#### Readout electronics for NIKA

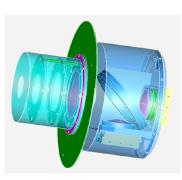
O. Bourrion A. Bideaud A. Benoit A. Cruciani J.F. Macias-Perez A. Monfardini M. Roesch L. Swenson C. Vescovi

CNRS-IN2P3-I PSC Grenoble

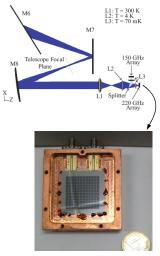
October 3, 2011

### NIKA camera









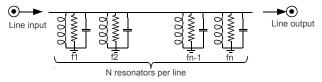
144 pixels array

# MKID: reminders



• Bolometer array = line with n high Q resonators

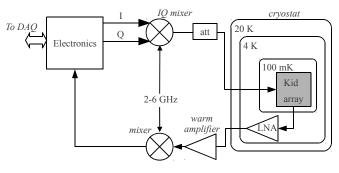
- Bolometer array built by microlithography
- Average resonator self resonant frequency spacing of 2 MHz.
- Resonance frequency at several GHz



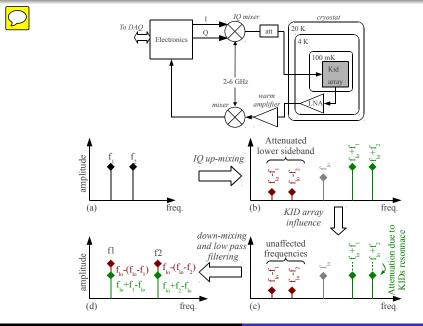
- $\bullet$  Detection principle  $\rightarrow$  shift of the resonator self resonant frequency when illuminated.
- Constraints:
  - Array at very low temperature (cryostat at 100 mK)
  - Cable feedthrough must be kept to a minimum
  - Work in RF domain
  - Full array readout at several Hertz

# Array instrumentation method (1/2)

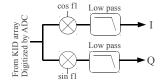
- $\bigcirc$
- Generation of a frequency comb (frequency multiplexing):
  - $\bullet\,$  Containing the largest possible number of frequency (  $\rightarrow\,$  Output analog frequency (Shannon))
  - Each frequency adjustable at a kHz resolution.
- Op-mixing of the baseband generated frequency comb
- The signal passes through the array and is eventually modified
- At the array's output, down-mixing to baseband
- Signal processing: determine each tone amplitude and phase



## Array instrumentation method (2/2)



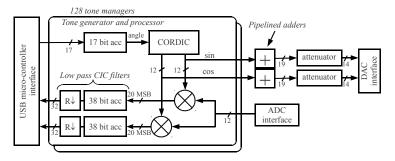
- Sine and cosine waves generated by CORDIC (COordinate Rotation DIgital Computer)
  - Using only adder/subtracters and a small precomputed arc tangent table
  - Easily algorithm "pipelining"
  - Can reach sine and cosine resolution of  $1/2^{n-1}$ , where n is the number of +/- stages and atan constants
- Icine output signal analyzed by Digital Down Conversion (DDC)
  - As much processors as spectral rays to analyze
- Principle: signal is shifted to baseband and projected on I, Q axis by multiplying the returning signal by the original sine and cosine wave
- Low pass filter actually implemented by 1 ms signal averaging (not moving average →CIC!!)
- For  $A\times \sin(\omega t+\phi) \Rightarrow |A|=\sqrt{I^2+Q^2}$  and  $\phi=\arctan\frac{Q}{I}$



### FPGA content

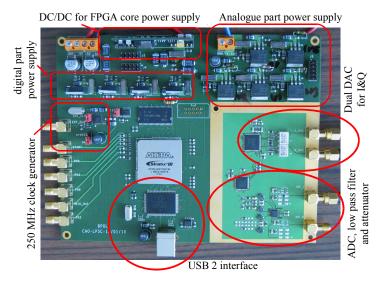


- 128 CORDIC generators
- 128 DDC



#### First prototype

#### • Fadc=FDAC=250 MHz, fanalog max 125 MHz



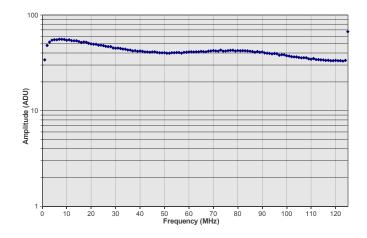
### Equipped rack

- Electronic board
- Data server PC (Ubuntu) for Ethernet interfacing
- AC/DC power supplies + fan control



### Frequency response

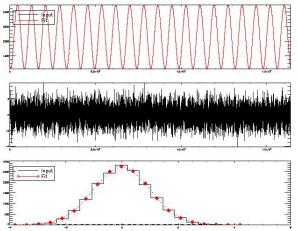




- Flat response over the whole bandwidth (-20 dB over 125 MHz).
- Attenuation mostly due the input Variable Gain Amplifier.

### Signal to Noise in loopback mode

- $\mathcal{O}$
- Sine wave at  $\sim$  300 kHz
- $\bullet~\mbox{Fiiting}$  of a perfect sine wave  $\rightarrow~\mbox{RMS}{=}1.1$
- Electronic chain allows to recover up to  ${\sim}11$  effective bit (out of 12)



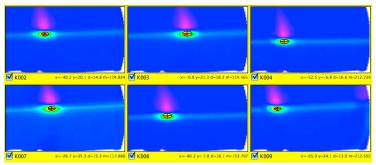
### First images with the sky simulator

 $\mathcal{O}$ 

• A source at ambient temperature is placed between a cold plate and the MKID array and moved in 2D

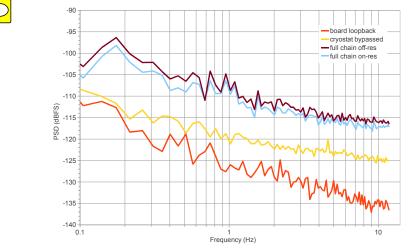


Thin Nylon wire Moving "Planet"



• The "planet" is seen when passing in front of a MKID pixel.

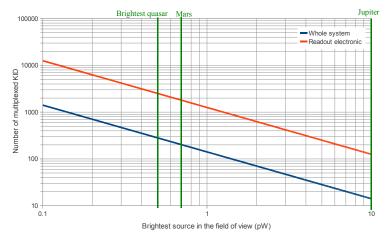
## System noise contributor identification



- Noise is not due to the MKIDs themselves (see off/on resonance)
- Noise floor electronic alone at -135 dB
- **③** Noise added by mixing electronics is +10 dB
- Old amplifier adds 10 dB of noise

# Multiplexing limit

- $\mathcal{O}$
- When targeting a constant resolution of  $50~{\rm aW}/{\sqrt{\rm Hz}}$  at an acquisition rate of 20 Hz with a fixed dynamic range of 115/135 dB, the multiplexing limit is fixed by the brightest spot in the FOV

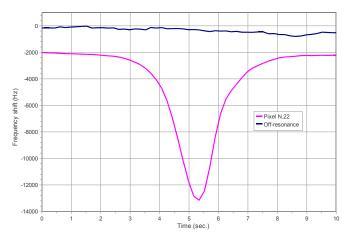


• Mars in FOV ightarrow 110 MKIDs, Jupiter in FOV ightarrow 10 MKIDs!!

## Crosstalk between MKIDs



- Using sky simulator with cold plate at 50 K
- Highly emissivity ball simulating the planet at 300 K



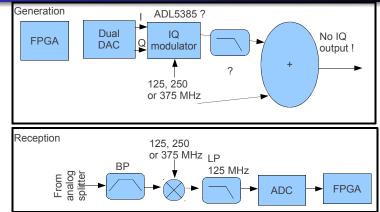
#### Summary 1<sup>st</sup> prototype

- Technology and know-how validated for 128 spectral rays fitting in a bandwidth of 125 MHz
  - $\bullet\,$  Validation done with 64 bands separated in average by 2 MHz
- see 2011 JINST 6 P06012, also available at arXiv:1102.1314

#### Future

- Equip arrays featuring 2000+4000 pixels
- Design and construct electronic boards able to manage 256 spectral rays over a bandwidth of 500 MHz
  - Limited by trade off between number of spectral rays and multiplexing limit
  - Technical difficulty (computing power/FPGA size, bandwidth, ...)

# Obvious (?) "analog" solution



- Idea: split the 500 MHz bandwidth in 4 bands: 0 $\rightarrow$ 125, 125 $\rightarrow$ 250, 250 $\rightarrow$ 375, 375 $\rightarrow$ 500 MHz
- 1<sup>st</sup>drawback: impossible to build directly the comb in IQ
- 2<sup>nd</sup> drawback: practically impossibility to have highly selective filters massive crosstalk due to image frequencies!!

# All "digital" solution



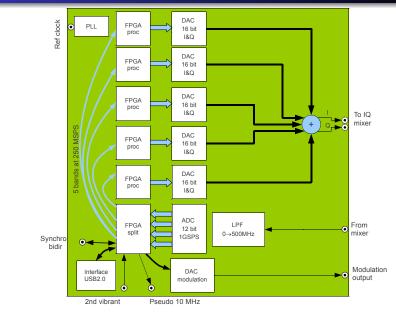
#### Frequency comb generation

- Nowadays DAC providing analog samples at 1 GSPS while receiving digital inputs at 250 MSPS exist off the shelves
- **Principle**: features digital modulators, interpolators and very steep (high order) filters
- $\bullet \, \Rightarrow$  Use 5 DACs to build 5 100 MHz wide bands to generate the excitation comb

#### Returning signal digitization and processing

- ADC running at 1 GSPS exist but impossible to manage so many spectral rays in a single FPGA
- Using polyphase filtering and digital demodulation, it is possible to separate the 5 bands and bring them back in baseband for a "regular" processing.
- Becomes almost identical to 5 times the processing developed and implemented in version 1

#### Board block diagram



## Conclusion

- One board will instrument between 256 (2 MHz spacing) and 500 pixels (1 MHz spacing)
- ullet  $\Rightarrow$  For 4000 pixels, less than 16 boards required
- Algorithms of the frequency band separator developed and coded in VHDL
- New board available and in debug

