

Powering test results of HTS undulator prototype coils for compact FELs at 4.2 K

Sebastian C. Richter^{1,2}, A. Ballarino¹, A. Bernhard², A. W. Grau², D. Saez de Jauregui² and A.-S. Müller²



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Background: free-electron laser (FEL)



The plain undulator...



... in an FEL



Self-amplified spontaneous emission (SASE) \rightarrow Microbunching

$$\mathbf{r} = \frac{\lambda_{\rm u}}{2\gamma_{\rm r}^2} \left(1 + \frac{\mathrm{K}(\mathbf{B}, \lambda_{\rm u})^2}{2}\right)$$

Schmüser, Dohlus, Rossbach; Ultraviolet and Soft X-Ray Free Electron Lasers, Springer (2008).

Background: damping undulator/wiggler



• Definition *undulator* vs. *wiggler:* K parameter \rightarrow radiation spectrum,



 $K = \frac{e \cdot B\lambda_{\rm u}}{2\pi m_e c}$



P. Peiffer, "The Status of the Damping Wiggler Project for the CLIC Damping Rings", The 16th Pan-American Synchrotron Radiation Instrumentation Conference, Chicago (2010).

Link to <u>CLIC</u> and <u>FCC-ee</u>:
 High magnetic fields (> 2 T),
 Long period lengths (> 40 mm).



D. Schoerling *et al.*, "Design and system integration of the superconducting wiggler magnets for the Compact Linear Collider damping rings" (2012), doi: 10.1103/PhysRevSTAB.15.042401.

Background: use case



- The next generation of compact, highly brilliant light sources may profit from high-temperature superconducting (HTS) undulators:
 - Potential enhancement of undulator parameters,
 - e.g., magnetic flux density (B) amplitude for given undulator period length (λ_u),
 - Facilitated operation compared to LTS, like Nb-Ti or Nb₃Sn
 - \rightarrow Relaxed cryogenic requirements (lower costs), larger margins.
- Link to <u>CompactLight</u>:
 - Hard X-ray FEL

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- Short-period undulators
- Low electron beam energy



- (< 1 nm), (~ 13 mm),
- (2.5 to 5.5 GeV).



F. Nguyen *et al.* "XLS - D5.1: Technologies for the CompactLight Undulator" (2019), doi: 10.5281/zenodo.5024409

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Background: different superconductors





More on superconductor's critical current densities: <u>ASC Plot</u> (by P. Lee)

** J. van Nugteren, High Temperature Superconductor Accelerator Magnets, PhD (2016)

Motivation: 2D e/m-simulations





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Other HTS undulator approaches (I)



I. Kesgin *et al.*

- Continuous ReBCO tape winding (4 mm width, 95 µm thick),
- Non-insulated and partial-insulated jointless winding with U-turns:
 - Mirror-model with all VR coils wound from one tape,
 - $B_y \approx 1 \text{ T for } \lambda_u = 16 \text{ mm}, \text{ g} = 9.5 \text{ mm}$ $(I_{op} = 800 \text{ A} \rightarrow J_{op} \approx 2.1 \text{ kA/mm}^2).$





I. Kesgin *et al.*, "High-temperature superconducting undulator magnets" (2017), doi: 10.1088/1361-6668/aa5d48.

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Other HTS undulator approaches (II)



T. Holubek et al. and A. Will et al.

- 30 layers of laser-structured ReBCO tapes (12 mm width, 55 µm thick),
- Non-insulated jointless winding or soldered-stacked design:
 - The structure in each tape forces the current on a defined path,
 - $B_y = 1$ T for $\lambda_u = 8$ mm, g = 4 mm ($I_{op} = 500 \text{ A} \rightarrow J_{op} \approx 2.2 \text{ kA/mm}^2$).







T. Holubek *et al.*, "A novel concept of high temperature superconducting undulator" (2017), doi: 10.1088/1361-6668/aa87f1

A. Will et al., "Design and Fabrication Concepts of a Compact Undulator with Laser-Structured 2G-HTS Tapes" (2021), doi: 10.18429/JACoW-IPAC2021-THPAB048.



About the Project





Further investigations on bending radii < 5 mm.</p>



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VR Undulator Coil: design



- Two non-insulated sub-coils with opposite current direction on the same winding body, separated by an insulator.
- Innermost turns of both sub-coils are soldered along the curved side to a 10 mm wide coated ReBCO tape (main electrical connection).
 - *Current flow*: sub-coil 1, spiral to its center, bridge to sub-coil 2, spiral out.



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VR Undulator Coil: manufacturing

4 mm wide and

- 100 µm thick Bruker HTS tape (VR coil #1 and #2),
- 45 μm thick SuperPower tape (VR coil #3).
- The first turn was fixed by a pin and soldered along the curved side to the 10 mm tape,
 - Sn62Pb36Ag2 solder paste @ 185 °C for 5 min.
- Winding with controlled winding tension {30 N, 25 N}.
- The last turn was soldered along the curved side,
 - 97In3Ag solder paste @ 155 °C for 5 min.

Contact: copper lead with indium foil,
4 voltage taps (sub-coil's start and end).









S. C. Richter *et al.*, "Progress on HTS undulator prototype coils for compact FEL designs" (2021), doi: 10.1109/TASC.2022.3150288.

VR Undulator Coil: 3D modelling



- J_c was defined by considering the worst-case scenario: the max. magnetic field on the conductor B_{cond} perpendicular to the tape plane,
 At 4.2 K: max. B_⊥ ≈ 99.95% B_{cond}.
- 0.2 kN 4.9 T 4.8 kN -4.0 T 4.8 kN 16 MPa 3.0 T E 4.2 K 0.2 kN m 2.0 T 10 MPa 3.9 kN 3.91 O.S. F.V 1.0 T 11 MPa 0.0 T $J_{e}(4.2 \text{ K}) = 2071 \text{ A/mm}^{2}$

	VR coil #2	VR coil #3	
Undulator period λ_u	13 mm		
Sub-coil x-section	$4 \text{ mm} \times 5 \text{ mm}$	$4 \text{ mm} \times 4.6 \text{ mm}$	
HTS conductor	Bruker HTS	SuperPower	
with dimensions	4 mm x 100 µm	4 mm x 45 µm	
Number of turns	51	102	
J _{op. sim} (4.9 T, 4.2 K)	2071 A/mm ²	2222 A/mm ²	
I _{op, sim} (4.9 T, 4.2 K)	828 A	400 A	
$B_{y,1}(I_{c,sim}, d = 3.5 \text{ mm})$	1.38 T	1.24 T	

Opera 2020 Based on the Biot–Savart law

S. C. Richter *et al.*, "Progress on HTS undulator prototype coils for compact FEL designs" (2021), doi: 10.1109/TASC.2022.3150288.

VR Undulator Coil: signal tests at 77 K (LN2)



- current ramping with 0.05 A/s and 0.5 A/s until a drift in voltage was measured.
- With an outermost turn length of 30 cm:

• $I_c(30 \mu V) \leftrightarrow E_c=1 \mu V/cm$





S. C. Richter *et al.*, "Powering Test Results of HTS Undulator Coils at 77 K for Compact FEL Designs" (2022), doi: 10.18429/JACoW-IPAC2022-THPOPT058.

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Hall probes

VR Undulator Coil: signal tests at 77 K (LN2)

Current steps of 2 A with a 300 s decay time

• up to $\approx 300\% I_{c}$

For I > 80 A all sub-coils showed a stable resistance R_{t} .



S. C. Richter et al., "Powering Test Results of HTS Undulator Coils at 77 K for Compact FEL Designs" (2022), doi: 10.18429/JACoW-IPAC2022-THPOPT058.

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Sub-coil 1/2

Fe

G10



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VR Undulator Coil: LHe setup



CASPER I* test station with liquid helium cryostat (at KIT),

- Current: 1500 A/ ±5 V and 500 A/ ±5 V power supplies,
- Quench detector for coil protection,

1 mV (later 4 mV),
 10 Hz DAQ time.





- 1) Current ramping with 0.25 A/s
 - Voltage peaks,
 - drifts in decayed voltage.







- 2) Effective time constant τ :
 - Current step function (0 A 200 A),
 - Measure voltage decay over time: $U \approx a \cdot e^{-t/\tau_i} + b \cdot e^{-t/\tau_{avg}}$





	VR coil #2		VR coil #3	
τ	76 s	74 s	(5 s)	121 s

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- 3) Magnetic field build-up:
 - Hall sensor signal







- 4) Current steps and overflow:
 - Current steps of 40 A (VRC#2) and 20 A (VRC#3) with a 300 s decay time

 \rightarrow too short and 30 μ V too conservative







- 5) Overflow and quench
 - Current steps continued until U runaway.
 - VRC#2: no value (defect Nb-Ti current lead),
 - VRC#3 at 660 A (~3.6 kA/mm²).





Summary and Conclusion



- The technical potential of HTS for undulators has been demonstrated.
- 3 VR prototype coils were manufactured and tested in LN2 and 2 in LHe.
 - Simulations matched the experiment,
 - Stable operation at the designed current,
 - Stable up to I_c and beyond without any degradation,
 - Tunable undulators may be challenging without metal/partial insulation.

Next steps:

- Controlled turn-to-turn resistance:
 - Higher resistance is preferred at 4.2 K.
- Investigation of
 - Mechanical margins,
 - Field quality (+ ramping),
 - Beam tracking.

Future plans:

- 3 VR coil short model,
- Manufacture the world's first ReBCO tape helical undulator (demonstrator).



Helical undulator short model

What's next? Appetizer: helical HTS undulator

Why a helical undulator?

→ More compact and efficient! **B**_y \ge 2.3 T for λ_u = 13 mm, g = 5 mm, Wound with 4 mm wide ReBCO tape.



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