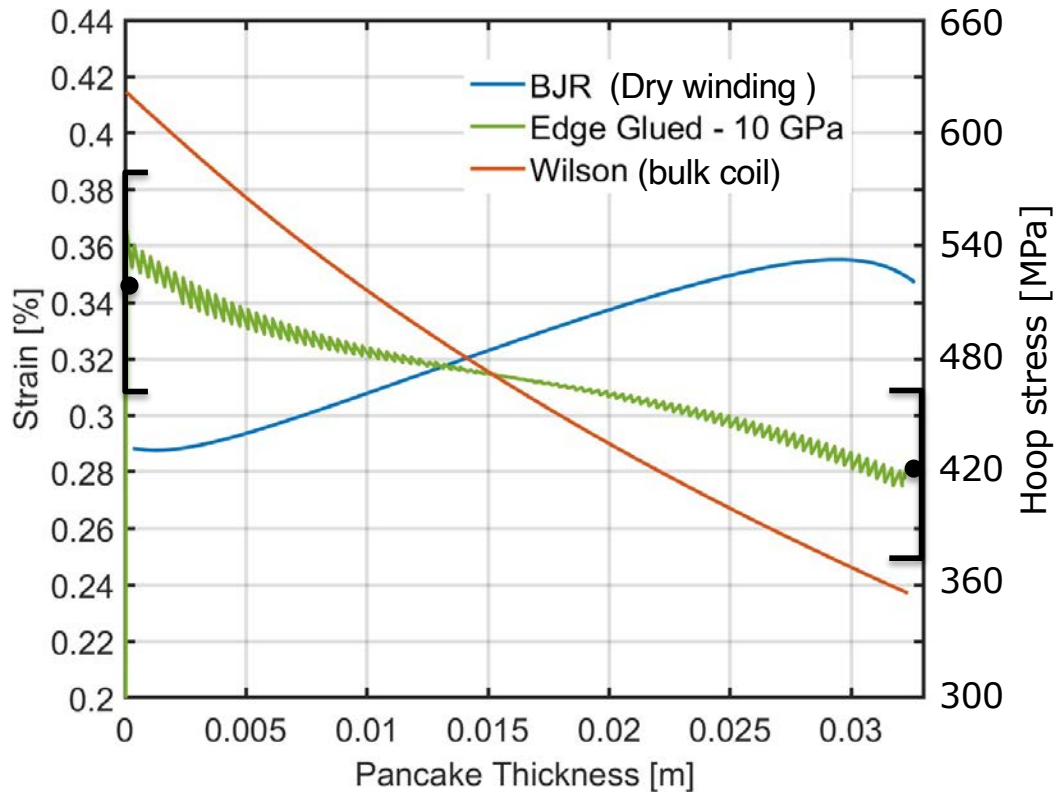


- **Mechanics: Solid deformation, no friction/dry contact → not valid with radial compression**
- Whole conductor is averaged :
 Young Modulus : 150 GPa for 2 x 150 μm REBCO
- Polyimide + Fluorine Insulation represented by elastic interface (in green)
 Very low Young Modulus (1 MPa) represent non-stick behavior
- Epoxy between conductor - FRP flanges : elastic interface (in blue)
 Young Modulus : 10 GPa
- Every turns represented independently or groups of several: save computing time, similar results)



Mechanical study : 2 tape co-wound pancake by Toshiba

Basic studies : “Wilson” hypothesis (all turns glued strongly together)
or “BJR” (all turns acting independently)

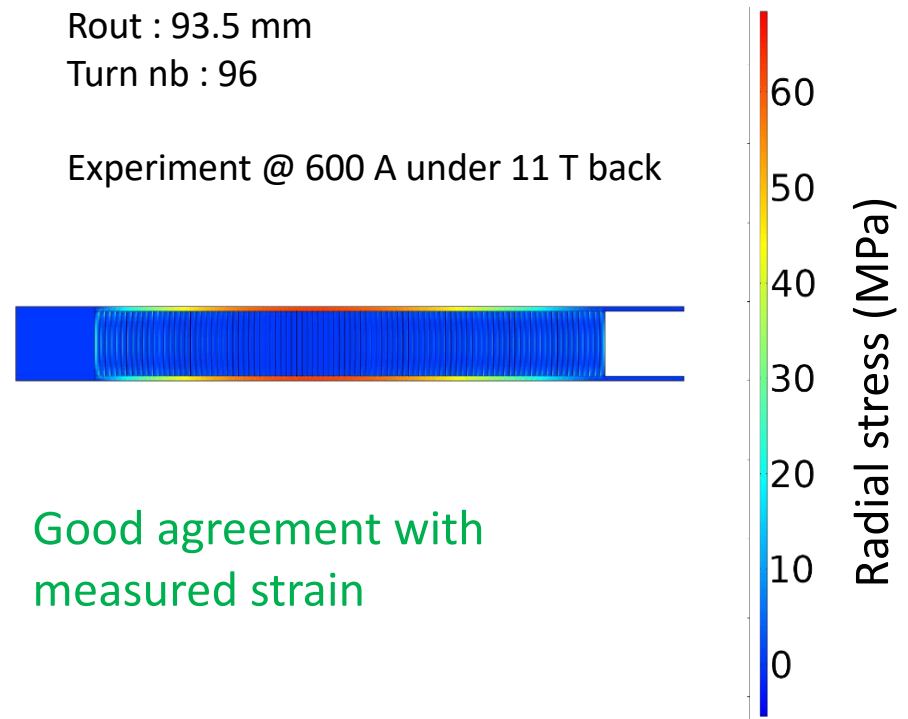


K. Takahashi, IEEE TAS, 2021

30 T project sub-scale test pancake

Conductor : 4mm wide, 2 x 150 um Fujikura tape
Rin : 60 mm
Rout : 93.5 mm
Turn nb : 96

Experiment @ 600 A under 11 T back



Good agreement with measured strain

Question: How's screening current induced stress?



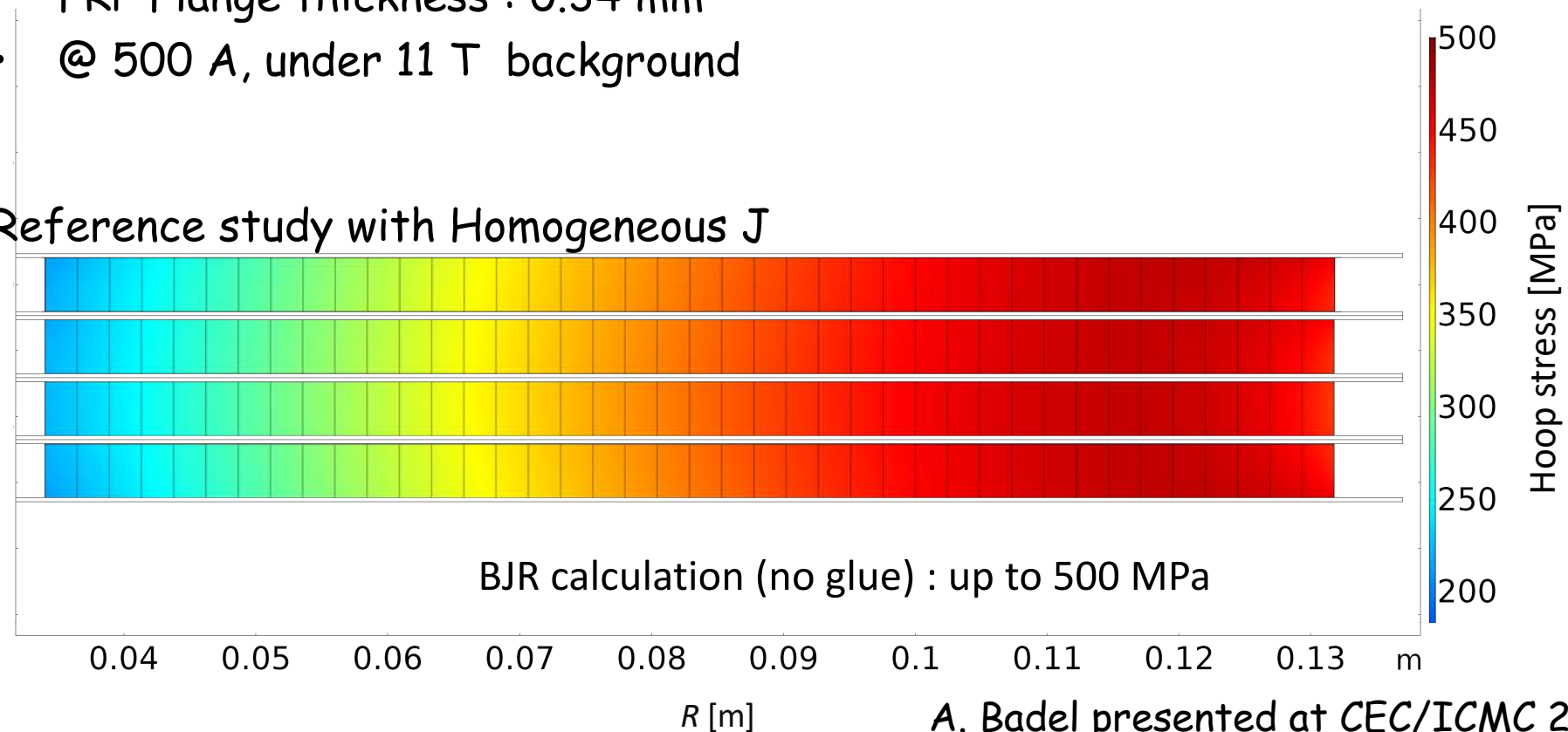
Effect of inhomogeneous J on stress distribution - Reference

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Modelled case : stack of 4 full-scale pancakes from 30 T project insert

- Conductor : 4mm wide, 2 x 150 um Fujikura tape
- R_{in} : 34 mm
- R_{out} : 132 mm
- Turn nb : 300
- FRP Flange thickness : 0.34 mm
- @ 500 A, under 11 T background

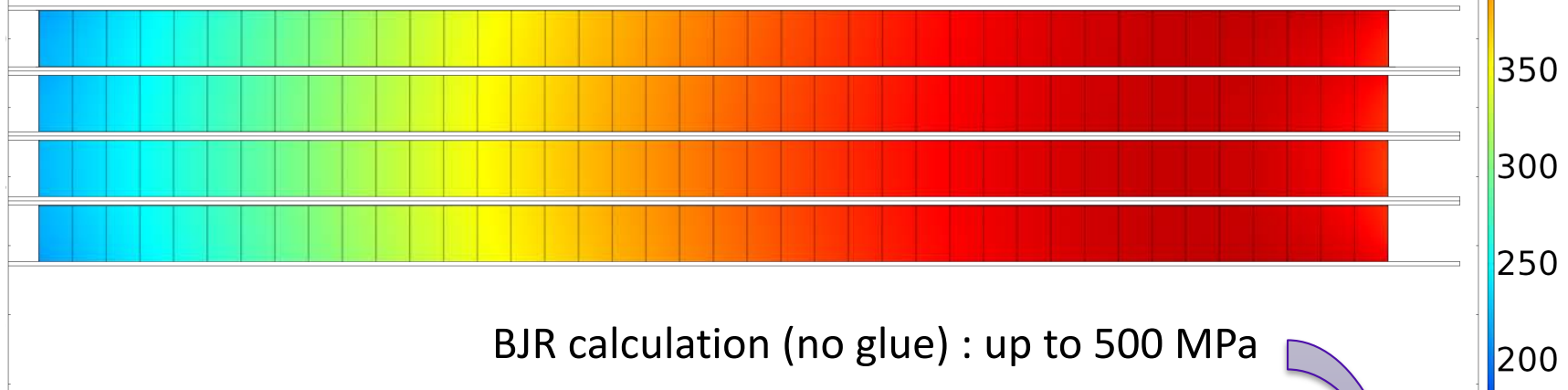
Reference study with Homogeneous J



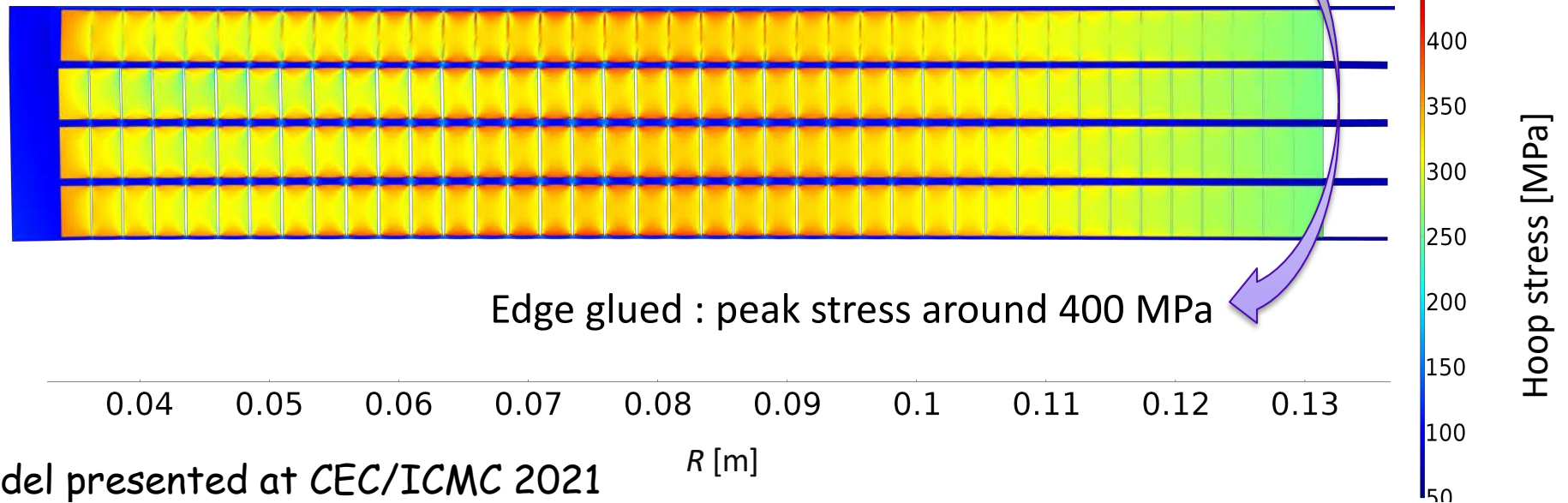


Effect of inhomogeneous J on stress distribution - Reference

Dry winding with Homogeneous J



Edge impregnation with Homogeneous J





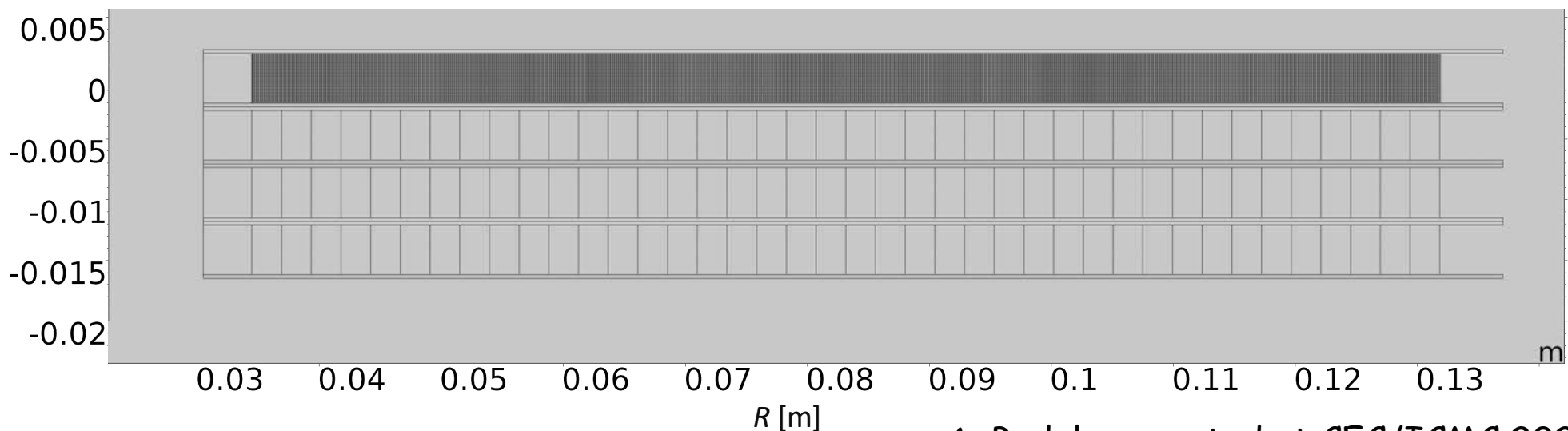
Effect of inhomogeneous J on stress distribution - model

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- Input: Current density distribution @ 500A including transport, shielding and coupling currents

Obtained from detailed transient ElectroMag model (static background of 11 T added)

- In static magneto-mechanical model, top pancake modelled tape by tape: detailed local J and resulting Lorentz force $F_v = J \times B$ applied
- Other three pancakes simplified and considered with homogeneous J (as before) to include their field contribution, background field also added





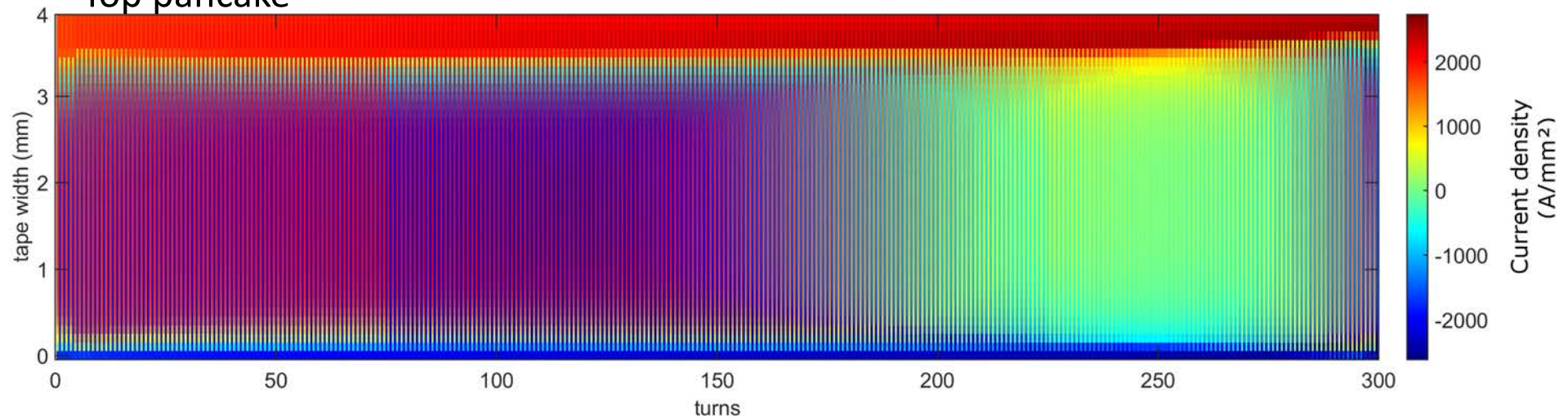
Effect of inhomogeneous J on stress distribution - model

17

- Input: Current density distribution @ 500A including transport, shielding and coupling currents

Obtained from detailed transient ElectroMag model (static background of 11 T added)

- In mechanical model, top pancake modelled tape by tape: detailed local Lorentz force $F_v = J \times B$ applied
- Other three pancakes simplified and considered with homogeneous J (as
Top pancake

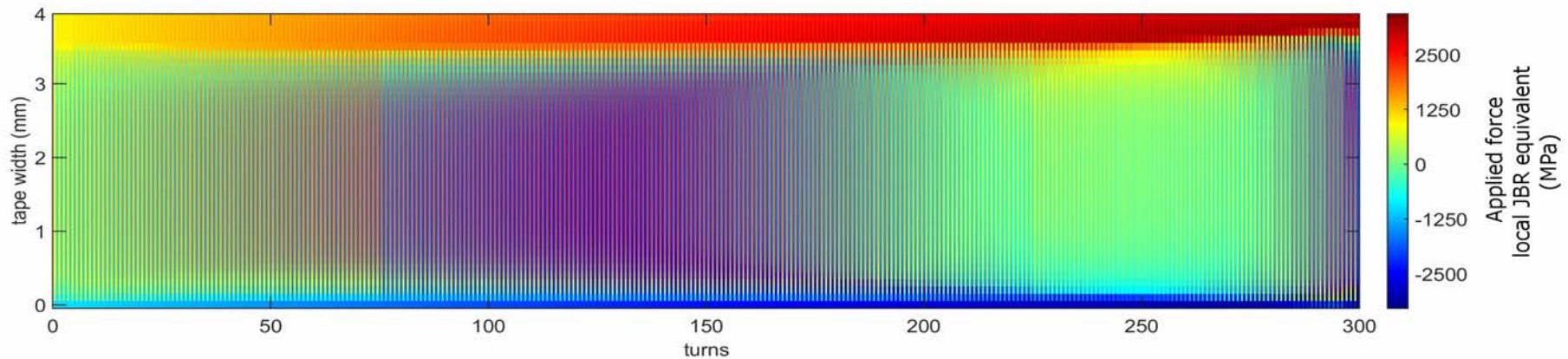




Effect of inhomogeneous J on stress distribution

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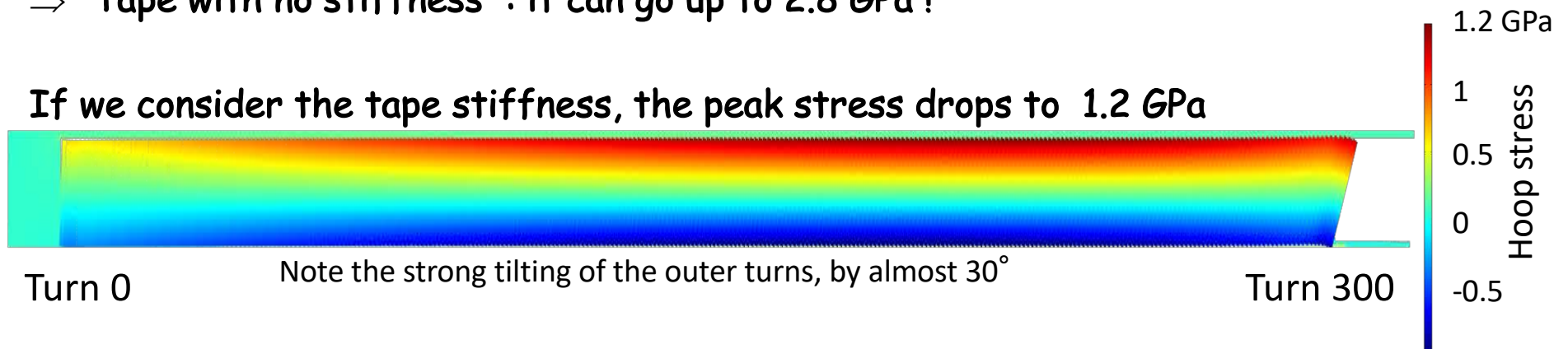
With J and B, we have the applied Lorentz force F_V , but not the stress σ
Indeed $\sigma = B J R$ not valid locally, only when integrated over the conductor



Local BJR equivalent: What local stress would be if every element of each tape acted independently

⇒ Tape with no stiffness : it can go up to 2.8 GPa !

If we consider the tape stiffness, the peak stress drops to 1.2 GPa



Turn 0

Note the strong tilting of the outer turns, by almost 30°

Turn 300

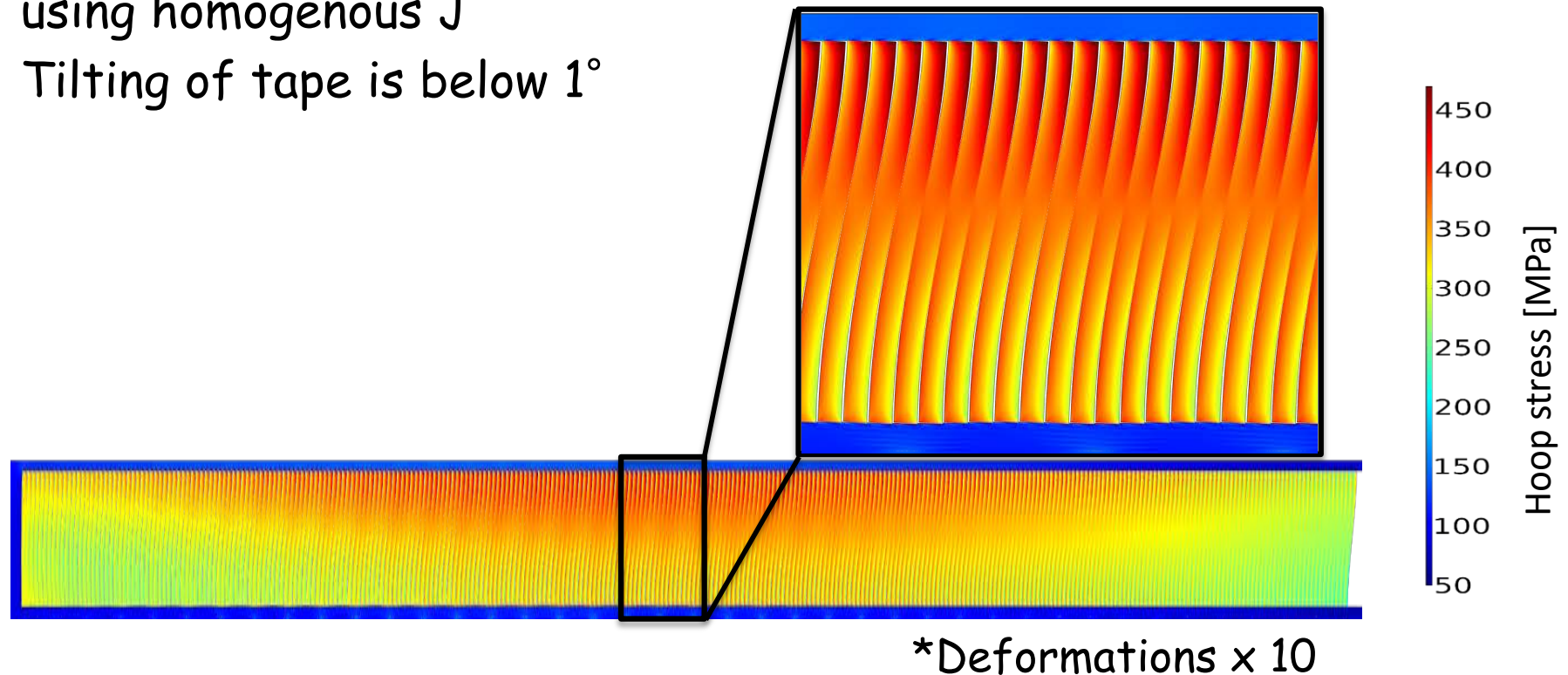


Effect of inhomogeneous J on stress distribution

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We must also consider the interactions of the turns, with each other and with the flanges

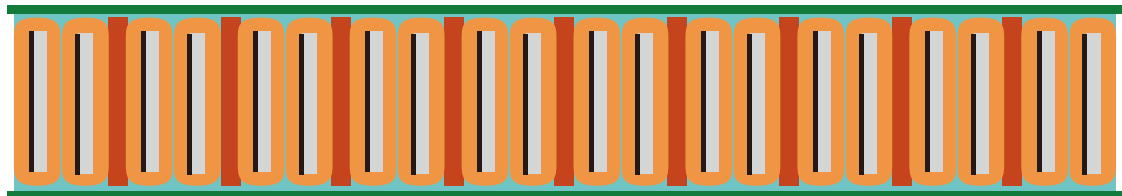
- Glued edge (10 GPa) and turn to turn separation
 - Peak stress is reduced to 455 MPa, about 10 % than estimation using homogenous J
 - Tilting of tape is below 1°



⇒ Edge impregnation concept: effectively reduce damage risks due to shielding currents without the drawbacks of full impregnation

Conclusion

- We propose the “robust” coil concept for REBCO coated conductor.
- Robust against local degradation
 - The effectiveness of two tape co-winging is confirmed by damaged coil.
- Robust against mechanical stress
 - Edge impregnation: Thin flange helps containing the turns while keeping radial stress low on the tape
 - Turn to turn separation to limit the risk of delamination
 - Adjust the hoop stress profile
 - Reduce the screening current induced stress drastically
- Further studies are needed to check the performances of tape - flange bonding
but experimental results so far are reassuring, even under high stress



Thank
you !