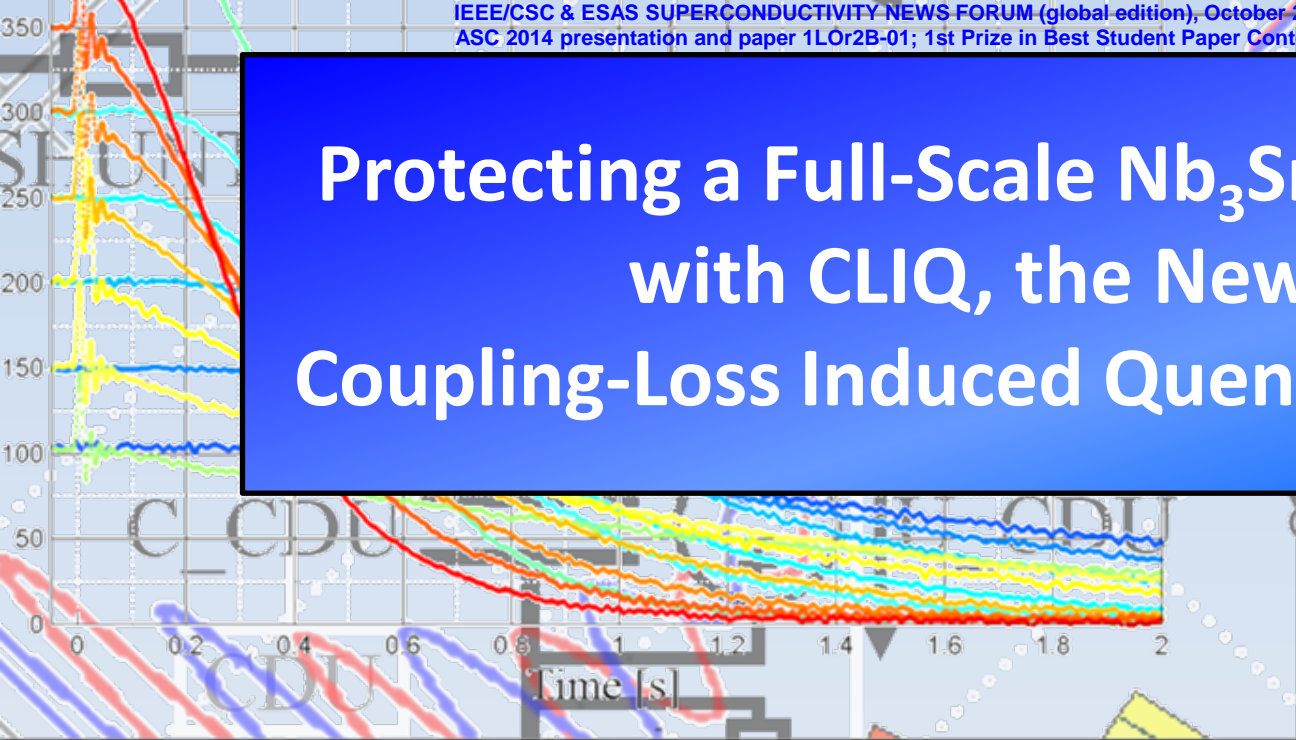


Protecting a Full-Scale Nb₃Sn Magnet with CLIQ, the New Coupling-Loss Induced Quench System



Emmanuele Ravaioli^{a,b}

H. Bajas^a, V. I. Datskov^a, V. Desbiolles^a, J. Feuvrier^a,
G. Kirby^a, M. Maciejewski^{a,c}, GianLuca Sabbi^d,
H. H. J. ten Kate^{a,b}, Arjan P. Verweij^a

^aCERN, Geneva, Switzerland

^bUniversity of Twente, Enschede, The Netherlands

^cLodz University of Technology, Lodz, Poland

^dLawrence Berkeley National Laboratory, Berkeley, USA

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Protecting a Full-Scale Nb₃Sn Magnet with CLIQ

CLIQ

Coupling-Loss Induced Quench

First CLIQ tests on
a Nb₃Sn magnet

Validation of the
simulation tools

Optimization
strategy

**CLIQ-based solution for the protection
of full-scale quadrupole magnets**

Analyzed case: Quadrupole magnet for the LHC
high luminosity upgrade (US-LARP collaboration)

Quench Protection in a Superconducting Magnet

High Current Density

$$J \approx \text{kA/cm}^2$$

High Magnetic Field

$$B = 5\text{-}10 \text{ T}$$

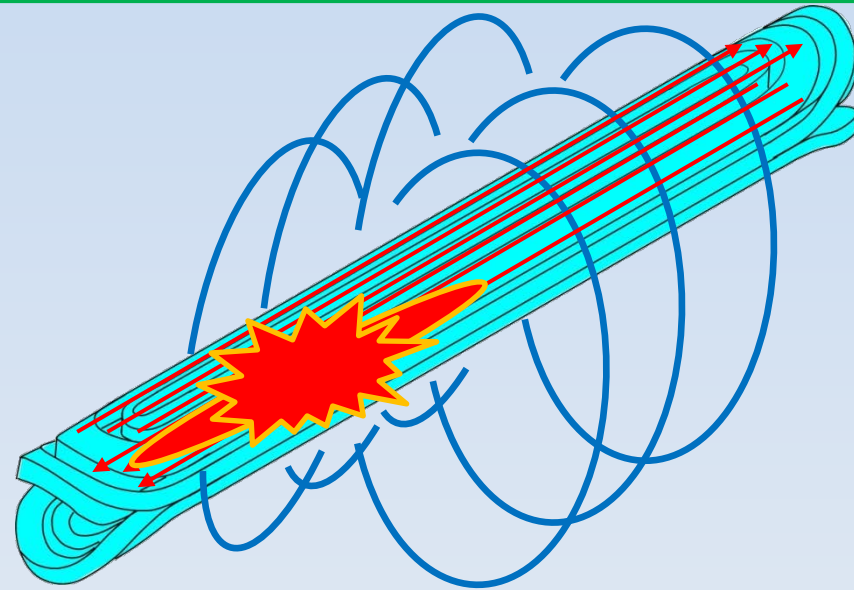
High Energy Density

$$e = B^2 / (2 \mu_0) \approx 10\text{-}40 \text{ MJ/m}^3$$

Quench

If a portion of cable suddenly becomes non-superconducting, it starts heating up

The energy stored in the magnet is usually sufficient to melt kilos of Copper and destroy the magnet!



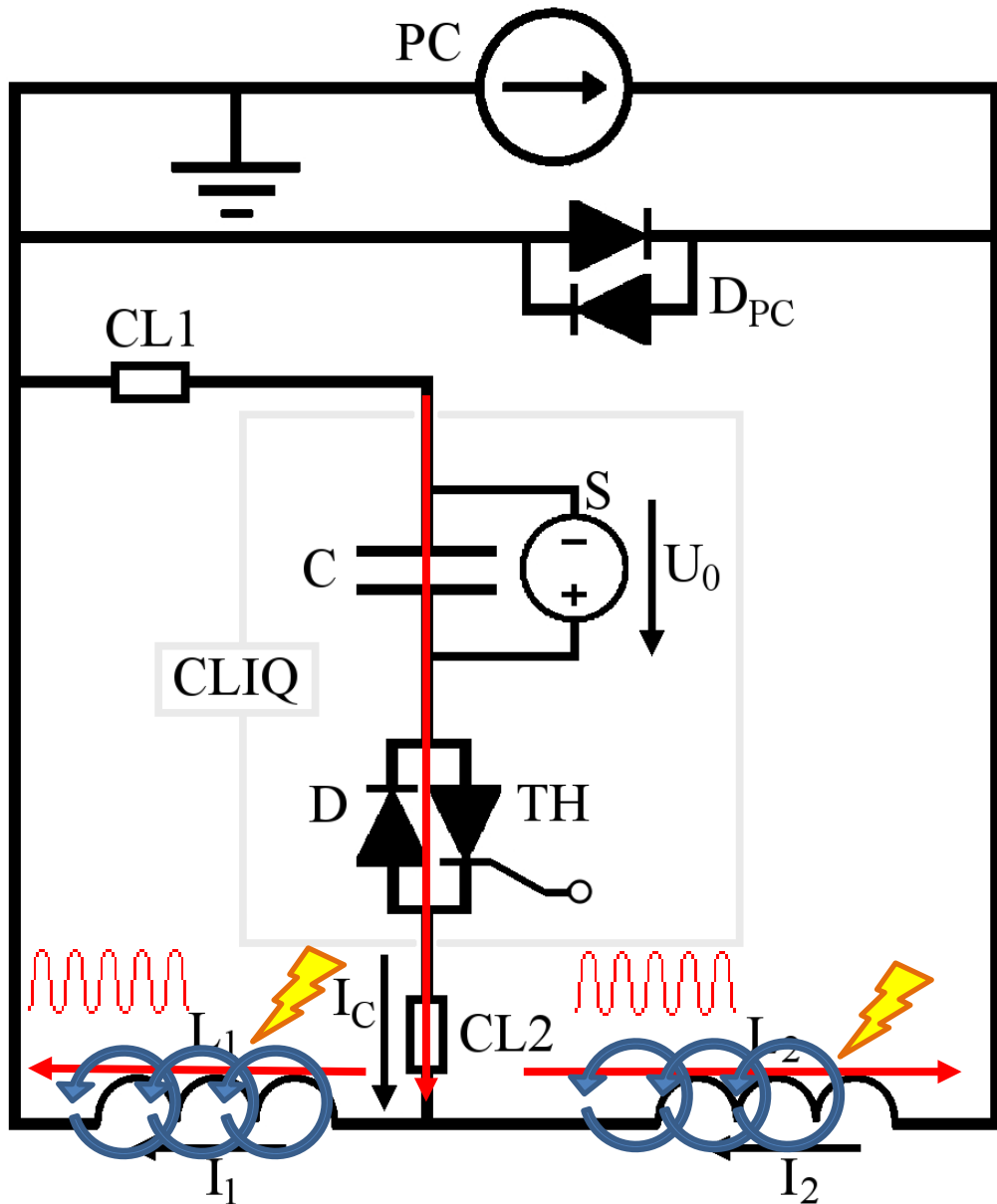
Quick propagation of the quench needed

Homogeneous
distribution of the
quench energy

Discharge of the
magnet current
with coil resistance

Conventional **Quench Heaters** may be too **slow** (relying on thermal diffusion across insulation layers) and are prone to **electrical breakdown** (thin insulation)

CLIQ – Coupling-Loss Induced Quench



Current Change

Magnetic Field Change

Coupling Losses (Heat)

Temperature Rise

QUENCH

CLIQ – Main Advantages



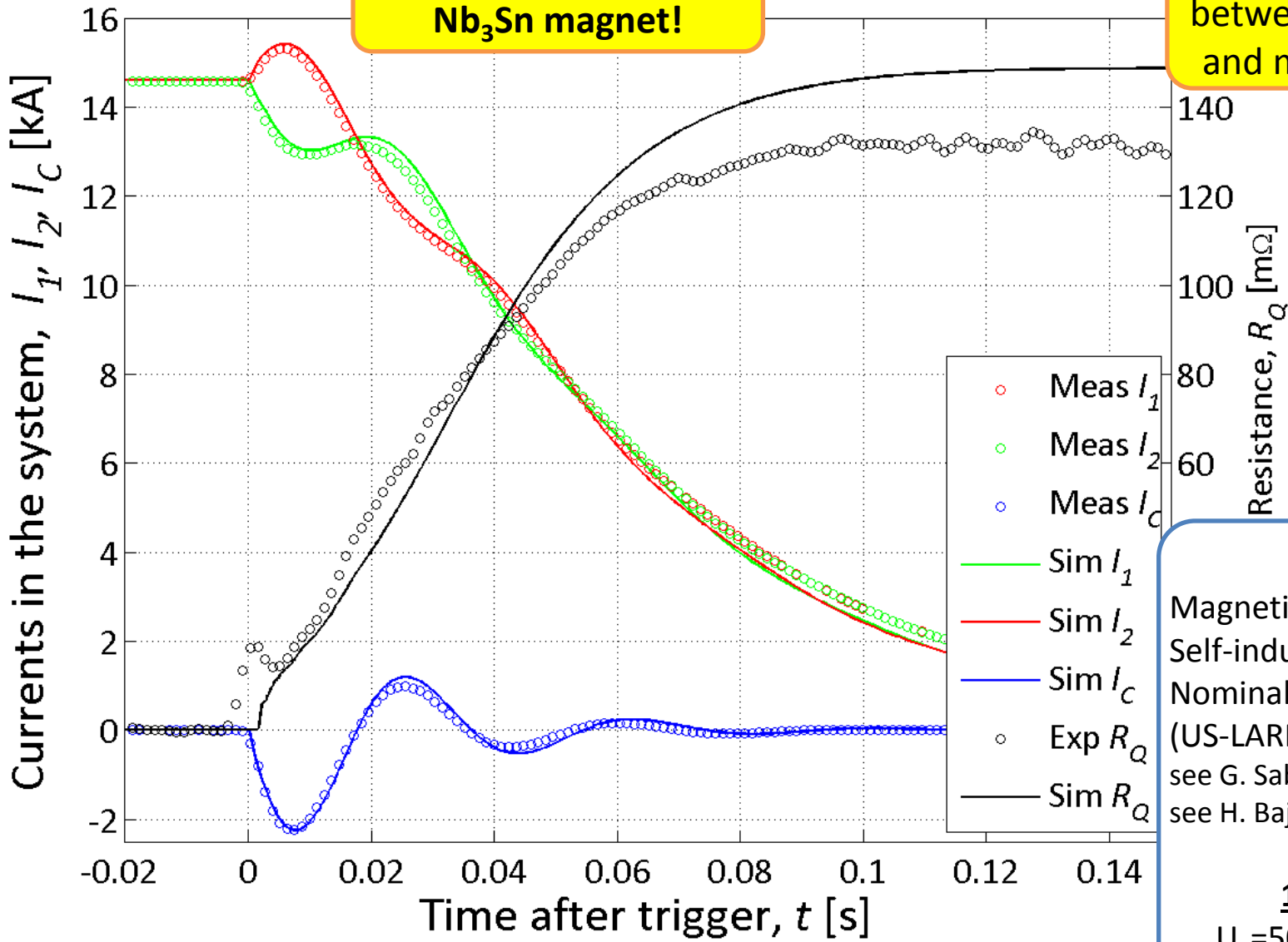
- More **efficient** energy deposition
- **Faster** and more **homogeneous** quench initiation
- **More robust** design
- **Easier** to implement and repair
- Lower expected **failure rate**
- **External** system not interfering with the coil winding technology
- Possible to use CLIQ as a **back-up solution** for protecting magnets with failing quench heaters

All you need is available **connection(s) to the middle of the magnet** (a few mm² of copper) and a good understanding of **how CLIQ works**

CLIQ tests on the model magnet for the LHC high luminosity upgrade

First CLIQ tests on a Nb₃Sn magnet!

Excellent agreement between simulations and measurements

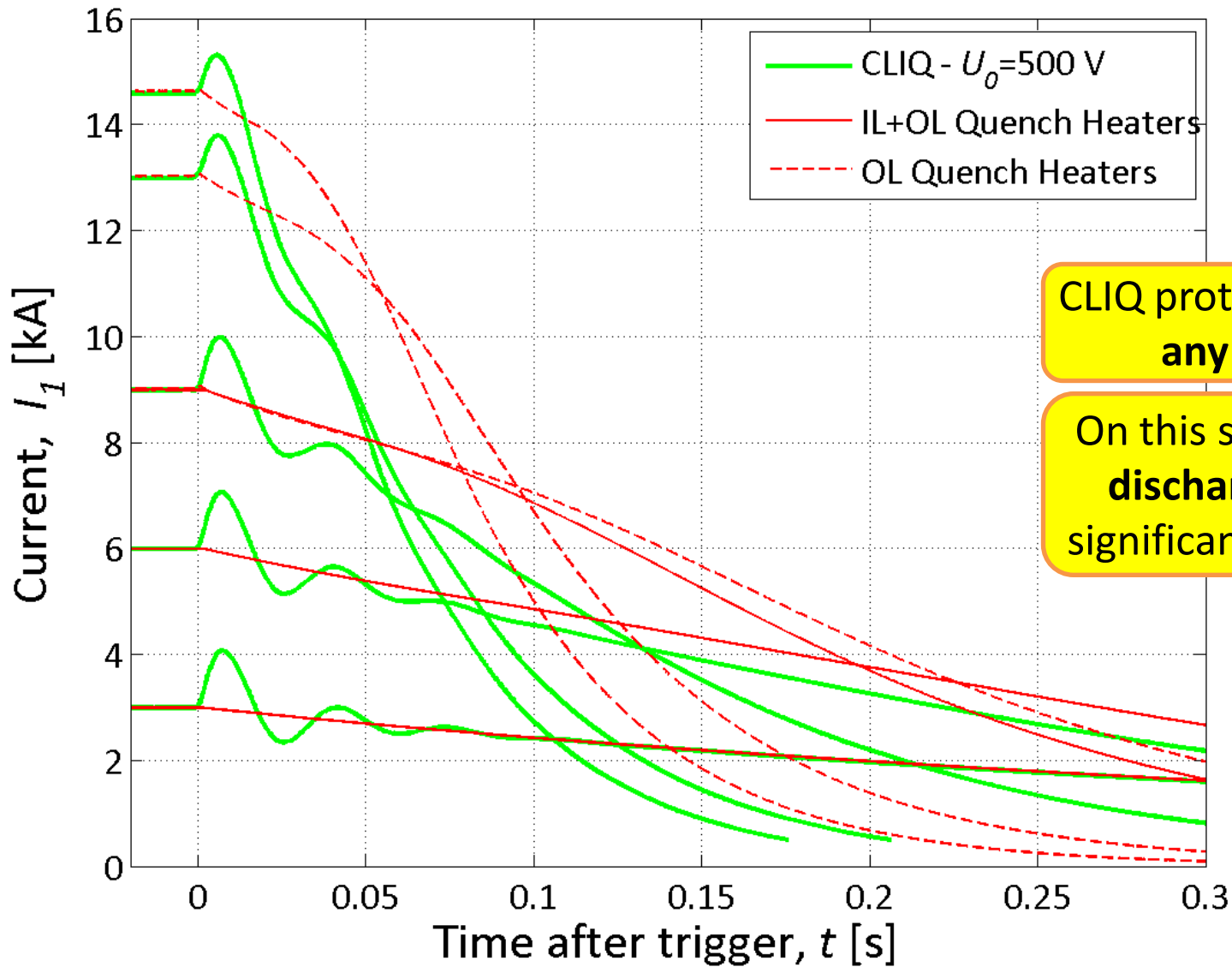


- Meas I_1
- Meas I_2
- Meas I_C
- Sim I_1
- Sim I_2
- Sim I_C
- Exp R_Q
- Sim R_Q

HQ02b
 Magnetic Length 0.8 m
 Self-inductance 6.4 mH
 Nominal current 14.6 kA
 (US-LARP collaboration)
 see G. Sabbi, [1L0r2B-02](#)
 see H. Bajas, [4LPo2E](#)

1 CLIQ Unit
 $U_0=500$ V $C=28.2$ mF

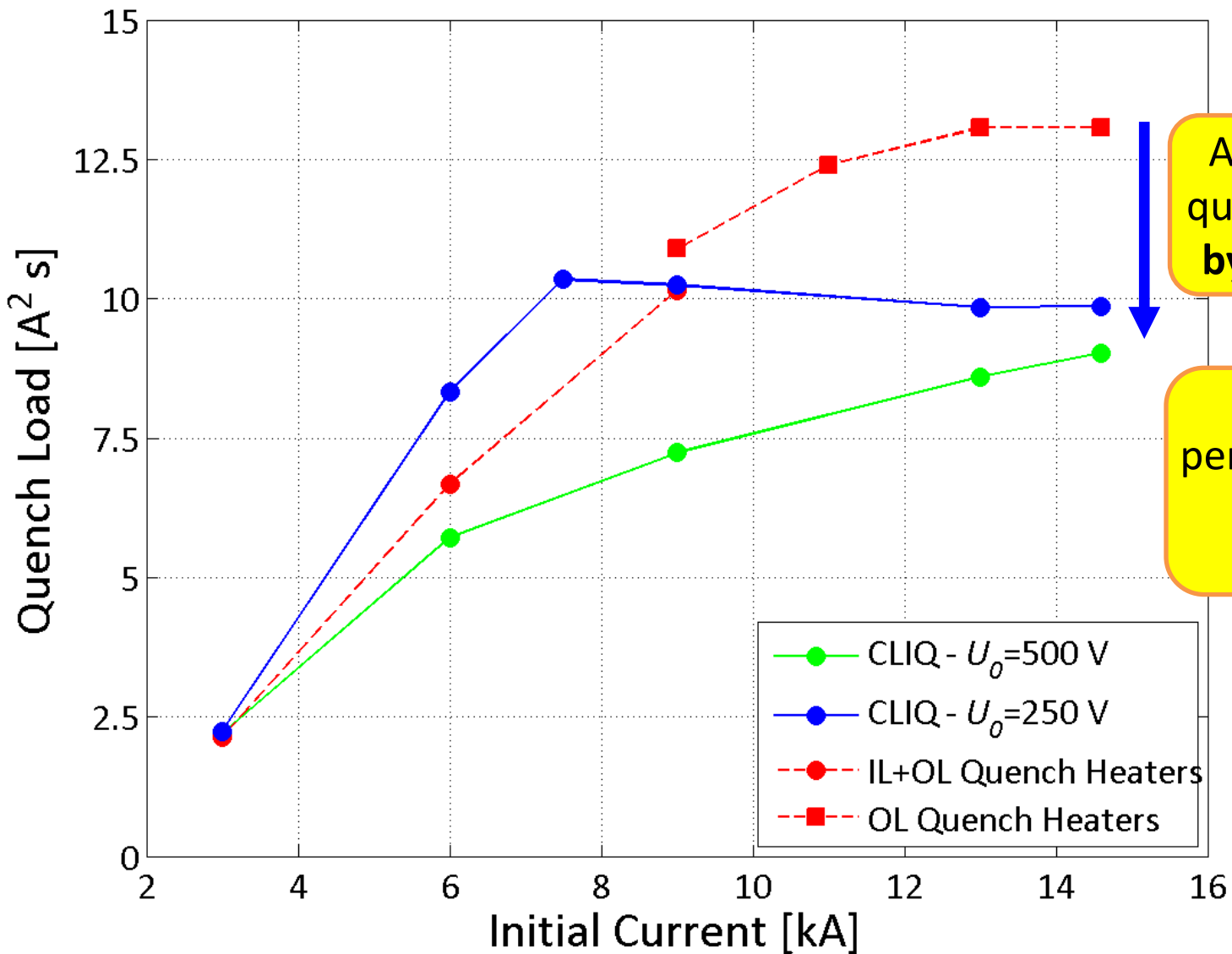
Comparison with Quench Heaters performance



CLIQ protects the magnet at **any current level**

On this short magnet CLIQ **discharges** the magnet significantly **faster** than QH

Summary of CLIQ and QH performance on the model magnet



At nominal current quench load **reduced by ~30%** using CLIQ

However, CLIQ performance strongly depends on the magnet length

Protecting full-scale magnets with CLIQ – The strategy

Power per unit volume deposited by CLIQ depends on inter-filament loss (IFCL)

Charging voltage

(limited for safety reasons)

Number of **CLIQ units**

(for quadrupoles up to **2 units**)

$$\frac{P_{IF}}{vol} \propto \left(\frac{dI}{dt} \right)^2 \propto \left(\frac{U_0}{l_m} \cdot \frac{N_C}{L_{1-CLIQ}} \right)^2$$

Equivalent **inductance** of the discharge circuit

- Coil **geometry**
- **Position** of CLIQ connections
- Electrical **order** of the poles (always an advantage, typically possible with minor changes)

Magnet length

(defined by design)

Capacitance of CLIQ unit

(no effect on power, but \propto to discharged energy)

For a **given** quadrupole magnet

Choose optimum CLIQ **configuration**

Increase **voltage** U_0

2-CLIQ

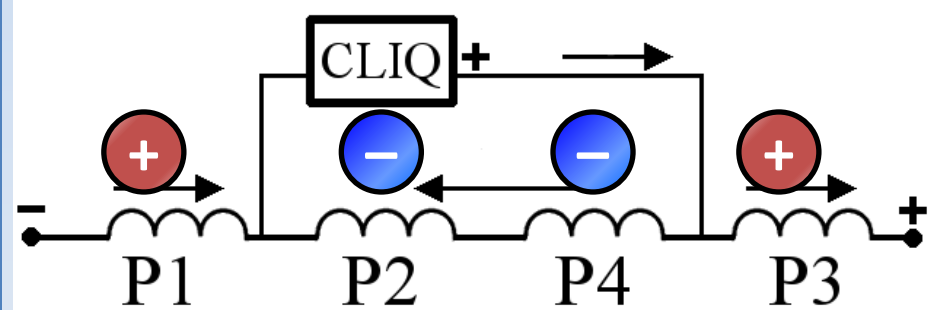
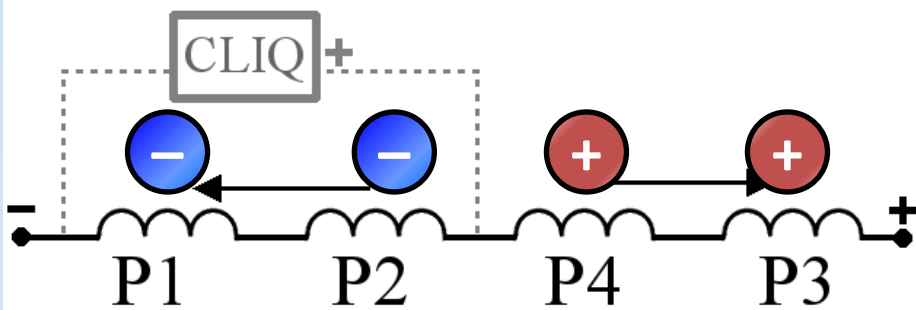
Increase **capacitance** of CLIQ unit(s)

Optimum CLIQ discharge configuration

-1

Not Optimized

Optimized



Significant **reduction** of L_{eq} (2.5-3 times!)
 → Increase of deposited loss (6-9 times!)

$$\frac{P_{IF}}{vol} \propto \left(\frac{dI}{dt} \right)^2 \propto \left(\frac{U_0}{l_m} \cdot \frac{N_c}{L_{1-CLIQ}} \right)^2$$

Golden rule for optimizing any CLIQ discharge circuit

Introduce opposite current change in coils which are physically adjacent

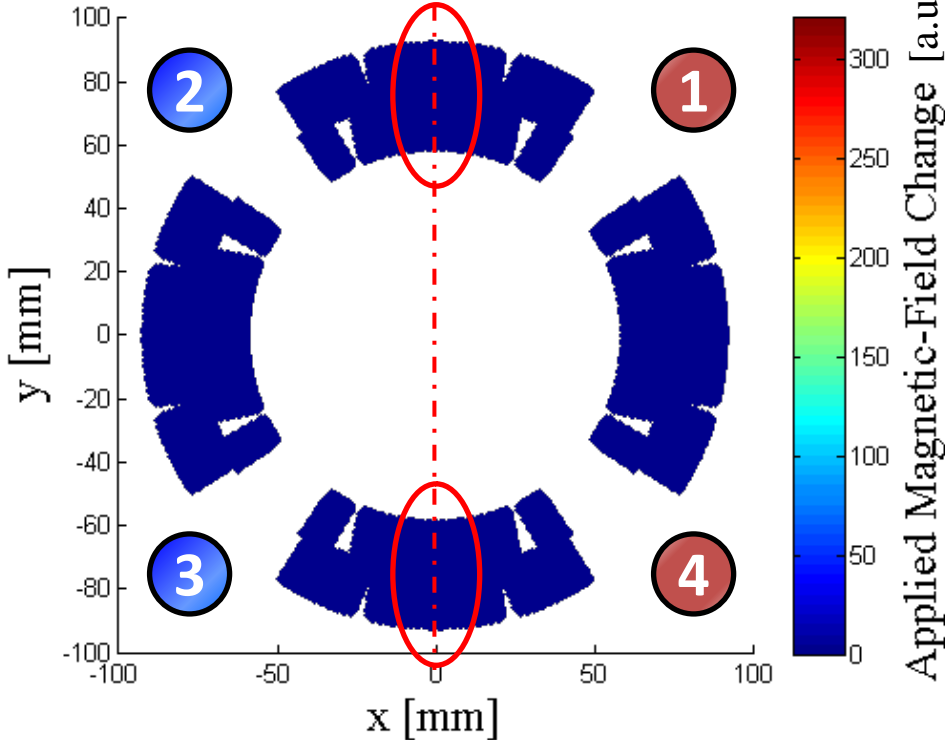
Optimum CLIQ discharge configuration

-2

Efficient distribution of magnetic-field change

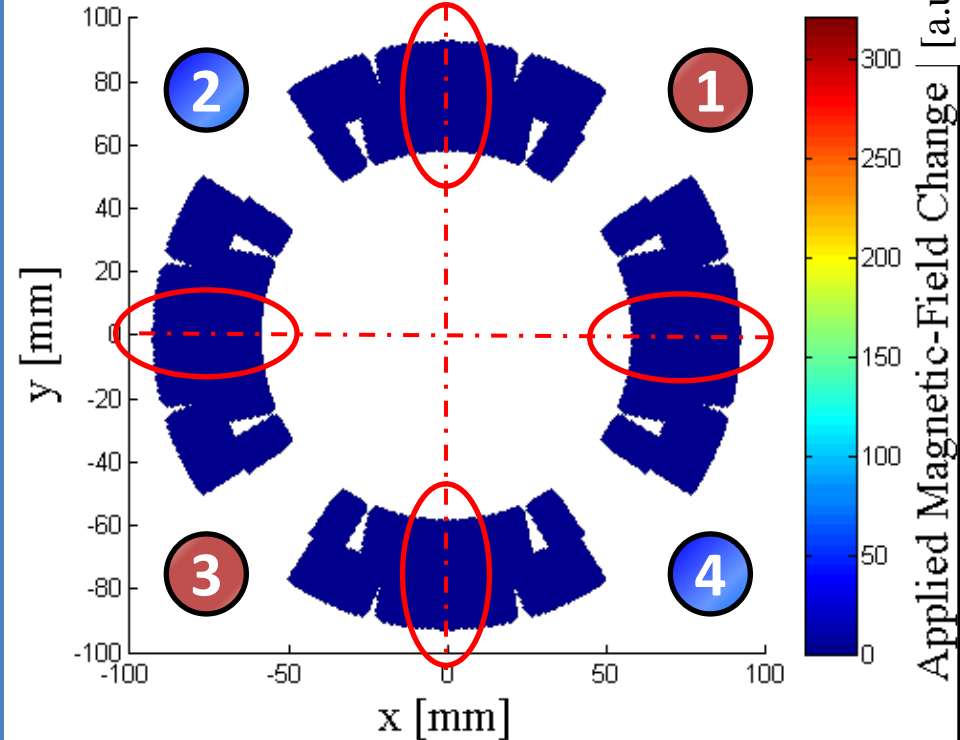
Not Optimized

$t=0$ ms, $I_1=14600$ A, $I_2=14600$



Optimized

$t=0$ ms, $I_1=14600$ A, $I_2=14600$



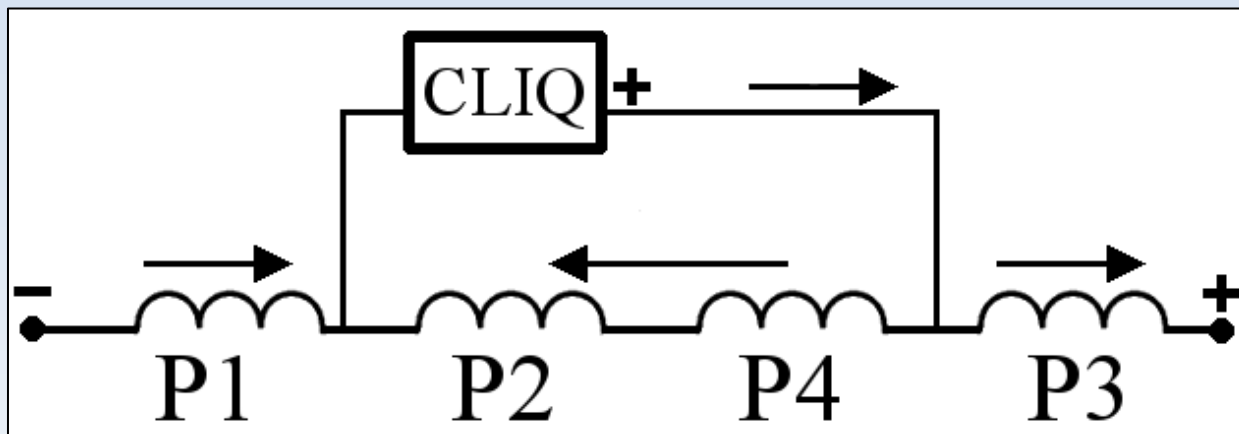
Golden rule for optimizing any CLIQ discharge circuit

Introduce opposite current change in coils which are physically adjacent

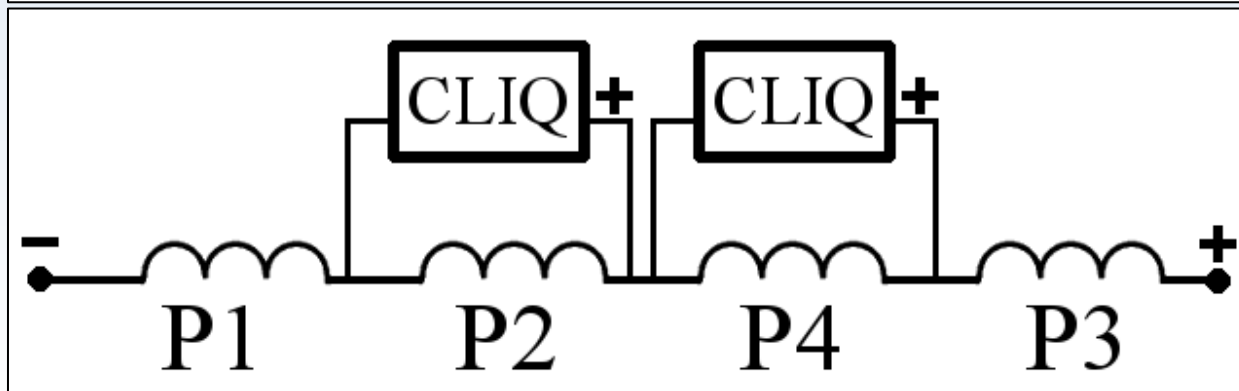
Multi-CLIQ

Further decreasing the impedance of the circuit can be reduced by **subdividing** the electrical circuit into $2 \times N_C$ elements, effectively **in parallel** when CLIQ is triggered.

$$\frac{P_{IF}}{vol} \propto \left(\frac{dI}{dt} \right)^2 \propto \left(\frac{U_0}{l_m} \cdot \frac{N_C}{L_{1-CLIQ}} \right)^2$$



1-CLIQ



2-CLIQ

Protecting a Full-Scale Nb₃Sn Magnet with CLIQ

CLIQ tests on the
model magnet
(HQ02b, 1 m)

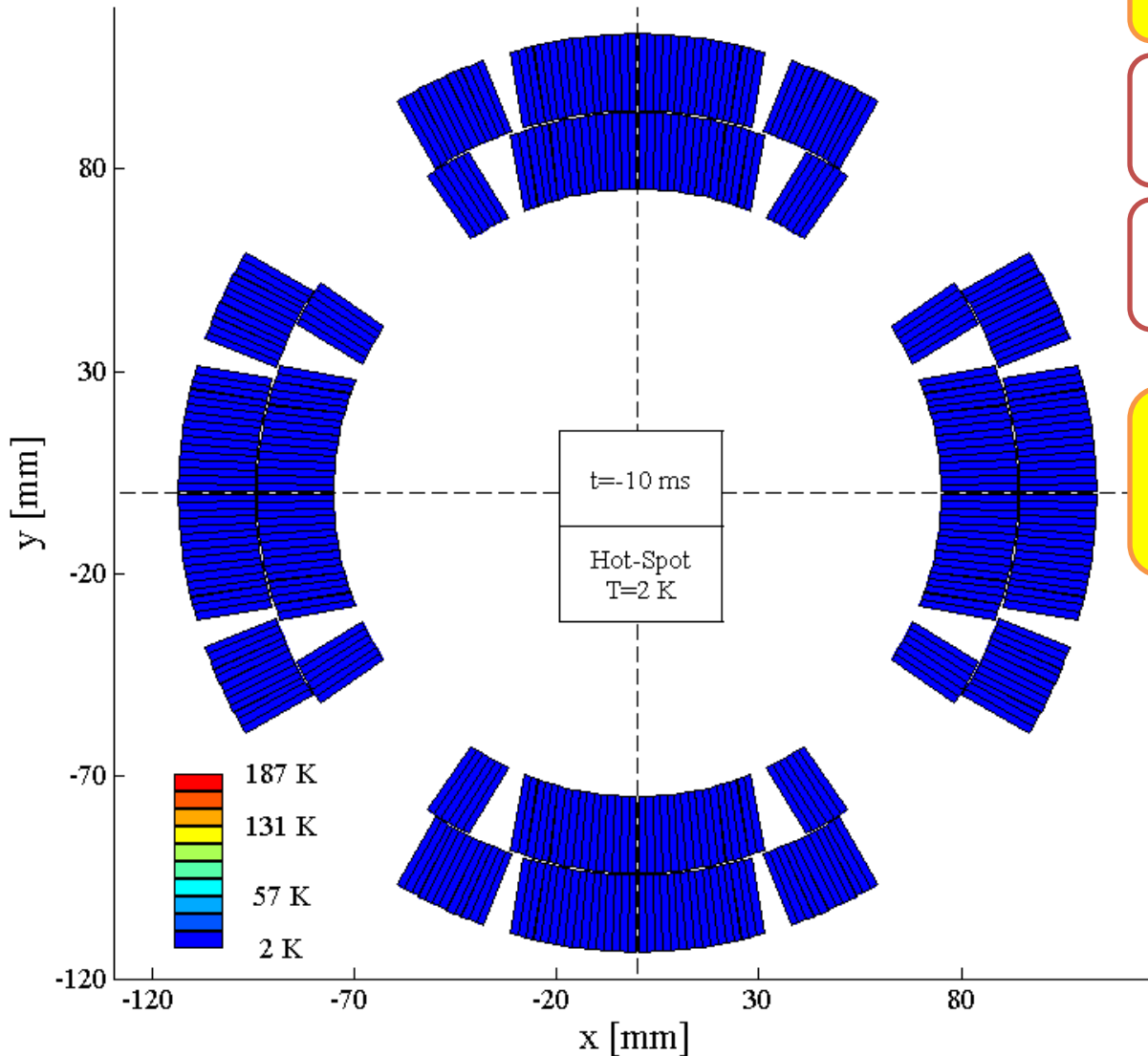
Validation of the
simulation tools

Optimization
strategy

**Simulations of the protection the
full-scale magnet (MQXF, 7 m) using CLIQ**

4 tested	1-CLIQ, 500 V	1-CLIQ, 1 kV
configurations	2-CLIQ, 500 V	2-CLIQ, 1 kV

Simulated T profile – $I_0=17.3$ kA (I_{nom}) – 2-CLIQ, $U_0=500$ V, $C=120$ mF



Very fast quench initiation

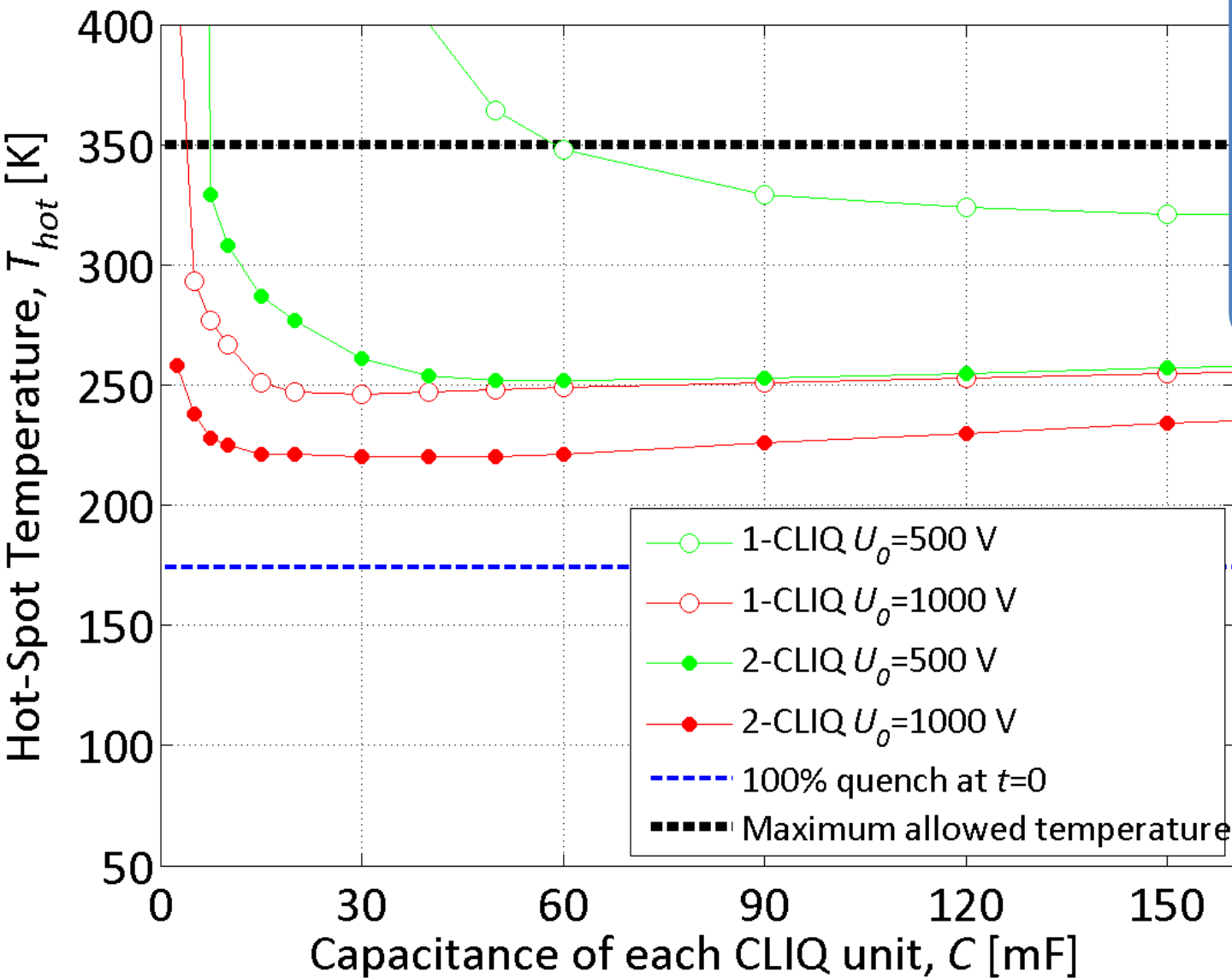
Entire inner layer quenched in **<10 ms**

90% of the magnet quenched in **<40 ms**

Homogeneous temperature distribution

Assumptions: no QH;
no EE; RRR=140;
10 ms detection time

Simulation results $- I_0 = 17.3 \text{ kA}$ (I_{nom})



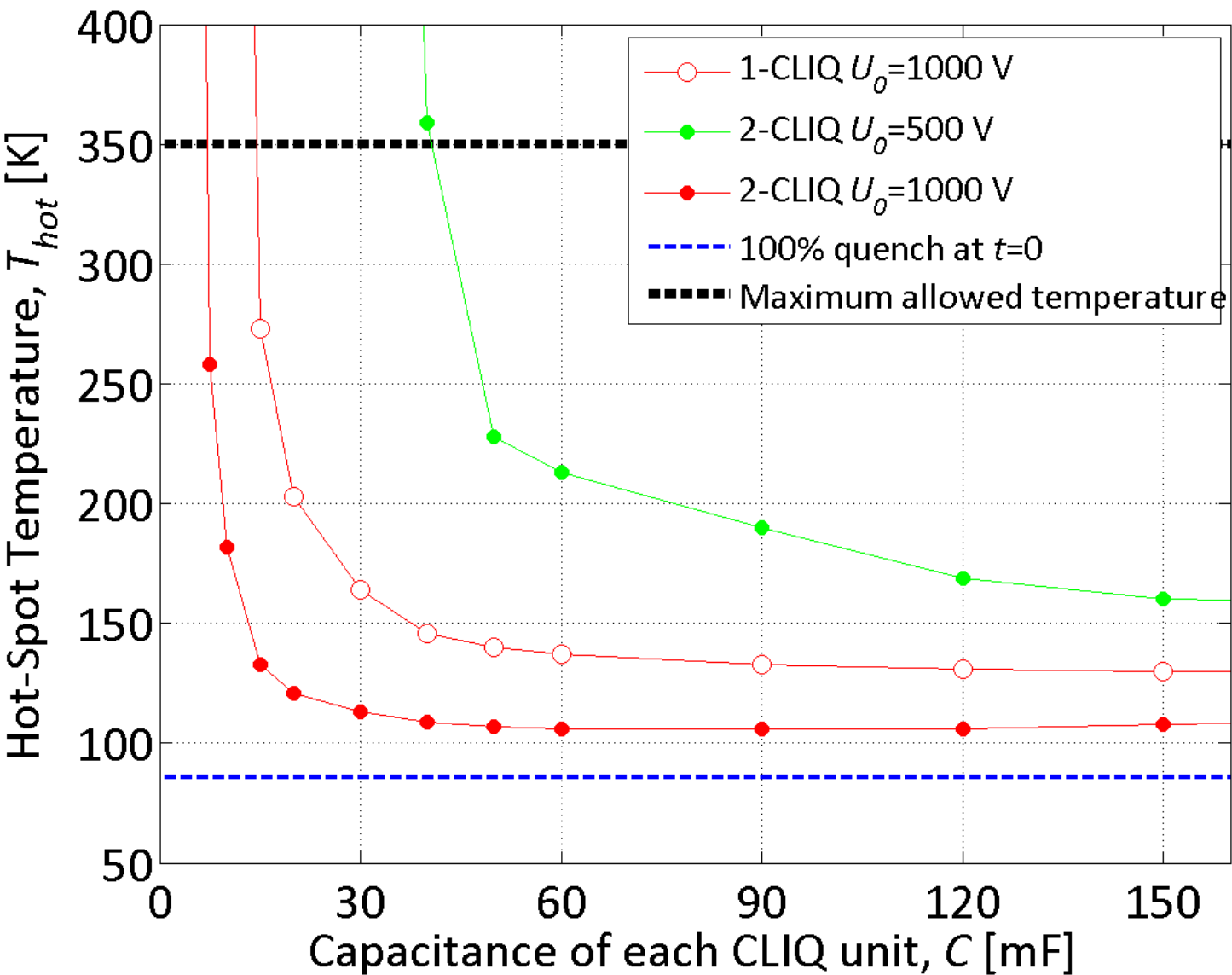
MQXF
 Magnetic Length 6.8 m
 Self-inductance 70 mH
 Nominal current 17.3 kA
 Quadrupole magnet for the LHC high luminosity upgrade (US-LARP collaboration)

For each studied configuration a minimum capacitance is needed to protect the magnet

As expected performance of 2-CLIQ-500 V similar to 1-CLIQ-1 kV

Assumptions: no QH; no EE; RRR=140; 10 ms detection time

Simulation results – $I_0 = 9 \text{ kA}$ ($\sim 50\% I_{\text{nom}}$)



1-CLIQ-500 V is not sufficient to protect the full-length magnet

Both 2-CLIQ-500 V and 1-CLIQ-1 kV are **valid protection solutions** for $C > 50 \text{ mF}$

Assumptions: no QH; no EE; RRR=140; 10 ms detection time

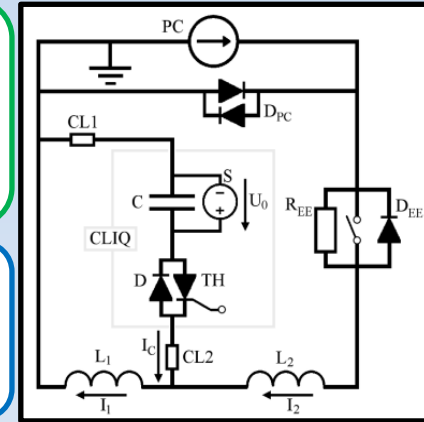
Protecting a Full-Scale Nb₃Sn Magnet with CLIQ -Conclusion

CLIQ

CLIQ is a very good solution for the protection of superconducting magnets: efficient, low hot-spot temperature, robust, easy to repair, less failures

Tests

First CLIQ tests on the **Nb₃Sn** model magnet for the LHC high luminosity upgrade very successful



Optimization

Optimization strategy for **full-scale** magnets clearly outlined

1. Select **optimum CLIQ discharge circuit**
- 2a. Increase CLIQ **charging voltage**
- 2b. **Multiple** CLIQ units (Multi-CLIQ)
3. Increase CLIQ **capacitance**

$$\frac{P_{IF}}{vol} \propto \left(\frac{dI}{dt} \right)^2 \propto \left(\frac{U_0}{l_m} \cdot \frac{N_C}{L_{1-CLIQ}} \right)^2$$

Simulations show that **CLIQ is a valid solution** for the protection of the full-scale quadrupole magnet for the LHC high luminosity upgrade (MQXF)

Next CLIQ test campaigns: 15 m LHC Main Dipole, Nb₃Sn quadrupole for LHC High-Luminosity Upgrade, LHC spare quadrupoles, 11 T dipole, Nb₃Sn solenoids from Oxford Instruments, ...?

QUESTIONS?

References

EU Patent EP13174323.9, June 2013.

E. Ravaioli et al., MT23, 2013.

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E. Ravaioli et al., CHATS-AS, 2013.

E. Ravaioli et al., Cryogenics, 2014.

E. Ravaioli et al., SuST, 2014.

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E. Ravaioli et al., ASC, 2014.

Ask me the
CLIQ Recipe!

Emmanuele.Ravaioli@cern.ch

Development of a CLIQ-based protection system for the full-scale quadrupole magnet for the LHC high luminosity upgrade

Preliminary Analysis and Simulations

CLIQ tests on the model magnet (HQ02b)

Validation of the simulation tools and further CLIQ optimization

Simulation of CLIQ-based protection the full-scale magnet (MQXF)

CLIQ tests on the model magnet (HQ03) with improved CLIQ config

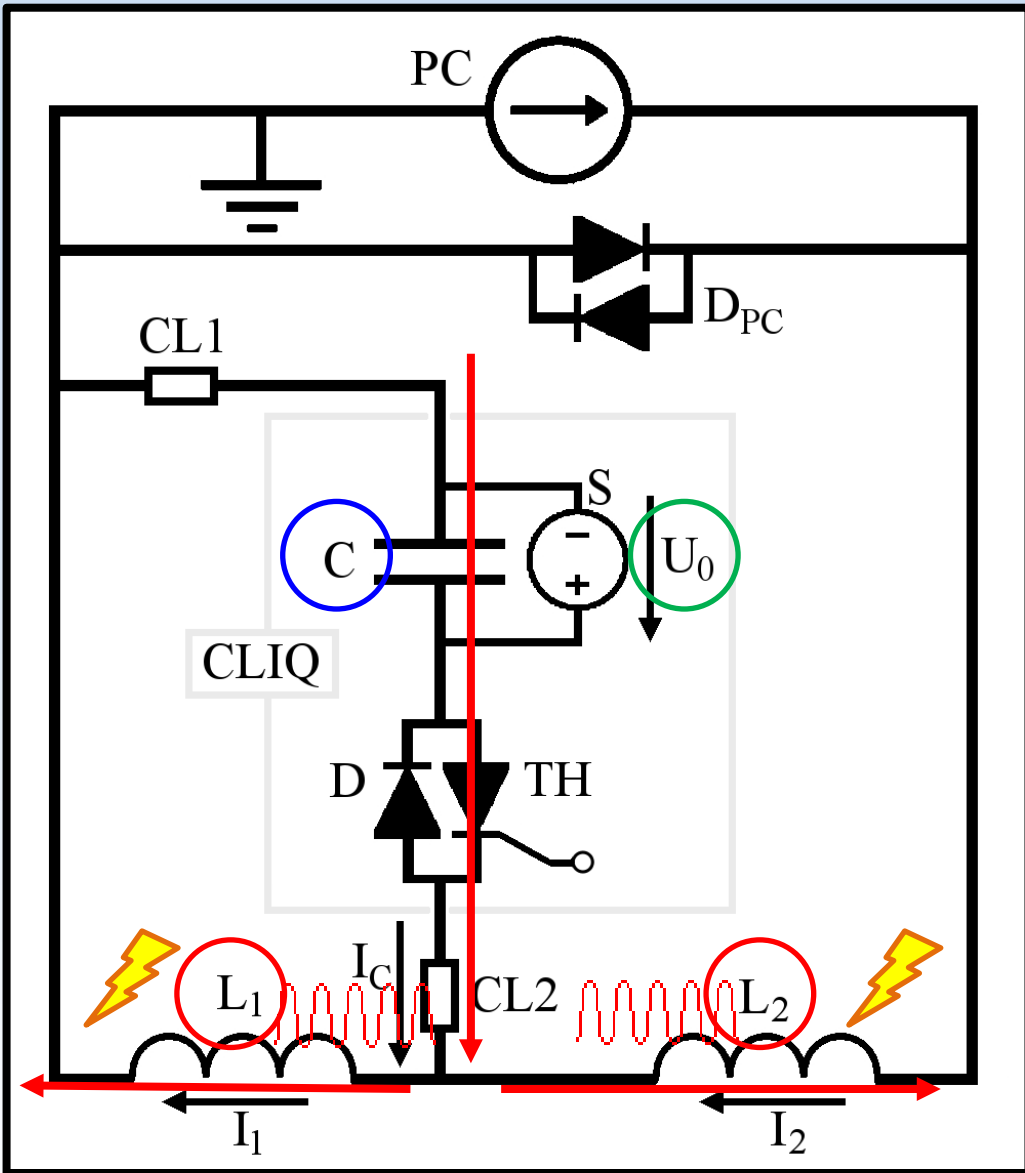
Design of a CLIQ-based protection for MQXF (possible integration with Quench Heaters or Energy Extraction)

Model magnet (HQ02b)
Nb₃Sn Quadrupole Magnet
Magnetic Length 0.8 m
Self-inductance 6.4 mH
Nominal current 14.6 kA

Full-length magnet (MQXF)
Nb₃Sn Quadrupole Magnet
Magnetic Length 6.8 m
Self-inductance 70 mH
Nominal current 17.3 kA

TODAY

CLIQ – Coupling-Loss Induced Quench



Current Change

$$I_C(t) \approx -U_0 \sqrt{\frac{C}{L_{eq}}} \cdot \sin\left(\frac{t}{\sqrt{L_{eq}C}}\right)$$

Magnetic Field Change

$$I_{C,peak} \propto U_0 \cdot \sqrt{\frac{C}{L_{eq}}}$$

$$\frac{dI_C(t)}{dt} \approx \frac{U_0}{L_{eq}} \cdot \cos\left(\frac{t}{\sqrt{L_{eq}C}}\right)$$

Coupling-Losses (Heat)

$$\frac{dB_t(t)}{dt} = f_m \frac{dI_C(t)}{dt} \left[1 - \exp\left(-\frac{t}{\tau_{IF}}\right)\right]$$

$$\frac{P_{IF}}{vol} = \beta_{IF} \left[\frac{dB_t(t)}{dt}\right]^2 \propto \left(\frac{U_0}{L_{eq}}\right)^2$$

Temperature Rise

$$\tau_{IF} = \frac{\mu_0}{2} \left(\frac{l_p}{2\pi}\right)^2 \frac{1}{\rho_{eff}(B)}$$

QUENCH

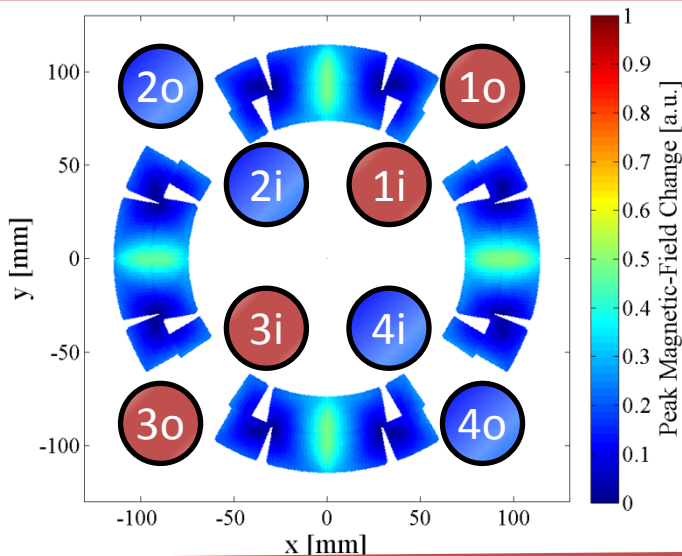
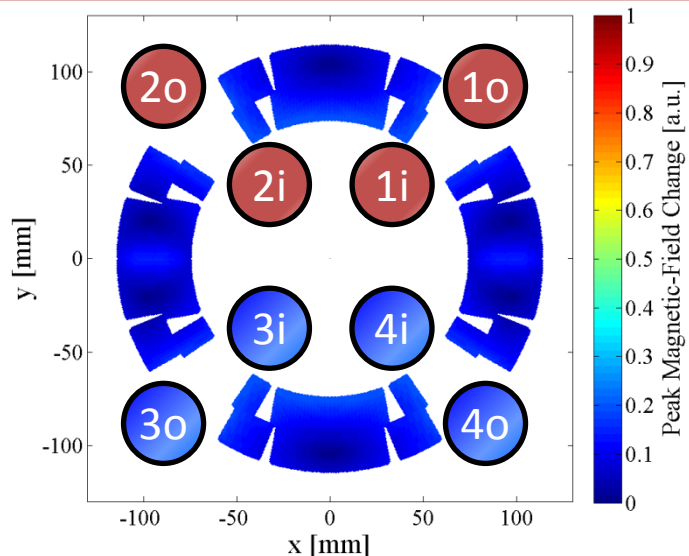
$$\beta_{IF} = \left(\frac{l_p}{2\pi}\right)^2 \frac{1}{\rho_{eff}(B)}$$

Principle: When subjected to a magnetic field change, **coupling losses** occur in superconducting wires and cables. These losses are **heat** generated directly in the superconductor to quench!

With CLIQ connections at the joint between inner/outer layers

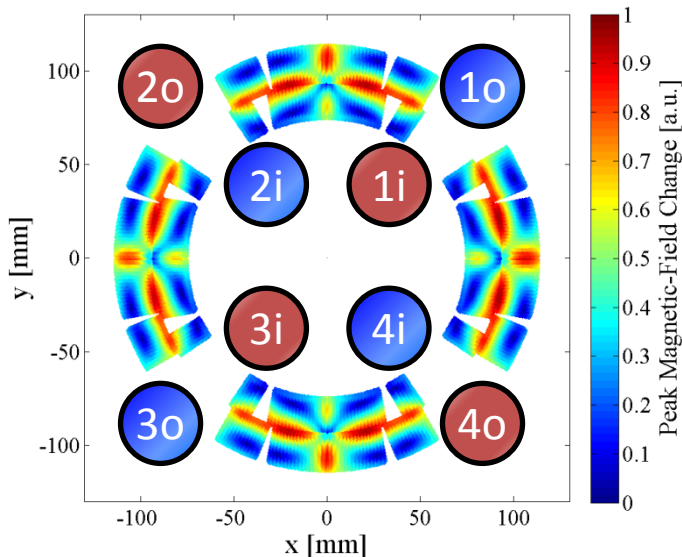
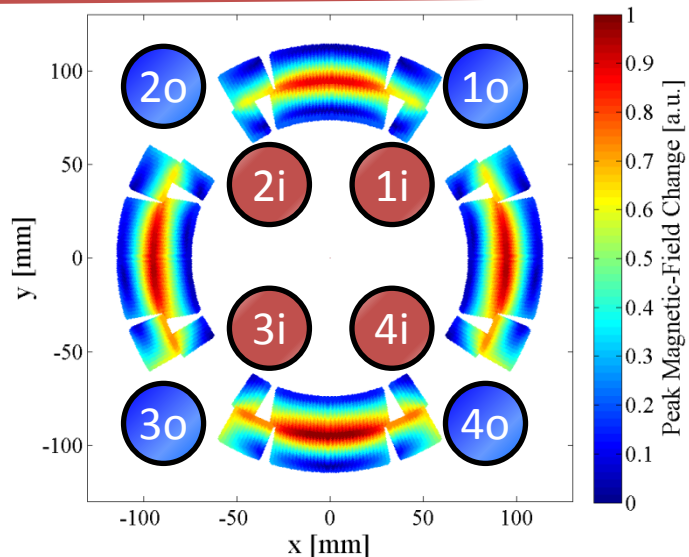
Golden rule for optimizing any CLIQ discharge circuit

Introduce opposite current change in coils which are physically adjacent



Existing magnets

Configurations **easy** to implement on most existing magnets



Future magnets

With connections between **in/out layers**

CLIQ – Advantages & Drawbacks (compared to Quench Heaters)

Advantages

- Heat generated directly in the superconductor to quench (not relying on thermal diffusion)
- Robust electrical design, easier implementation and repair
- Faster quench initiation
 - More homogeneous temperature distribution
 - Lower hot-spot temperature
- Lower failure risk
- Easy repair solution for a magnet with damaged quench heaters
- For the same price and size of conventional quench heater systems
- Possible to avoid the installation of quench heaters

Drawbacks

- Additional current lead(s) connected to the magnet (pulse current for <100 ms)
- High voltage introduced in the circuit
 - If applied to a magnet which is part of a chain, additional studies have to be carried out (how to implement, transient waves, avoid resonances, etc)
 - Integration with an energy-extraction system is possible but it needs to be carefully studied
- Additional mechanical stresses due to the introduced current need to be analyzed

Protecting long magnets with CLIQ – Issues & Solutions

Issues	Possible Solutions
Integration with an energy-extraction system: Avoid too high voltage to ground due to voltage superposition	Delaying the triggering of the energy-extraction system to wait the damping of the CLIQ oscillation (30-100 ms?)
If “1 CLIQ” solution is chosen, high voltage to ground (up to 1 kV?)	Increasing insulation thickness would not decrease the CLIQ performance
If “Multi-CLIQ” solution is chosen, three current leads connected to the magnet (pulsed current for $t < 100$ ms)	
Redundancy	More then one trigger thyristor in parallel (2?) More than one CLIQ unit connected in parallel (2?)
Use of CLIQ to protect a magnet which is part of a chain or of a nested circuit	Use by-pass elements (pair of diodes or parallel resistor) to allow introducing an AC current on a single magnet of the chain
Integration with Quench Heaters	No problem

CLIQ – How is the energy deposited? with Inter-Filament Coupling Loss

The current introduced in the magnet coil generates a change in the local magnetic field.

When a superconductor is subjected to an applied magnetic-field change, an induced magnetic field is generated which opposes to the applied field.

For fast transients, the actual magnetic field does not change much, because the applied and induced magnetic field almost cancel out.

The presence of the induced field generates currents between superconducting filaments and between superconducting strands. These currents flow through the copper matrix of the conductor, thus they generate loss (=heat) inside the cable.

For typical ranges of magnet inductance (5-100 mH) and CLIQ capacitance (5-50 mF), the range of the **CLIQ oscillation period is 10-100 ms** (frequency range 10-100 Hz)

Inter-Filament Coupling Loss

For typical filament twist-pitch and Cu transverse resistivity, time constant in the order of tens of ms

High energy deposition with CLIQ discharge

Inter-Strand Coupling Loss

For typical strand twist-pitch and cross-contact resistance, time constant in the order of hundreds of ms / seconds

Limited energy deposition with CLIQ discharge

Magnetization Loss

Very limited change in the local magnetic field, hysteresis loops are small

Limited energy deposition with CLIQ discharge

Optimum CLIQ discharge configuration – 1-CLIQ

	P1	P2	P3	P4
P1	L _s	M _c	M _f	M _c
P2	M _c	L _s	M _c	M _f
P3	M _f	M _c	L _s	M _c
P4	M _c	M _f	M _c	L _s

Self and Mutual inductance of the 4 poles of a quadrupole magnet

L_s Self inductance of one pole

M_c Mutual ind between close poles

M_f Mutual ind between front poles

$$L_{mag} = 4L_s + 8M_c + 4M_f$$

8.4 mH

MQXC2

L_s > M_c

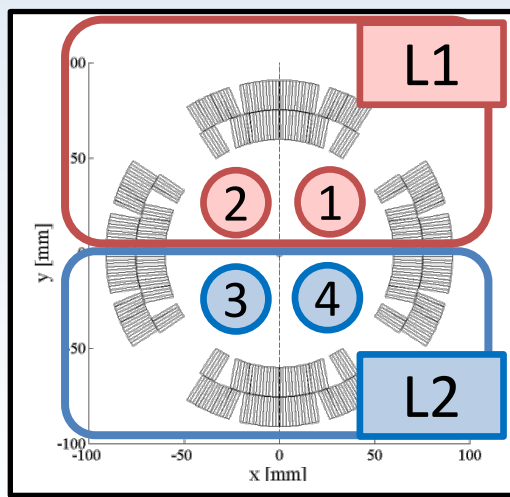
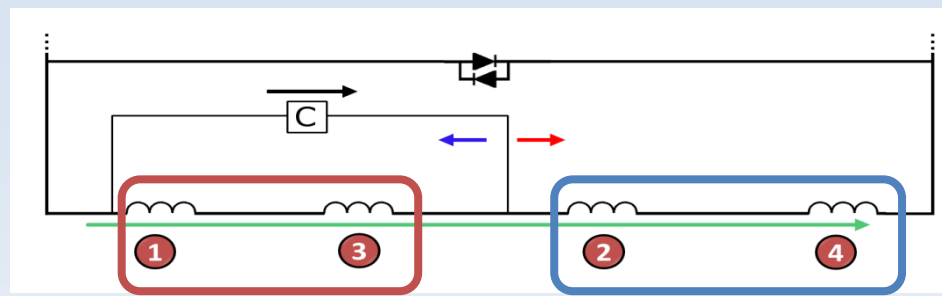
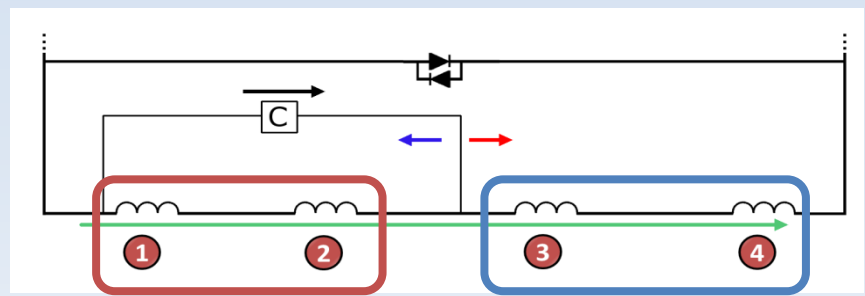
+1.6 mH

M_c > 0

+0.4 mH

M_f < 0

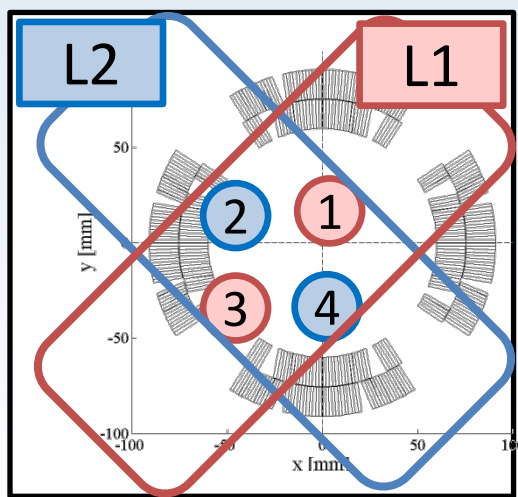
-0.2 mH



P12-P34

$$L_{eq} = L_s - M_f$$

MQXC2
1.8 mH



P13-P24

$$L_{eq} = L_s - 2M_c + M_f$$

MQXC2
0.6 mH
3 times smaller

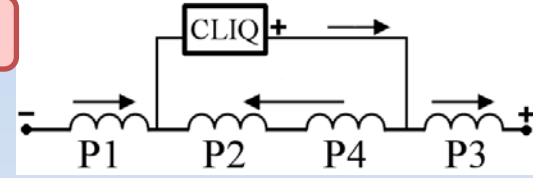
Multi-CLIQ – 2 CLIQ units, 4 CLIQ units, N_c CLIQ units...

L_{eq} can be reduced by further subdividing the electrical circuit into N_E elements, effectively in parallel when CLIQ is triggered.

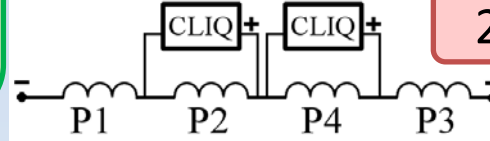
They can be **magnets** in a chain, **poles** of a magnet, or inner/outer **layers** of each pole.

Peak power deposition
 proportional to N_c^2

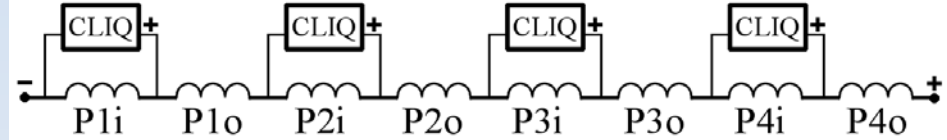
1-CLIQ



2-CLIQ

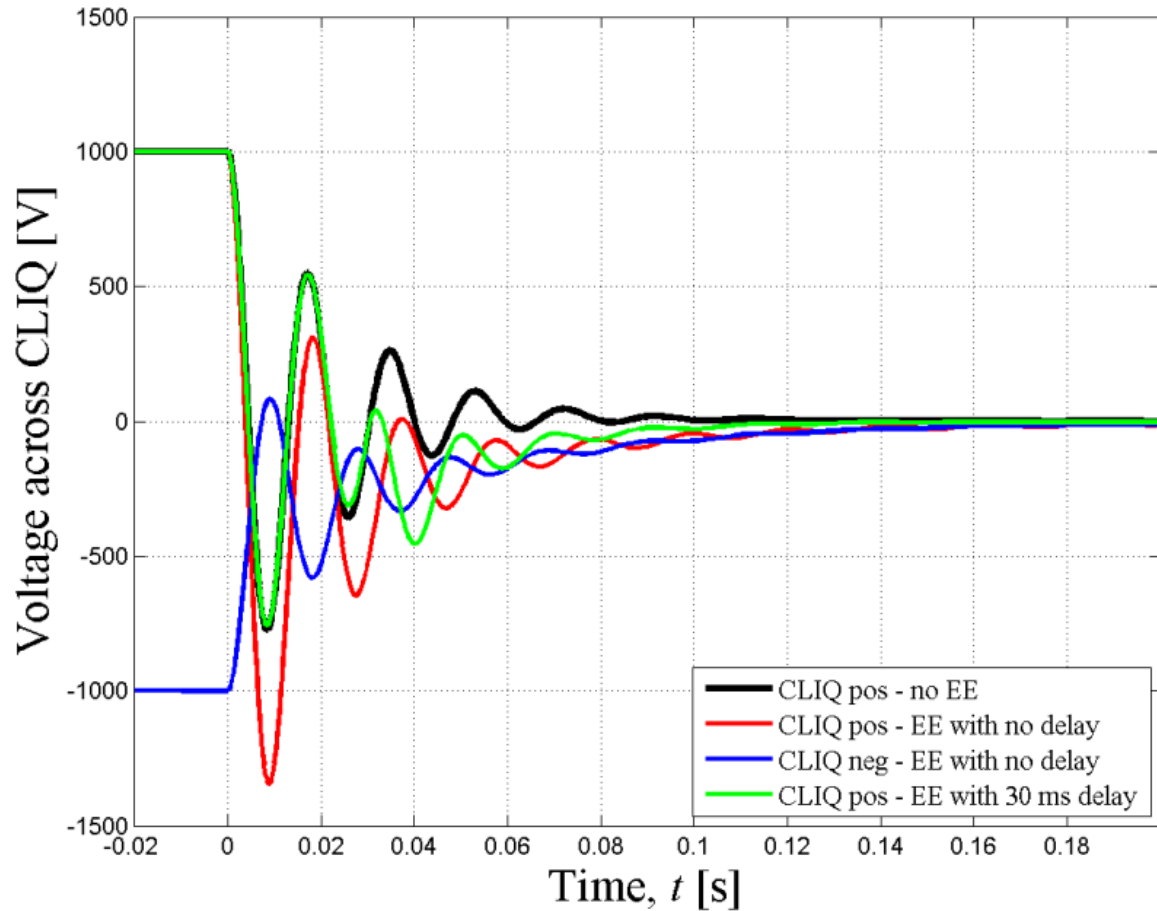
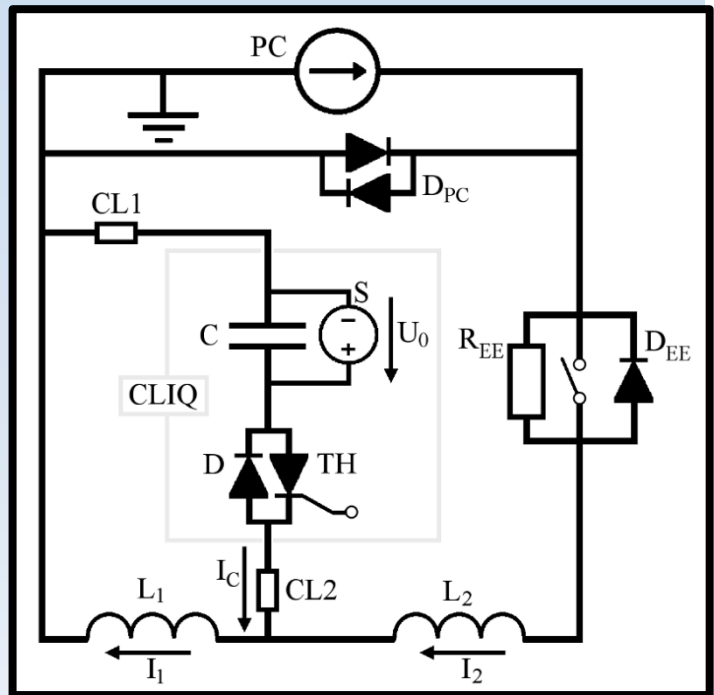


4-CLIQ



Parameter	1 CLIQ	1 CLIQ $2xU_0$	2 CLIQ	4 CLIQ	N_c CLIQ
Number of elements, N_E	2	2	4	8	$2 N_c$
Equivalent inductance, L_{eq}	L_{eq}	=	$\div 4$	$\div 16$	$\div N_c^2$
Total capacitance, C_{eq}	C	=	$\times 2$	$\times 4$	$\times N_c$
Charging voltage, U_0	U_0	$\times 2$	=	=	=
Peak current change, di/dt	$U_0/L_{eq}/N_E$	$\times 2$	$\times 2$	$\times 4$	$\times N_c$
Peak deposited loss	$\infty(U_0/L_{eq}/N_E)^2$	$\times 4$	$\times 4$	$\times 16$	$\times N_c^2$
Peak AC current, I	$\infty U_0 * \text{sqrt}(C_{eq}/L_{eq})/N_E$	$\times 2$	$\times 2^{0.5}$	$\times 2$	$\times N_c^{0.5}$
Frequency, f	$1/2/\pi/\text{sqrt}(L_{eq} * C_{eq})$	=	$\times 2^{0.5}$	$\times 2$	$\times N_c^{0.5}$

Why do we need to delay the triggering of the extraction-system?



Avoid interference between CLIQ and EE system

- Avoid superposition of voltage across CLIQ and across EE resulting in voltage too high
- Avoid reducing CLIQ performance

MQXC2

CLIQ protects the magnet at any current level

