



Body scanning for security: A sub-mm video camera using cryogenic detectors

- Security body scanning: demand and actuality
- Chance for cryogenic systems
- Realization of our camera
- Conclusion

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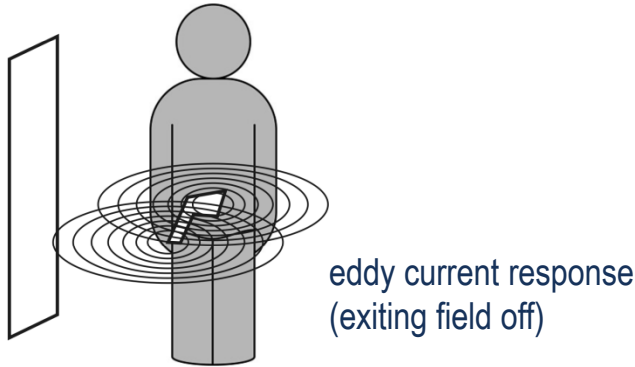
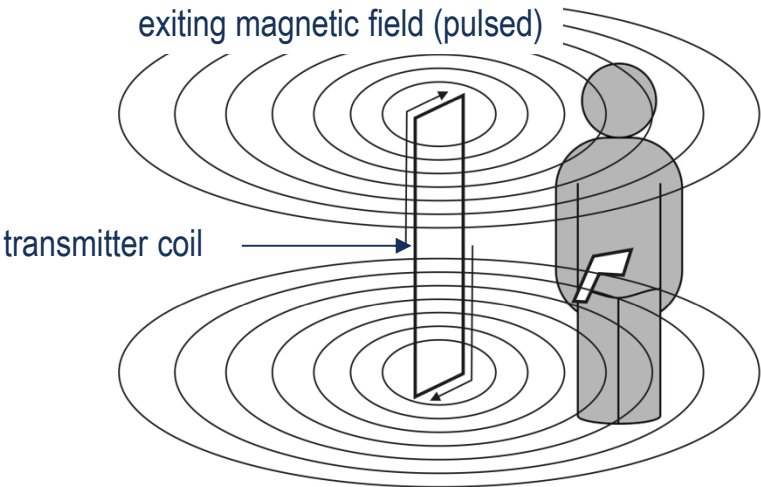
Supracon AG, Jena, Germany





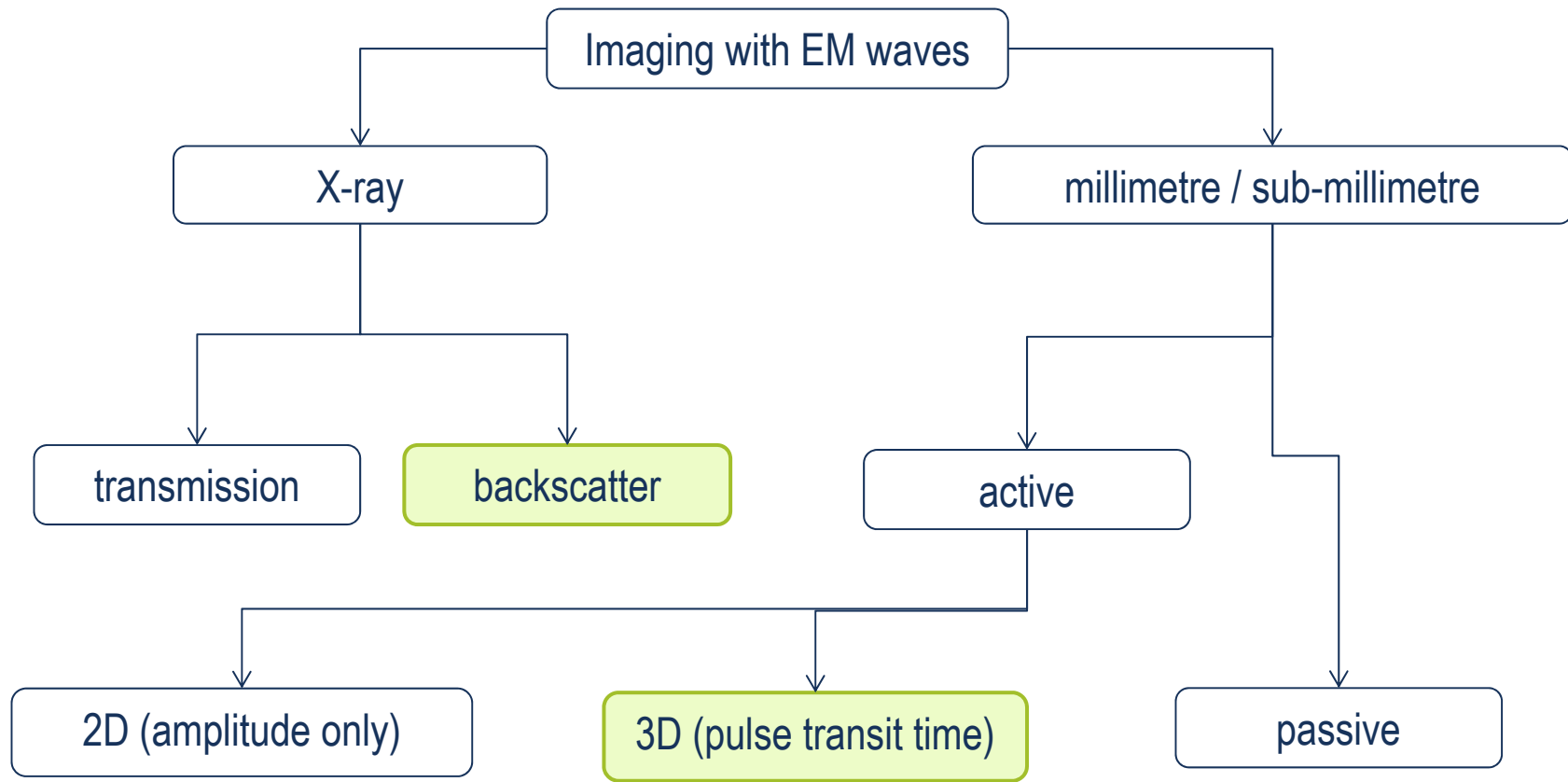
Demand for body scanning

- standard procedure walk-through metal detector: pulsed induction (coil transmits EM pulse → eddy currents created in conducting objects cause response)
- detection zones (first localization)
- statistically generated false alarm to trigger manual recheck





Variety of body scanning concepts



 mature



Prospects and limits of established solutions

What they have achieved

- full 3D image reconstruction with high spatial resolution
- high maturity level including automated object detection

What is difficult or (almost) impossible to reach:

- abandonment of artificial illumination
- operation from a distance (**stand-off** = optical imaging from a few meters) because of:
 - low spatial resolution
 - required high transmission power for real time





What is '*stand-off*' good for?

- '*stand-off*' is synonymic to '**flexible**':
 - camera for quasi-mobile deployment in different configurations,
- Perspective: reconsidering traditional security measures
 - detection of hazard **prior** to potential threat
 - **surveillance** of public events (e.g. sports)
 - check '**en passant**' (German '*Wandelgang*')
 - **temporary** protection of public buildings (embassies, election office etc.)



vision of the International Air Transport Association (IATA)



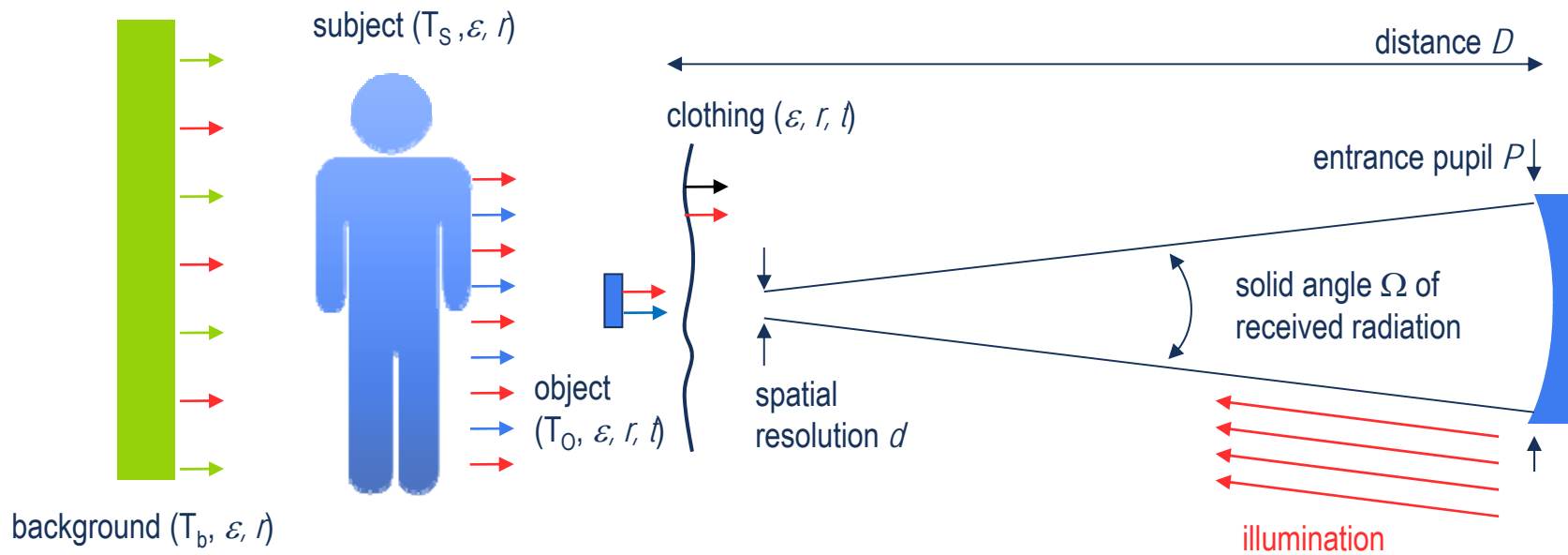
$$d = \frac{\lambda}{2n \sin \alpha}$$

Ernst Abbe, 1870

Optical (radiometric) imaging

spatial resolution $d \approx D \cdot \frac{\lambda}{P}$

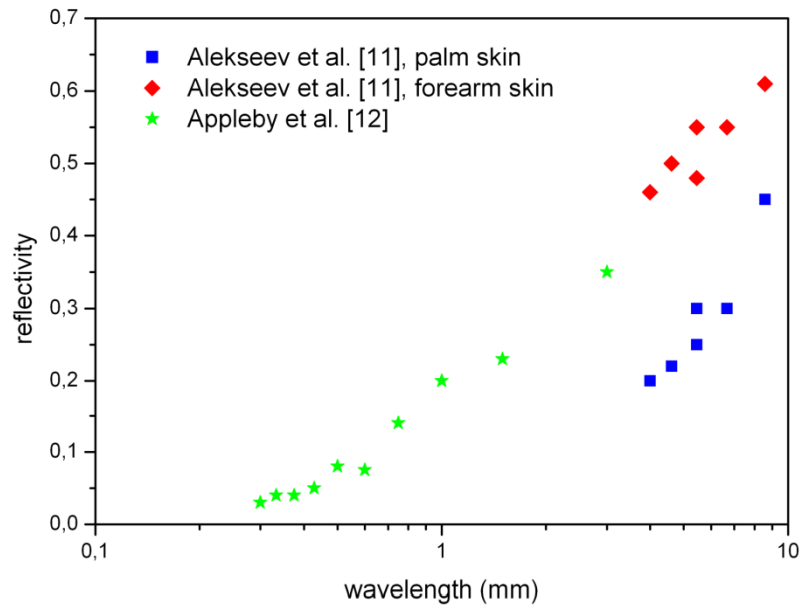
transmitted AND received signal $\sim \frac{1}{D^2} \cdot P$



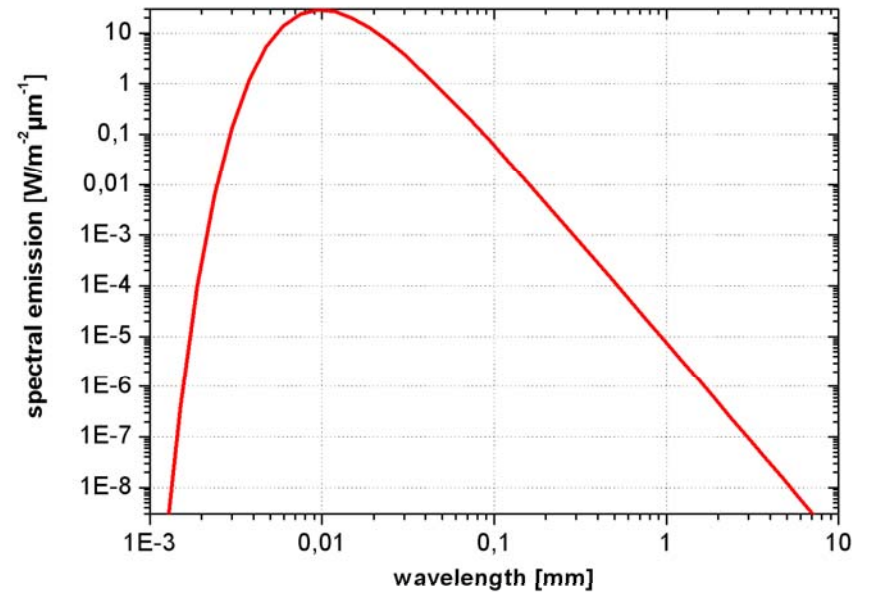


Physical (and other) limitations

reflectivity of human skin



black body emission at 310K



[11] S.I. Alekseev et al., Human Skin Permittivity Determined by Millimeter Wave Reflection Measurements, Bioelectromagnetics 28, 331-339 (2007)

[12] R. Appleby et al., Standoff Detection of Weapons and Contraband in the 100 GHz to 1 THz Region, IEEE Transactions on antennas and propagation, 55 (11), 2944 – 2956 (2007)

Note:
active illumination of persons with
EM waves beyond 300GHz
($\lambda < 1\text{mm}$) is not yet permitted by law!



Passive sub-mm imaging

Planck's equation for spectral emission of a black body with a radiating area of 1m^2

$38\mu\text{W}/\text{GHz}$ @ 310K

$35\mu\text{W}/\text{GHz}$ @ 295K

in atmospheric window $(355\pm 20)\text{GHz}$

→ $\Delta P = 120\mu\text{W}$, background power 1.4mW



chosen optical configuration:

airy disk \equiv radiating area 1.8cm^2

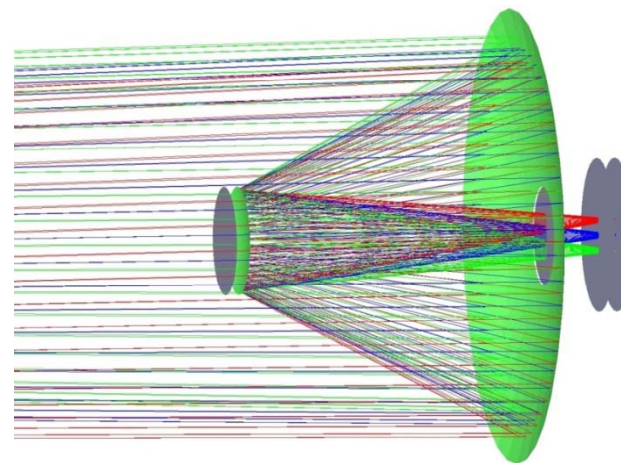
aperture \equiv receiving area $\varnothing 0.5\text{m}$ @ 10m distance ($\Omega = 0.008\text{sr}$)



received background power: 250pW

Thermal resolution 0.1K @ $\Delta T = 15\text{K}$: 150fW

simple on-axis telescope as example



\varnothing primary mirror: 0.5 m
spatial resolution (approx): 1.5 cm



That is the chance for cryogenic detectors!



Detector requirements

At the example of a 100 x 100 pixel THz image :

→ resolving 150fW in 100 millisecond integration time (10Hz frame rate):
 $NEP = 50\text{fW}/\sqrt{\text{Hz}}$

Implication: the need for a full detector array (10000 pixels)

→ resolving 156fW in a 10Hz frame, scanned with N pixels
integration time shortened by N/10000:
 $NEP = \sqrt{N} \cdot 0,5\text{fW}/\sqrt{\text{Hz}}$

reasonable concept using approved radioastronomy technology:
N = 20

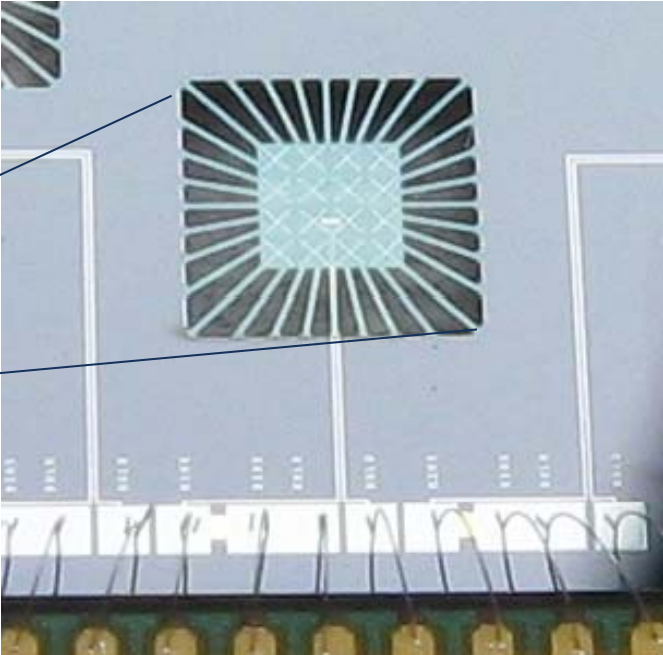
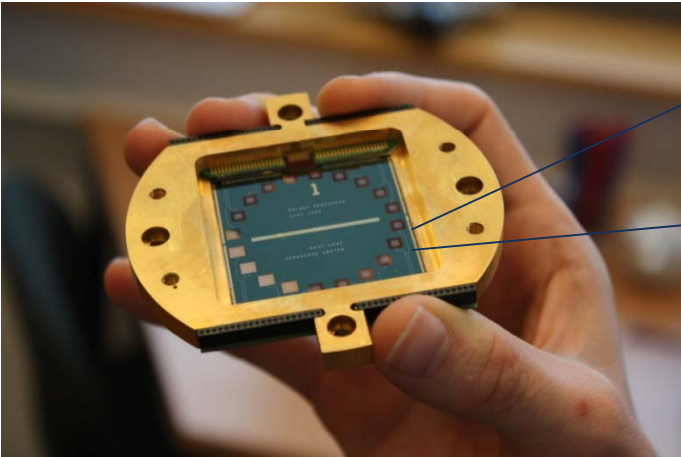
→ required NEP $2.2\text{fW}/\sqrt{\text{Hz}}$

figure of merit: NEP, defined as
resolvable power per square root of
integration bandwidth

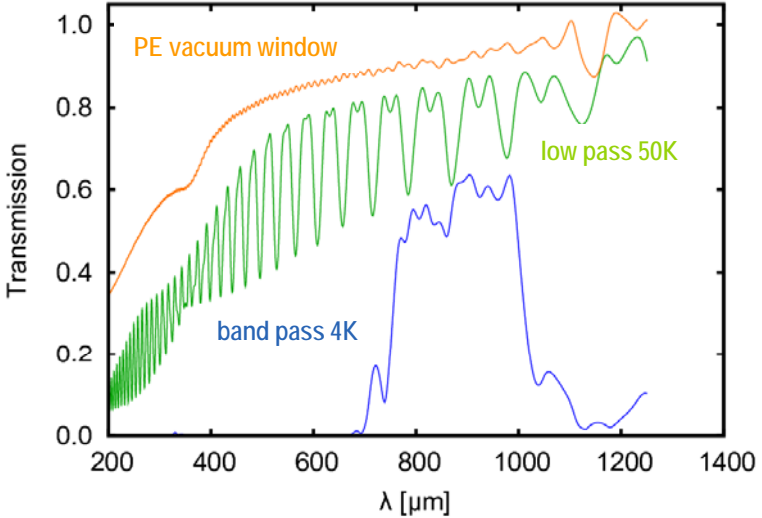
$NEP = 150\text{fW}/\sqrt{\text{Hz}} \equiv$ resolving 150fW
in 1 second integration time



Receiver



20 TES bolometers in a circular array

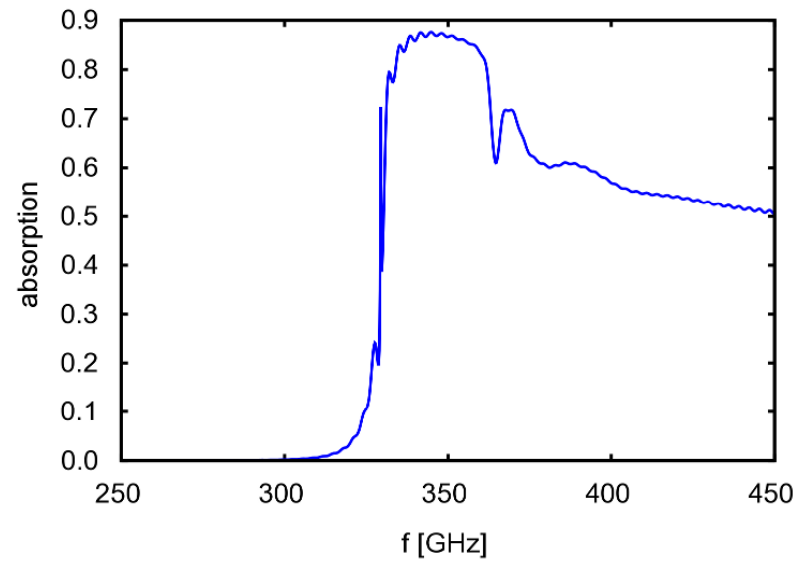
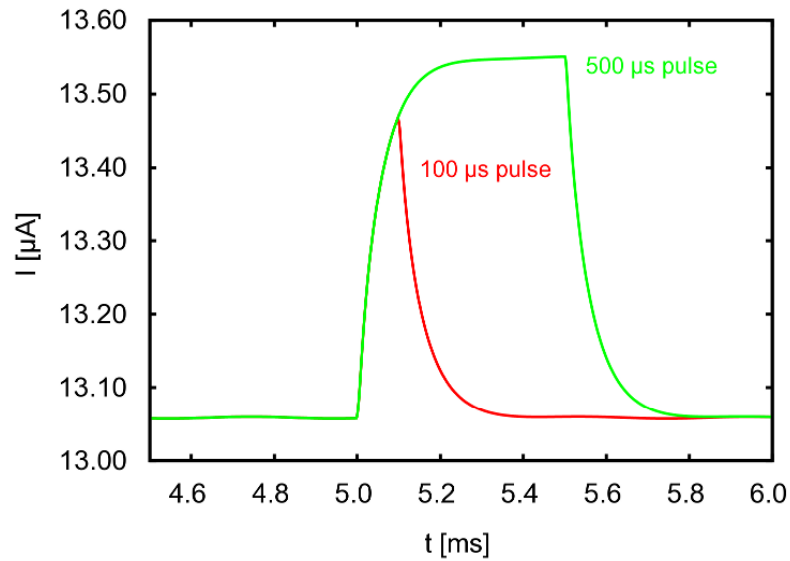
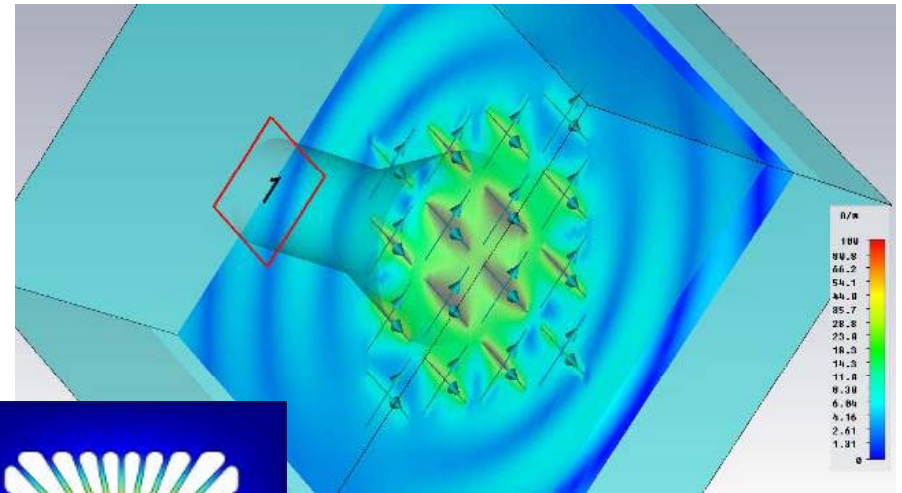


- 1 μm thick silicon nitride membrane with low thermal conductivity (1nW/K)
- absorption in an array of dipole antennas ($\lambda/2$)
- band definition by set of cryogenic filters (see poster Anika Brömel for details)



Detector optimization

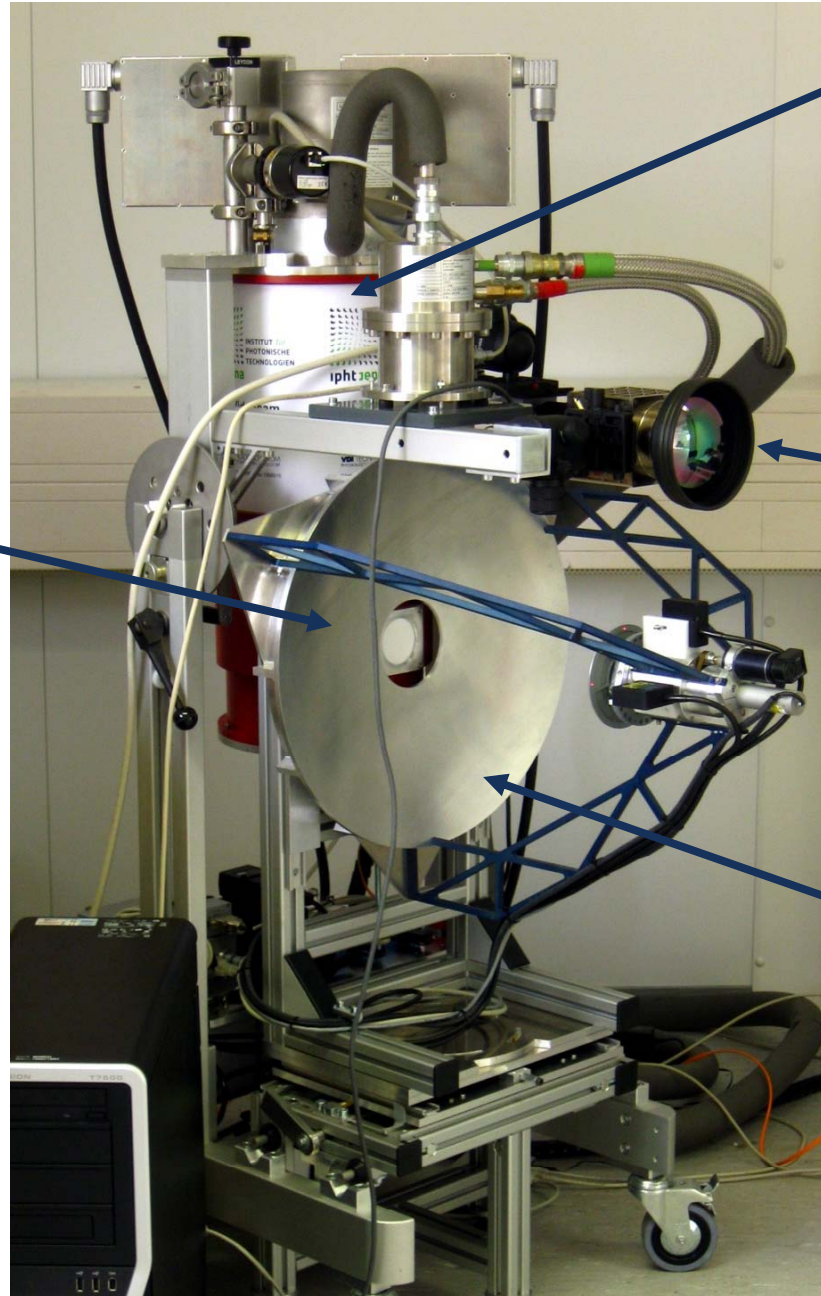
- FEM simulations (COMSOL® Multiphysics®)
- radiation, thermal properties, electrical behavior
- optimized: design, G, C
- $\tau \approx 50 \mu\text{s}$, efficiency $\approx 70 \%$





System

cryogenic receiver with temperature resolution about 0.5K at 10Hz video frame rate



cryogen free cooling system

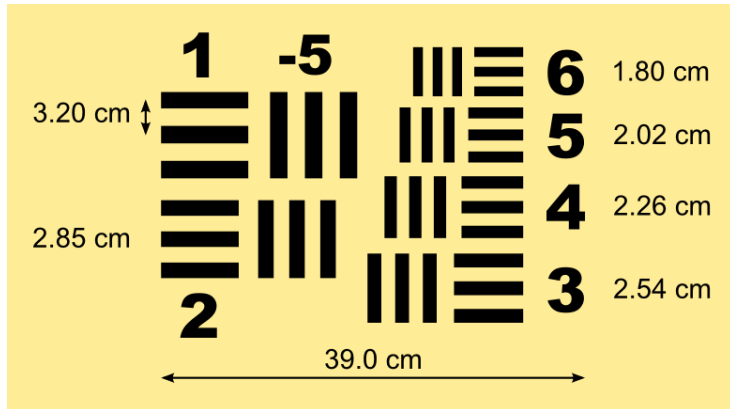
commercial module for simultaneous recording of visible and IR-video

reflecting optics for 7 to 10 meter distance (adjustable), spatial resolution 1.5cm

For details see E. Heinz et al., Journal of Infrared, Millimetre, and Terahertz Waves 2010



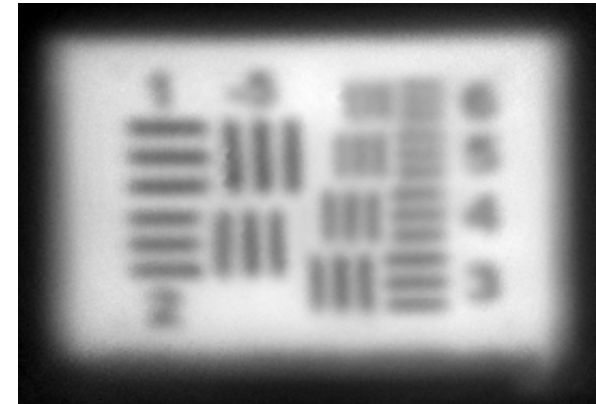
Achieved spatial resolution



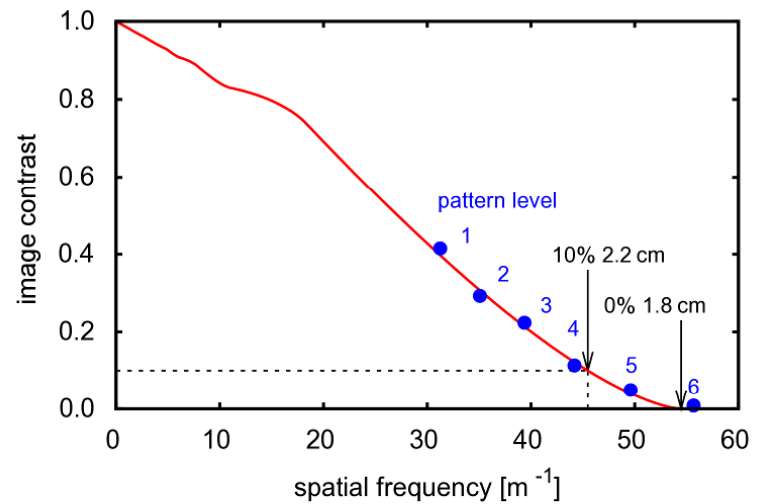
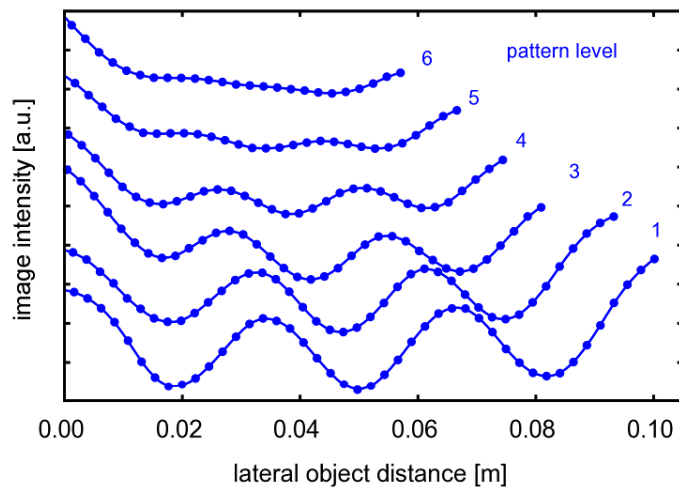
spatial cut-off frequency

$$s = D / \lambda d$$

Kottler/Perrin,
J.Opt.Soc.Am
56, 377 (1966)



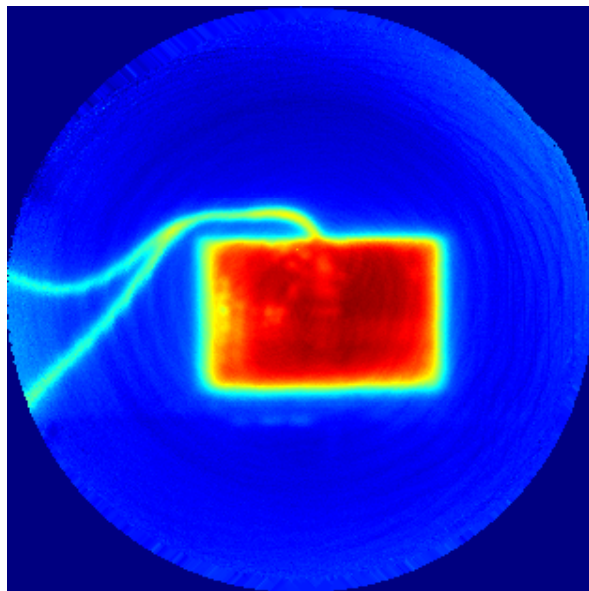
9 m distance, 20 s integration



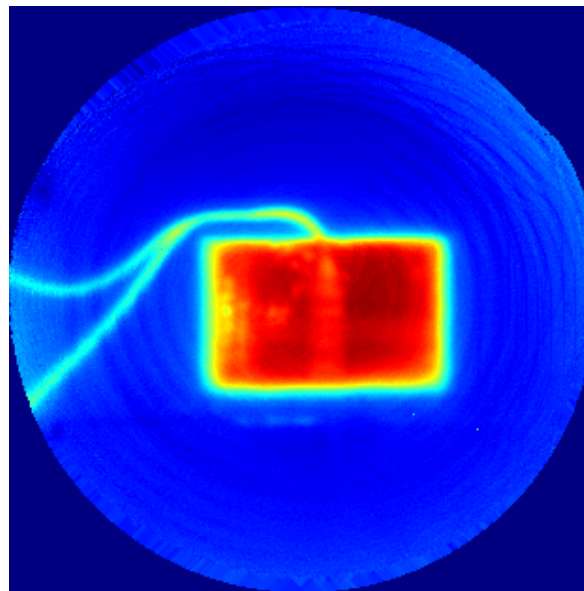


Achieved thermal resolution

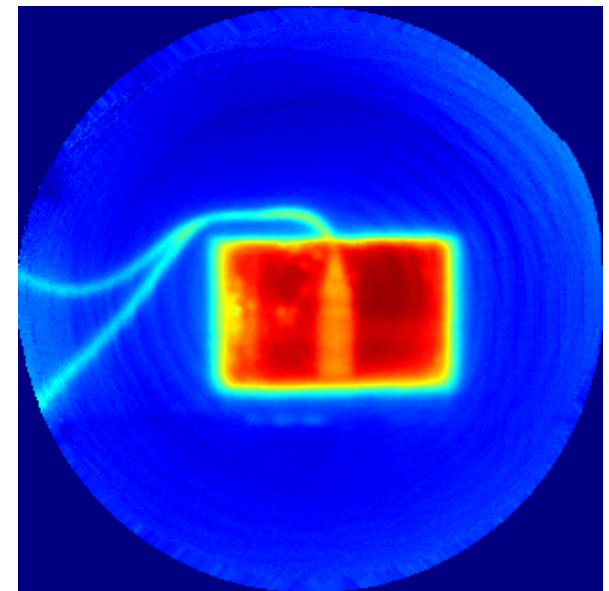
temperature resolution – experiment
background $\approx 24\text{ }^{\circ}\text{C}$, panel $35.1\text{ }^{\circ}\text{C}$,
temperature resolution is “confusion limited” (limited by spatial noise)



$\Delta T = 0.1\text{ K}$



$\Delta T = 1\text{ K}$

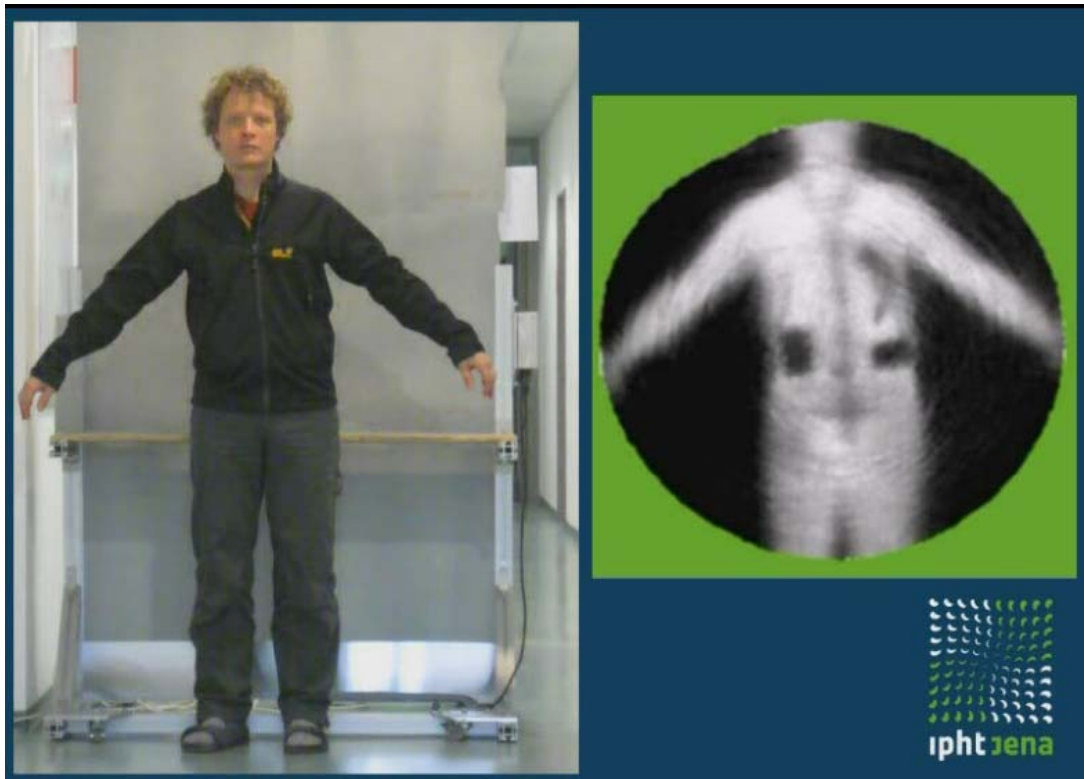


$\Delta T = 3\text{ K}$

Conclusion

1. The concept of near-field mm-wave imaging is mature. Cryogenic detectors can hardly compete in that field.
2. A passive sub-mm wave camera is the most effective solution for stand-off application scenarios. Cryogenic detectors are able to meet the demands of such a system
3. Such systems can answer a variety of application scenarios – so future systems should be as flexible as possible

Thanks for the attention and to the team



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