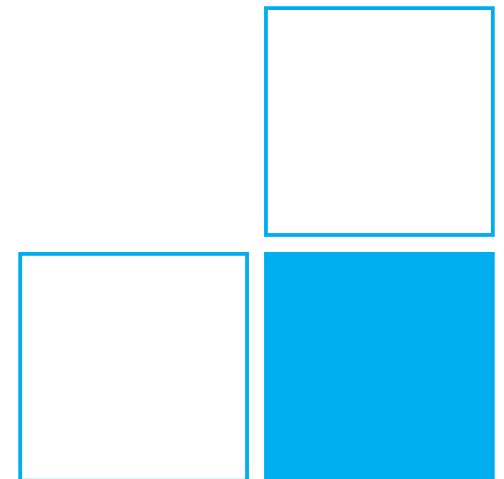


Thermometry at low temperature

Alexander Kirste

Kryo 2014, Berlin, 21 September 2014



Outline

- Thermometer types, properties
- Thermal contact

- PLTS-2000, dissemination of the kelvin
- ^3He melting curve thermometer (MCT)
- Coulomb blockade thermometer (CBT)
- Nuclear orientation thermometer

- Noise thermometers
 - Josephson junction noise thermometer (JNT)
 - Current sensing noise thermometer (CSNT)
 - Magnetic field fluctuation thermometer (MFFT)

- Conclusion

Thermometer Types

Thermometer function: $m = f(T, x_1, x_2, \dots)$ T - temperature
 x_i - parameter i

Primary thermometer:

- functional dependence $f(\dots)$ is known
- all other parameters x_i are known
(might be determined without knowing T)

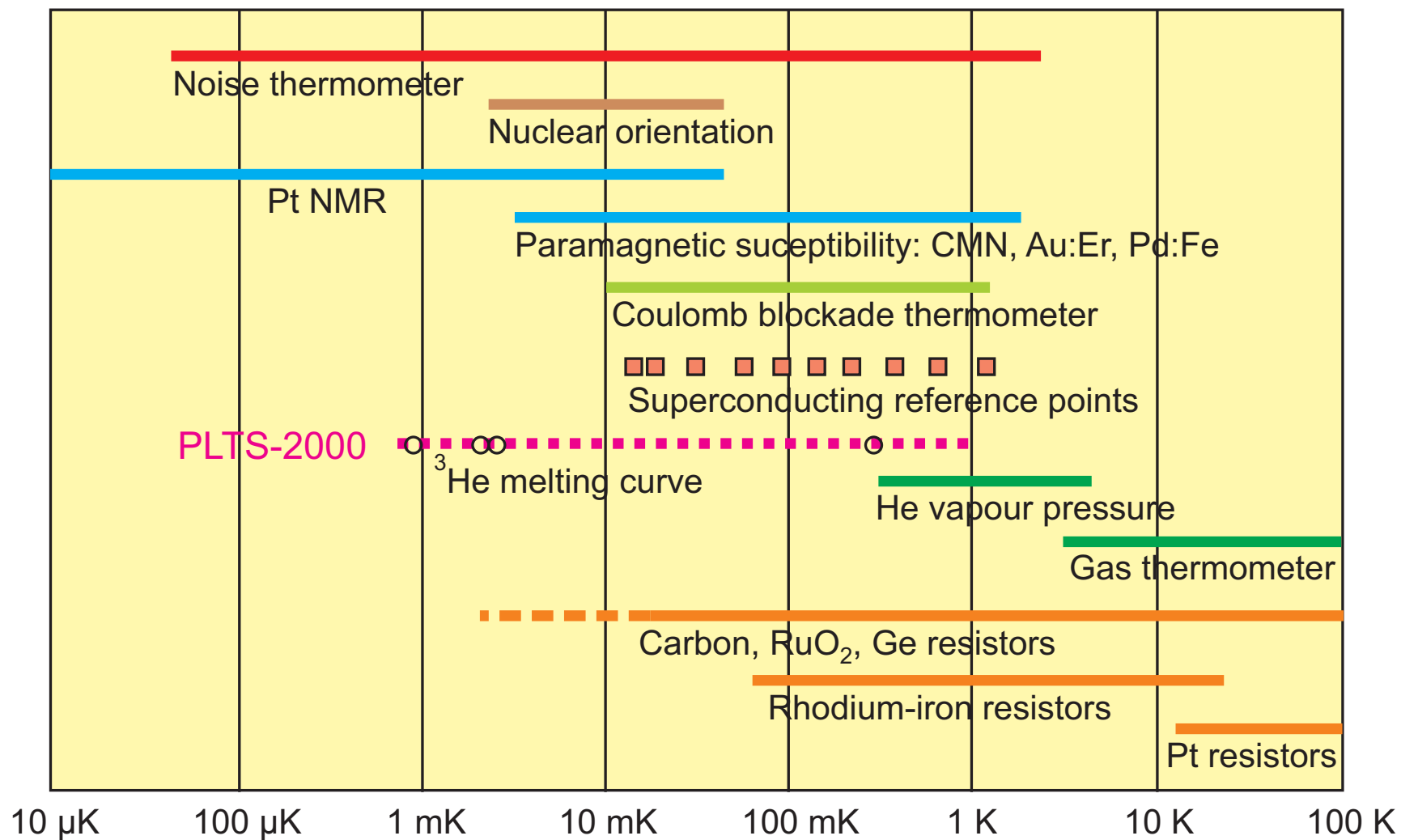
⇒ can be used without calibration

Secondary thermometer:

- **first kind:** functional dependence $f(\dots)$ is known,
but one or more x_i are unknown
- **second kind:** no physically founded functional
dependence $f(\dots)$ is known

⇒ must be calibrated at known T

Low Temperature Thermometers



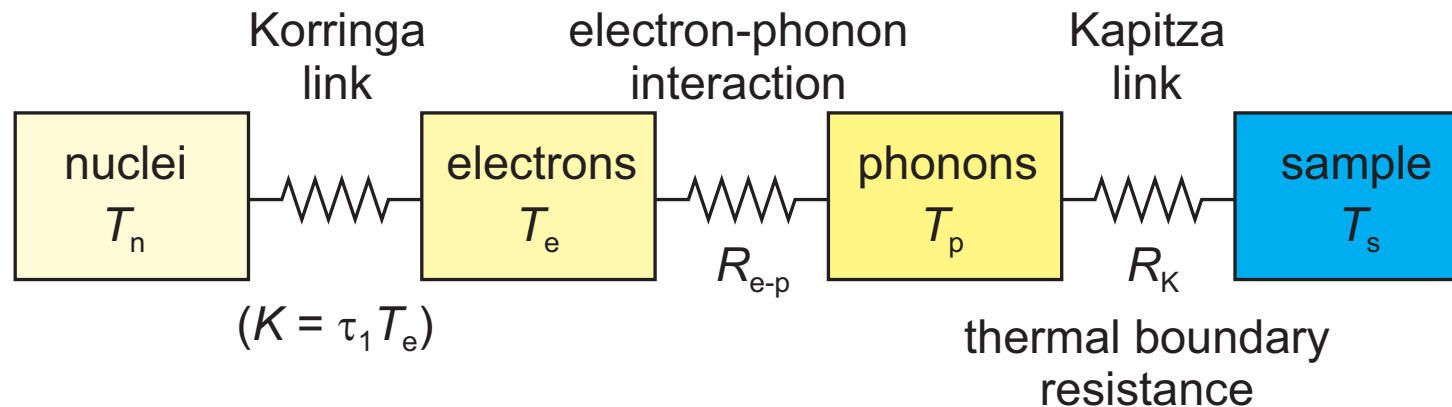
Properties of Thermometers

- **sensitivity**: $(\Delta f/f) / (\Delta T/T)$
- experimentally **easy measurement** of $f(T, x_1, x_2, \dots)$
- **relaxation times** to reach thermal equilibrium
 - internal: spin-lattice relaxation time τ_1 , spin-spin relaxation time τ_2
 - external: heat capacity, thermal conductivity, thermal contact
- **power** necessary to **read out** the device \Rightarrow dissipation & self heating

- **speed** of the thermometer: time to reach a given uncertainty $u(T)$

- **long-term stability**: drift of parameters x_i
- stability with respect to thermal cycling
- **external conditions**: e.g. magnetic field B can affect $f(\dots)$ (or B is required),
vibrations,
rf interference

Thermal Contact



Heat flow \dot{Q} through thermal resistance R causes **temperature step** ΔT :

$$\dot{Q} = \Delta T / R$$

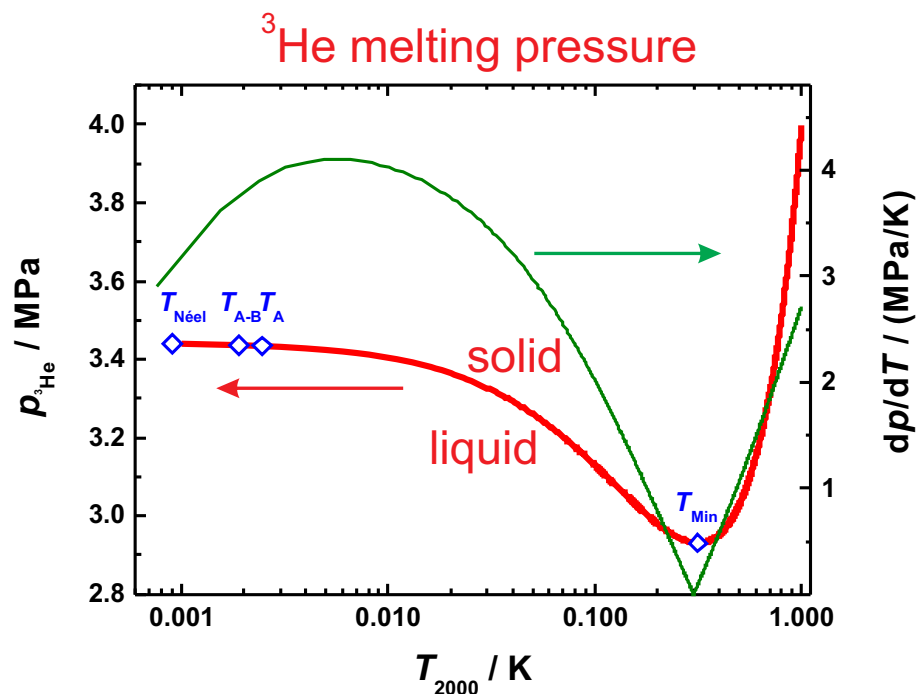
Metallic contact: **Wiedemann-Franz law**, relating thermal & electrical conductivities

$$L_0 = \kappa / (\sigma T) = 2.45 \cdot 10^{-8} \text{ W}\Omega\text{K}^{-2}$$

e.g. $0.1 \mu\Omega$ at 4 K for bolted contacts

The International Temperature Scale PLTS-2000

- PLTS-2000: **P**rovisional **L**ow **T**emperature **S**cale of 2000
- adopted by the International Committee for Weights and Measures (CIPM - *Comité International des Poids et Mesures*)



$$\frac{p_{3\text{He}}}{\text{MPa}} = \sum_{i=-3}^9 a_i \left(\frac{T_{2000}}{\text{K}} \right)^i$$

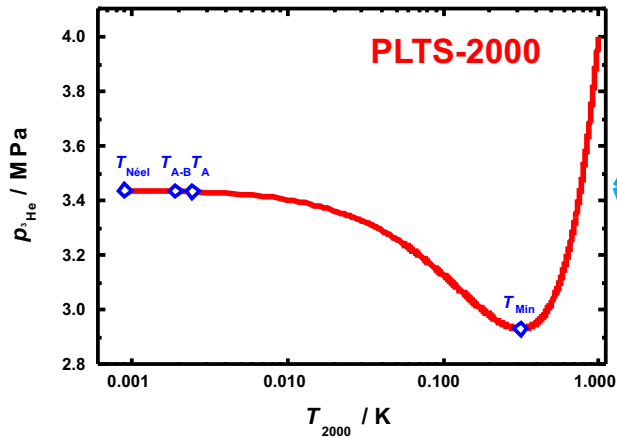
T range: 0.9 mK to 1 K
p range: 2.9 MPa to 4 MPa

Fixed points	$p_{3\text{He}} / \text{MPa}$	T_{2000} / mK
Minimum	2.93113	315.24
A	3.43407	2.444
A-B	3.43609	1.896
Neél	3.43934	0.902

- 4 inherent fixed points of the scale:
 3 phase transitions (A, A-B, Neél) besides the minimum of the melting curve $p_{3\text{He}}(T_{2000})$

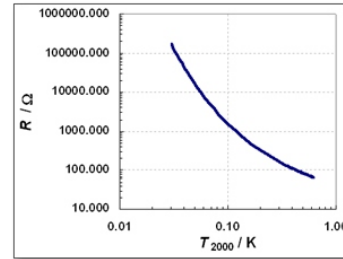
Dissemination of the Kelvin

Legal task of PTB:
 realisation and dissemination of SI units
 (m, kg, s, A, K, mol, cd)

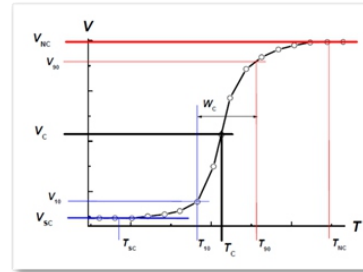


⇒ **Dissemination** of the international temperature scale **PLTS-2000** by calibration of practical thermometers for users worldwide

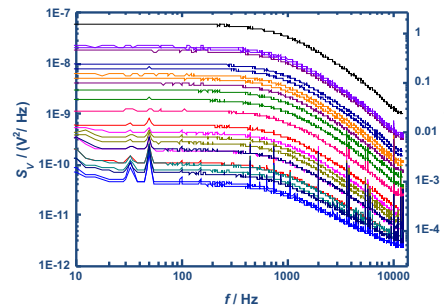
Resistance thermometers



Superconducting reference point samples

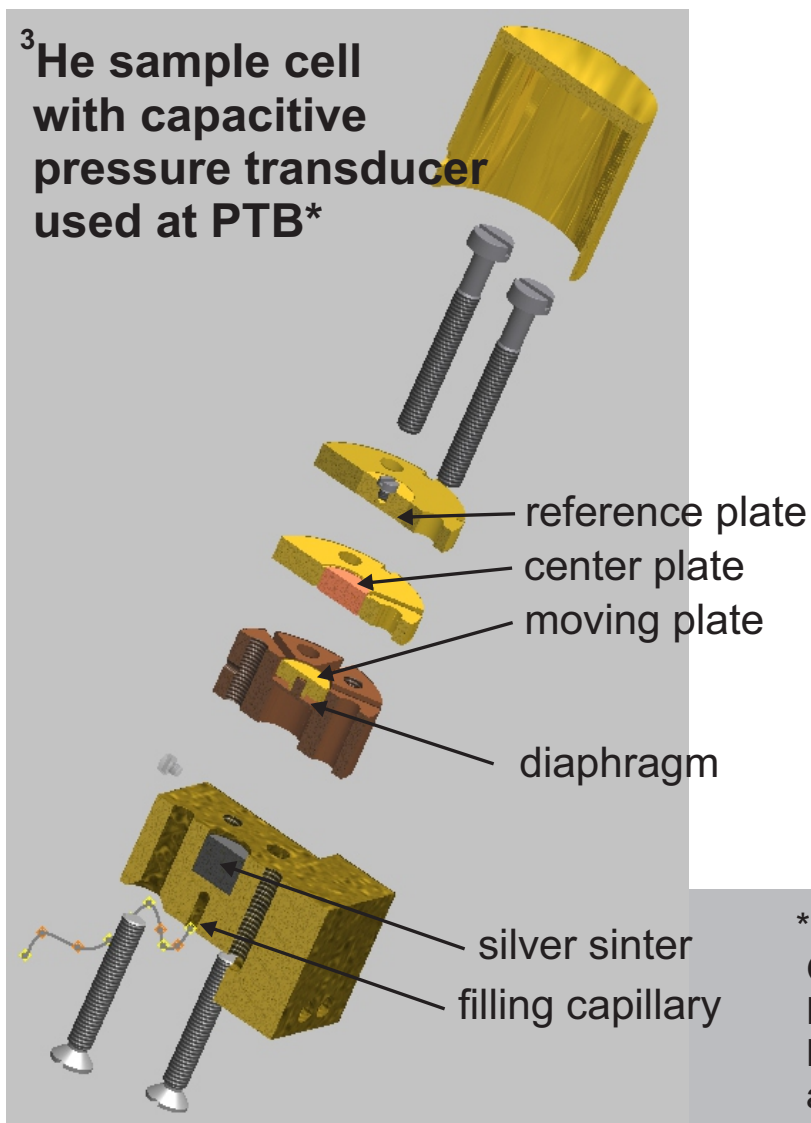


Noise thermometers: MFFT, CSNT



calibration certificate

Implementation of the ^3He MCT (PLTS-2000)



- laboratory standard in specialist labs
- field independent
- considered as difficult to implement for expanding community of users of ultra-low temperature platforms
- requires calibration of the pressure transducer
- measurement of absolute pressure
- slow traversing of fixed points

⇒ expert knowledge and experience required

*For details see:
G. Schuster, A. Hoffmann and D. Hechtfisher,
Realisation of the temperature scale PLTS-2000 at PTB,
PTB, Braunschweig, PTB-ThEx-21, 29pp, 2001,
available through www.ptb.de

Coulomb Blockade Thermometry



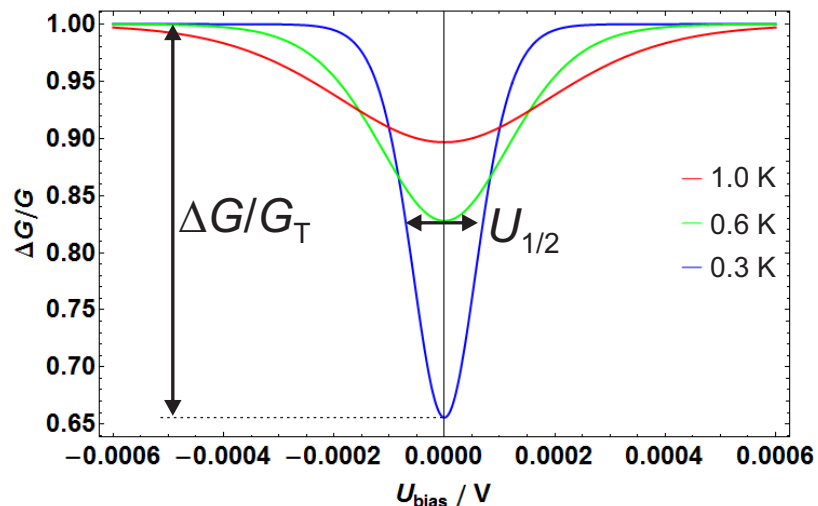
Aalto University

School of Science *Low Temperature Laboratory, PICO-group*

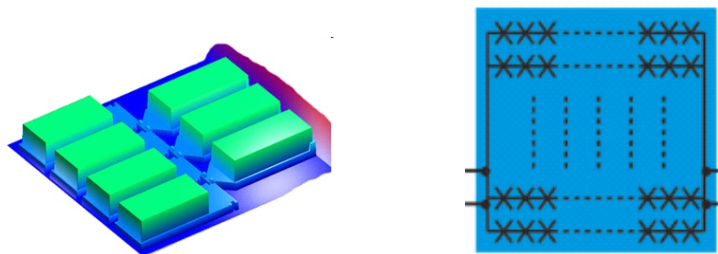
- arrays of tunnel junctions
- weak Coulomb blockade: $E_C \ll k_B T$
- measure differential conductance $\Delta G/G_T$
- **primary** or secondary thermometer mode

$$\frac{\Delta G}{G_T} = 1 - \frac{2(N-1)}{N} \frac{E_C}{k_B T} \left(\frac{x \sinh(x) - 4 \sinh^2(x/2)}{8 \sinh^4(x/2)} \right)$$

$$T = \frac{1}{5.439} \frac{eU_{1/2}}{Nk_B} \quad x = \frac{eU_{\text{bias}}}{Nk_B T}$$

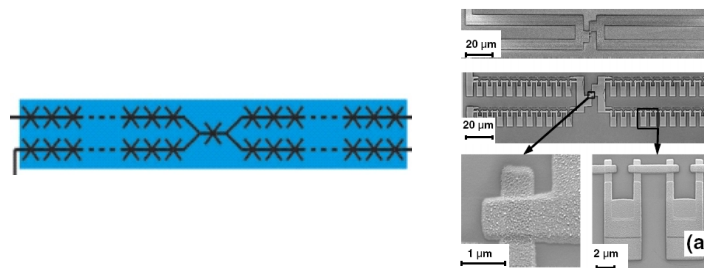


Coulomb blockade thermometer (CBT)



J. Pekola et al., Phys. Rev. Lett. 1994,
 „Thermometry by Arrays of Tunnel Junctions“

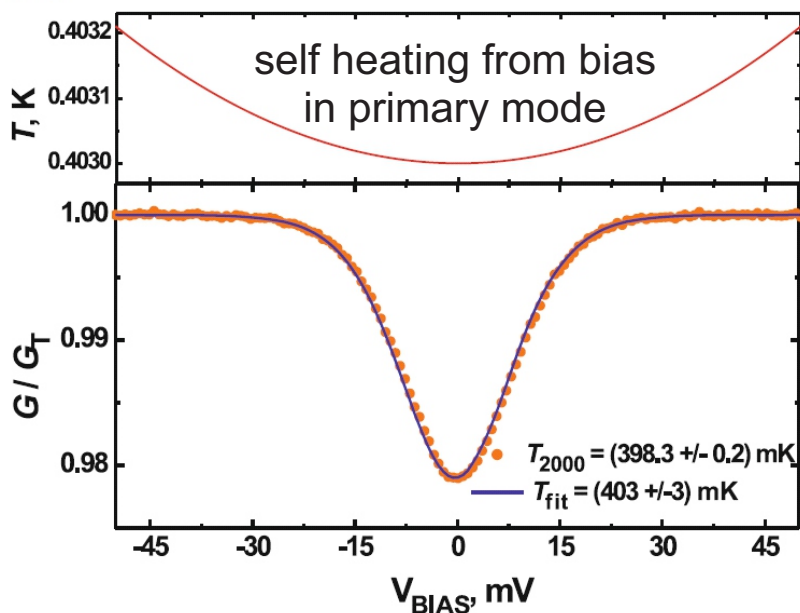
Single junction thermometer (SJT)



J. Pekola et al., Phys. Rev. Lett. 2008,
 „Primary tunnel junction thermometry“

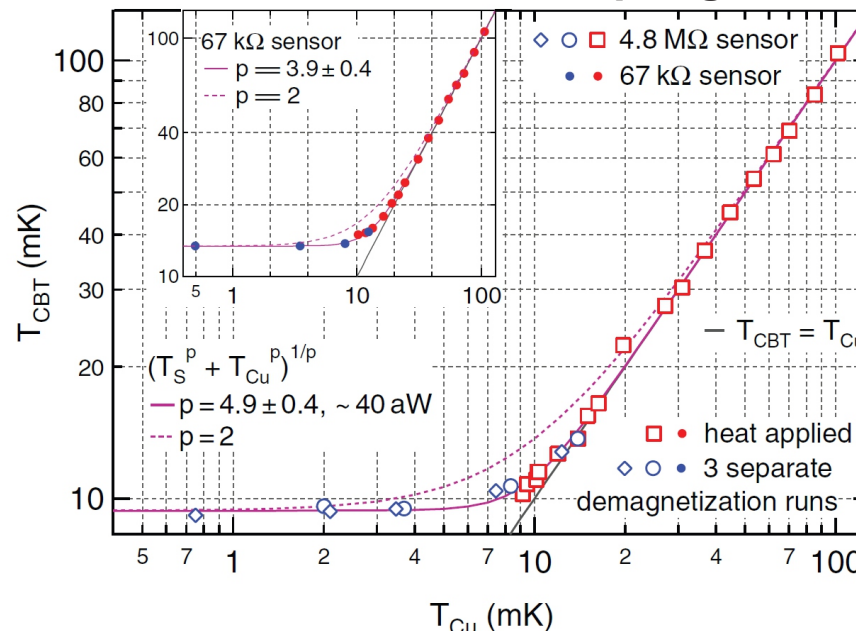
Coulomb Blockade Thermometry

(a) Experimental data at ≈ 400 mK



Meschke et al, Int. J. Thermophys. 2011

Thermal decoupling



Casparis et al, Rev. Sci. Instrum. 83 (2012) 083903

- no influence of magnetic field on T_{CBT}
- limitations:
 - inhomogeneities in the array (varying junction resistance)
 - high T : signal too small to measure if $\Delta G/G_T < 0.003$ (~ 30 K)
 - low T : increasing sensitivity to background charges if $\Delta G/G_T > 0.3$ (SET), hot-electron effect

Coulomb Blockade Thermometry

- Full references:

J.P. Pekola, K.P. Hirvi, J.P. Kauppinen, and M. A. Paalanen, Thermometry by Arrays of Tunnel Junctions, Phys. Rev. Lett. **73** (1994) 2903

J.P. Pekola, T. Holmqvist, and M. Meschke, Primary Tunnel Junction Thermometry, Phys. Rev. Lett. **101** (2008) 206801

- Meaning of symbols:

N - number of tunnel junctions in series

G_T - asymptotic conductivity at high bias voltages U_{Bias}

$E_C = e^2 / 2C_{\text{eff}}$ - charging energy, with C_{eff} being the effective capacitance of the array

$U_{1/2}$ - full width at half maximum (FWHM) of the charging peak, i.e. FWHM of the conductance drop of $\Delta G / G_T$

- Thermometer mode:

- primary thermometer mode: measure $U_{1/2}$

- secondary thermometer mode: measure $(\Delta G / G_T)^{-1}$ and determine E_C at a known reference temperature (calibration)

- Interpretation of the thermal decoupling graph:

The graph shows the CBT electron temperature T_{CBT} (in secondary mode) versus temperature of the bath T_{Cu} (copper in a nuclear refrigerator). Results for two CBTs with different resistances R are shown, with excellent agreement at high temperatures and a full thermal decoupling from T_{Cu} well below 10 mK. Lower temperatures are reached for the high-impedance CBT due to better isolation from the environment by lower dissipation.

Nuclear Orientation Thermometer

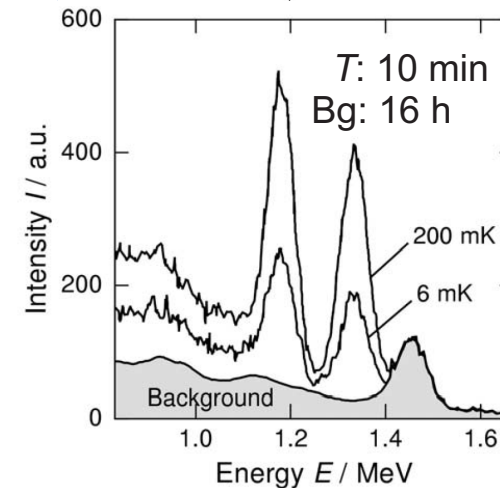
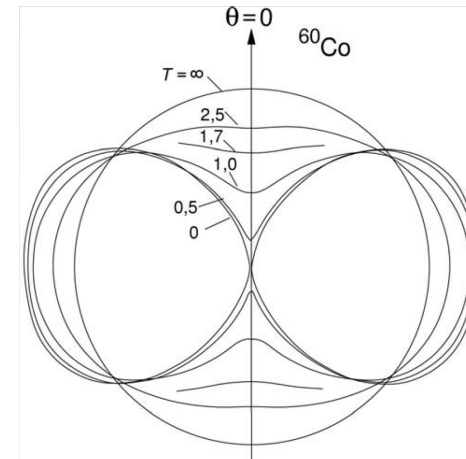
- anisotropic γ radiation from radioactive β decay from nuclei in magnetic field (ferromagnetic matrix)
- probe thermal population of nuclear energy levels
 \Rightarrow measure angular distribution of γ radiation

- Problems:

- heat from radioactive decay completely deposited in the sample
- long measurement times for low activity samples to obtain acceptable statistical uncertainty
- discriminate background radiation

\Rightarrow Primary thermometer with small usable temperature range:
 ^{60}Co in Co matrix: 3 mK ... 30 mK
 ^{54}Mn in Ni matrix: 6 mK ... 60 mK

- min. uncertainty 0.1% at 10 mK (Marshak, J. Res. NBS **88** (1983) 175)



Schuster, Hechtfisher, Fellmuth,
Rep. Prog. Phys. 57 (1994) 187

Noise Thermometry

... based on electronic noise in electric conductors (Johnson noise)

- Pros:**
- theoretically very well understood
 - primary thermometers possible
 - extremely large temperature range (... 50 μ K ... 2000 K ...)

... at low temperatures:

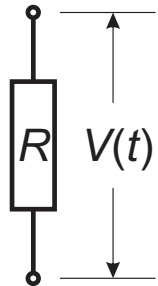
- measurement of noise in thermal equilibrium without excitation
⇒ no dissipation
- temperature sensors: metallic, large volume possible
⇒ good thermal contact of electrons
- large temperature range (≤ 50 μ K ... 4 K) with single sensor

- Cons:**
- sufficiently large measurement time (or number of averages) necessary for good statistics:

$$\frac{\Delta T}{T} = \frac{1}{\sqrt{M \cdot N}} = \frac{1}{\sqrt{t_{\text{meas}} \Delta f}}$$

- distinguish or suppress influence of non-thermal noise

Readout Schemes of Noise Thermometers



Thermal voltage fluctuations in resistor R : Johnson noise, Nyquist formula

$$\langle V^2(t) \rangle = S_V \cdot \Delta f \quad \text{with} \quad S_V \cong 4k_B T R \quad \text{for} \quad hf \ll k_B T$$

Johnson, Phys. Rev. **32**(1928)97,
Nyquist, Phys. Rev. **32**(1928)110

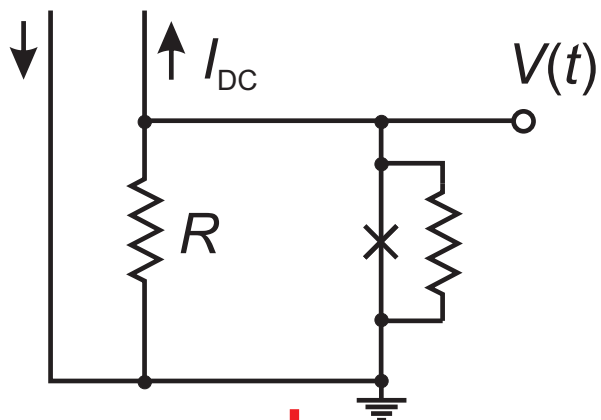
Modulation technique (Basis of the PLTS-2000 at NIST and PTB)
High-frequency carrier generated from Josephson contact („R-SQUID“)
⇒ frequency modulation by thermal noise
Josephson Junction Noise Thermometer (JNT)

Direct measurement of noise voltage or noise current
⇒ SQUID current sensor as low noise amplifier
Current Sensing Noise Thermometer (CSNT)

Indirect measurement of noise currents
⇒ SQUID magnetometer or gradiometer detecting the corresponding
fluctuations of the magnetic field
Magnetic Field Fluctuation Thermometer (MFFT)

Josephson Junction Noise Thermometer

Kamper, Zimmermann, *J. Appl. Phys.* **42** (1971) 132



Josephson effect: $f = V / \Phi_0$

$$V = I_{DC}R + V_{noise}$$

\Rightarrow frequency modulation by V_{noise} ,
 $f_0 = I_{DC}R / \Phi_0 + \text{side bands}$

e.g. $I_{DC} = 10 \text{ mA}$, $R = 10 \mu\Omega \Rightarrow f_0 \approx 50 \text{ MHz}$

- Primary thermometer

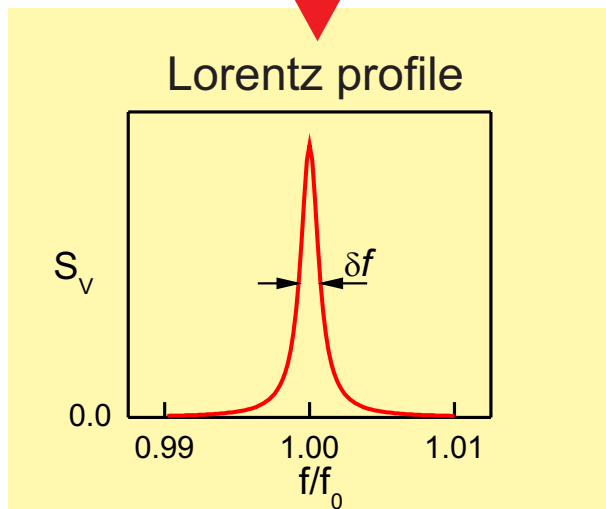
Two measurement techniques:

- Measurement of the spectrum, line width:

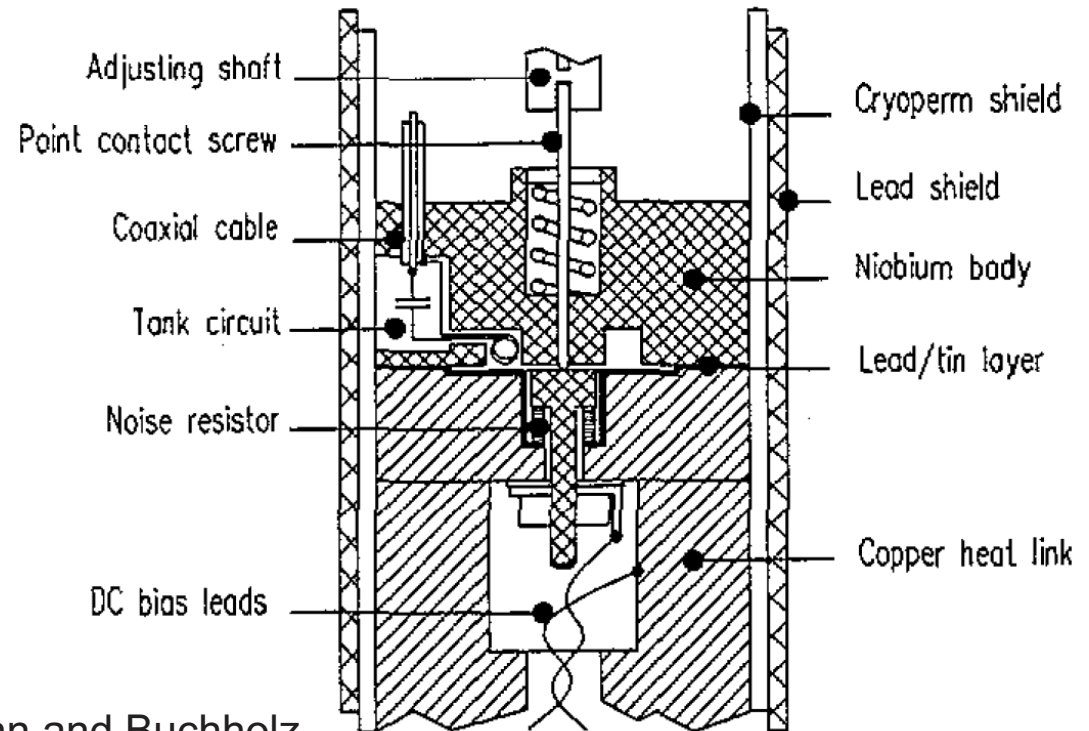
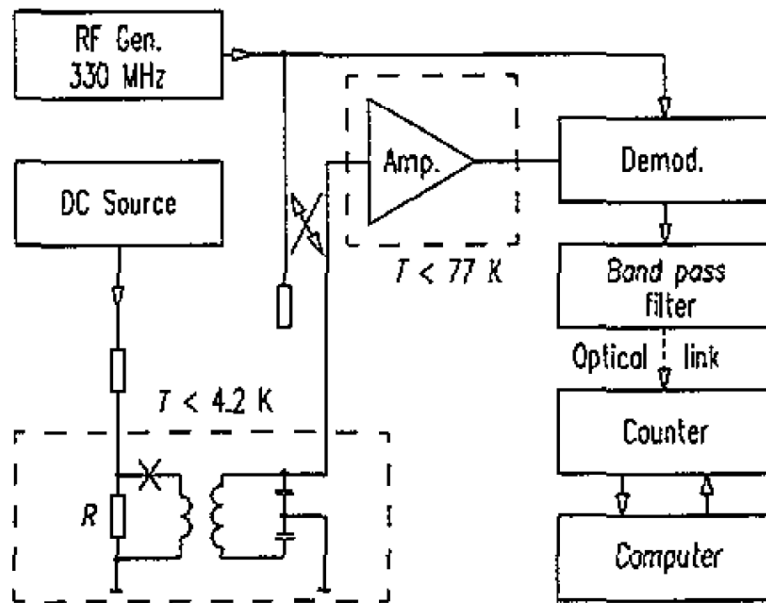
$$\delta f = \frac{4\pi k_B TR}{\Phi_0^2}$$

- frequency counting, variance at measurement time τ :

$$\sigma^2 = \langle (f - f_0)^2 \rangle = \frac{2k_B TR}{\tau \Phi_0^2}$$



Josephson Junction Noise Thermometer at PTB

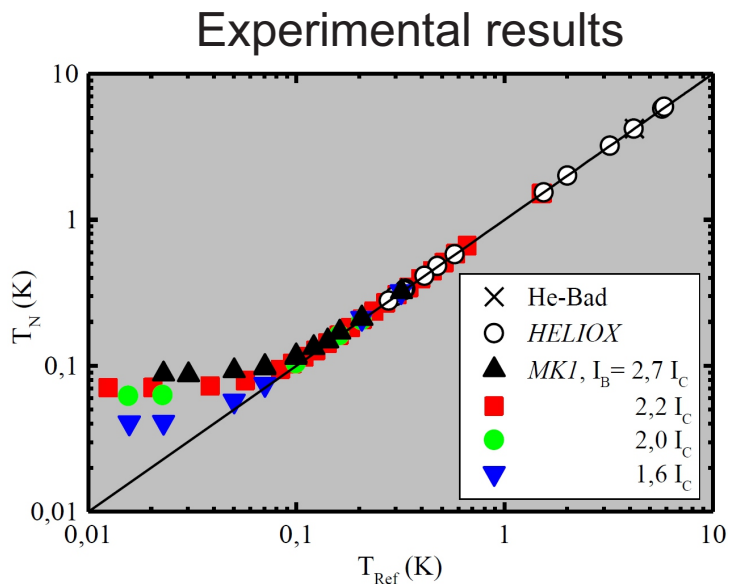
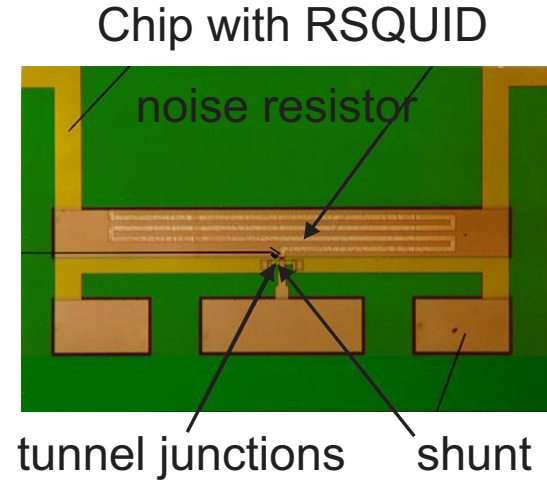
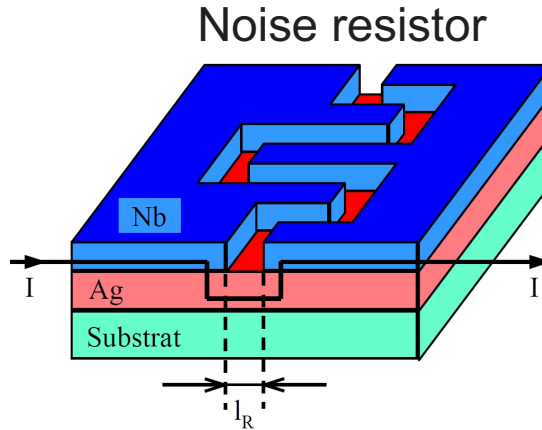
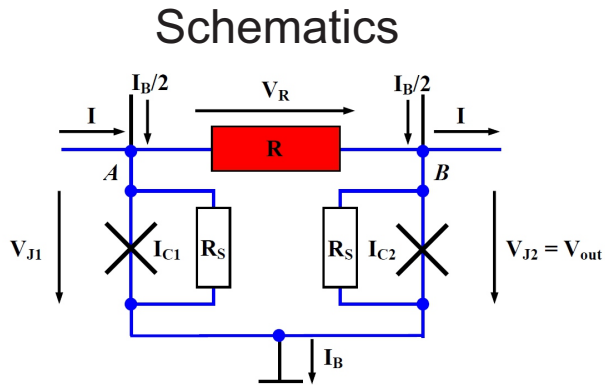


Hoffmann and Buchholz,
J. Phys. E: Sci. Instrum. 17(1984)1035

- uncertainties due to down mixing of external rf noise
- self heating of noise resistor due to bias
- slow: 0.1% (3σ) in a day

Thin-film DC RSQUID

Stefan Menkel, PhD thesis, 2001: *Integrierte Dünnschicht-dc RSQUIDs für die Rauschthermometrie*



- $R \approx (10 \dots 20) \mu\Omega$
- $\delta T/T = 0.66 \%$ in 24 min

- thermal decoupling due to hot-electron effect
- dissipation in shunt resistors

Thin-film DC RSQUID

Background information:

The RSQUID in thin-film technique was thought to replace the bulk-rf RSQUIDs with their practical disadvantages in adjusting the Josephson point contact.

Thin-film devices offer several advantages over bulk devices:

- advantages of the thin-film devices:
 - thin-film tunnel contacts
 - good reproducibility of shape, electrical parameters, ...
 - small devices
 - easy practical use
- dc RSQUID instead of rf RSQUID for easier readout

At the same time a possible disadvantage must be solved or put up with:

- proper integration of the noise resistor into the SQUID loop to achieve good thermal coupling

Results:

- Thermal decoupling below 100 mK for the tested devices.

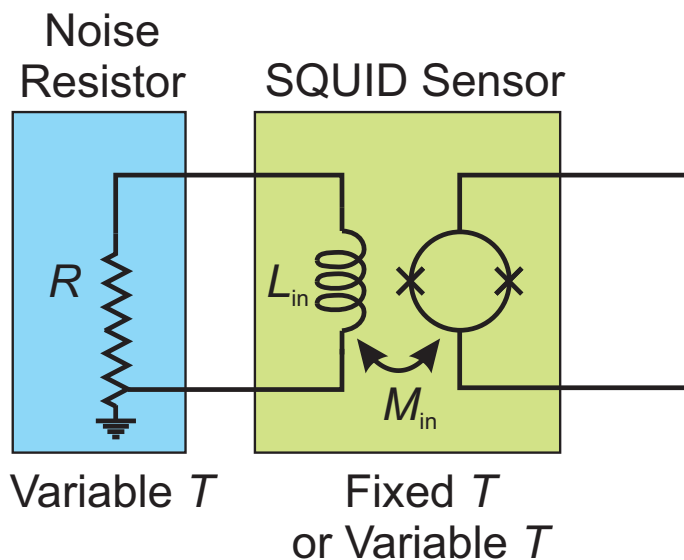
General:

- Hot-electron effect:
 - Overheating of the electron gas due to the decreasing electron-phonon coupling at low temperatures. The electron system can have considerably higher temperatures than the phonons and/or completely decouple from the phonon temperature.
 - Cf. F.C. Wellstood, C. Urbina, and J. Clarke, Hot-electron effects in metals, Phys. Rev. B **49** (1994) 5942
 - Compare with results found for the CBTs.

CSNT and MFFT

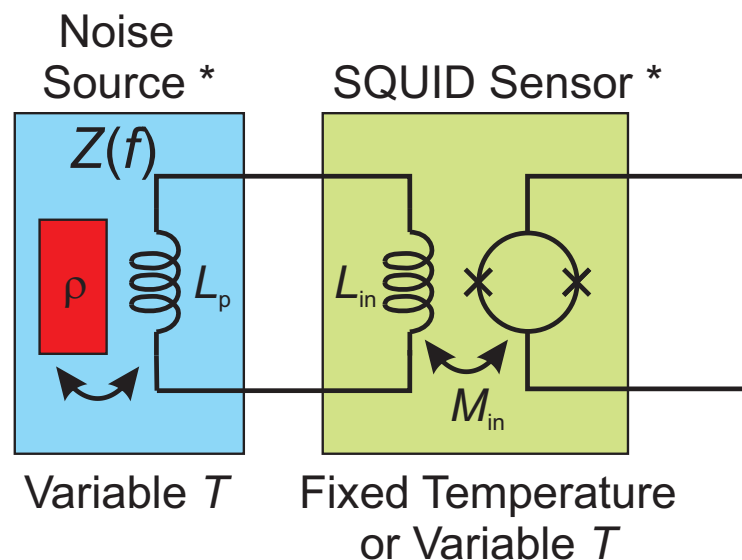
CSNT

Current Sensing Noise Thermometer



MFFT

Magnetic Field Fluctuation Thermometer



$R(T) = \text{const.}$

Secondary thermometer

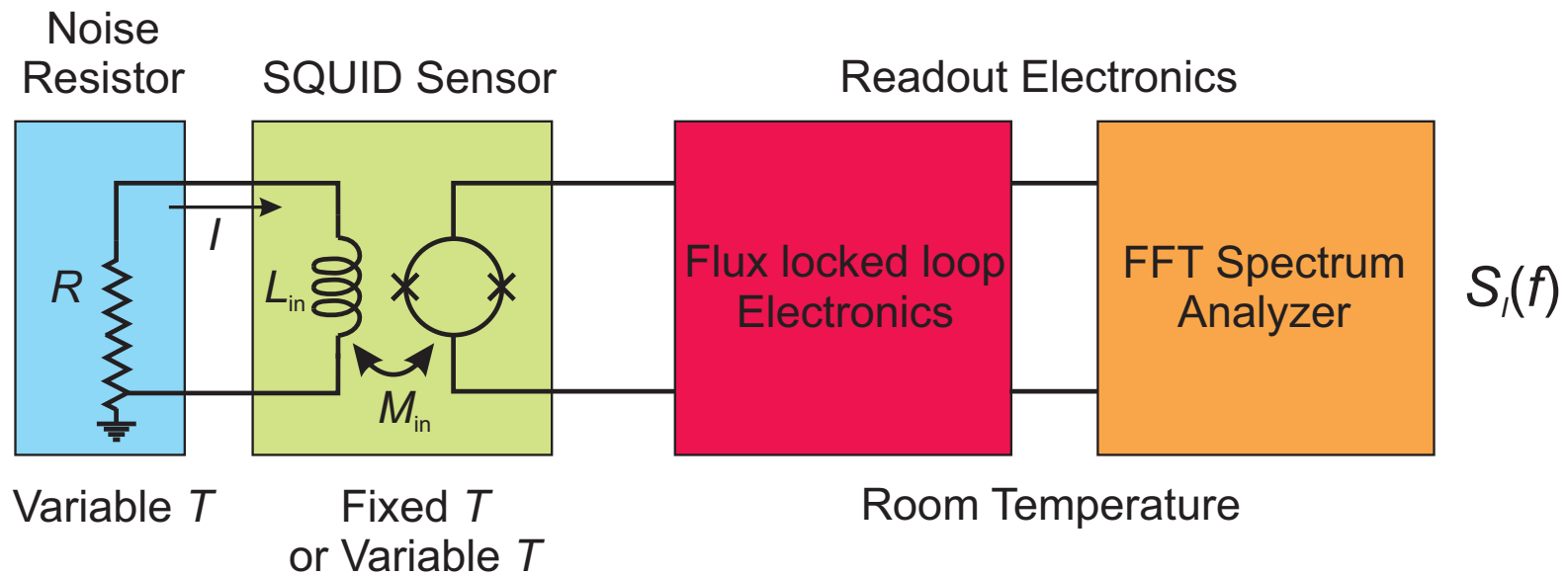
$$\frac{T}{T_{\text{Ref}}} = \frac{S_x(f, T)}{S_x(f, T_{\text{Ref}})}$$

$\rho(T) = \text{const.}$
 $\mu(T) = \text{const.}$

* alternatively for MFFT:
 multiloop SQUID field sensor

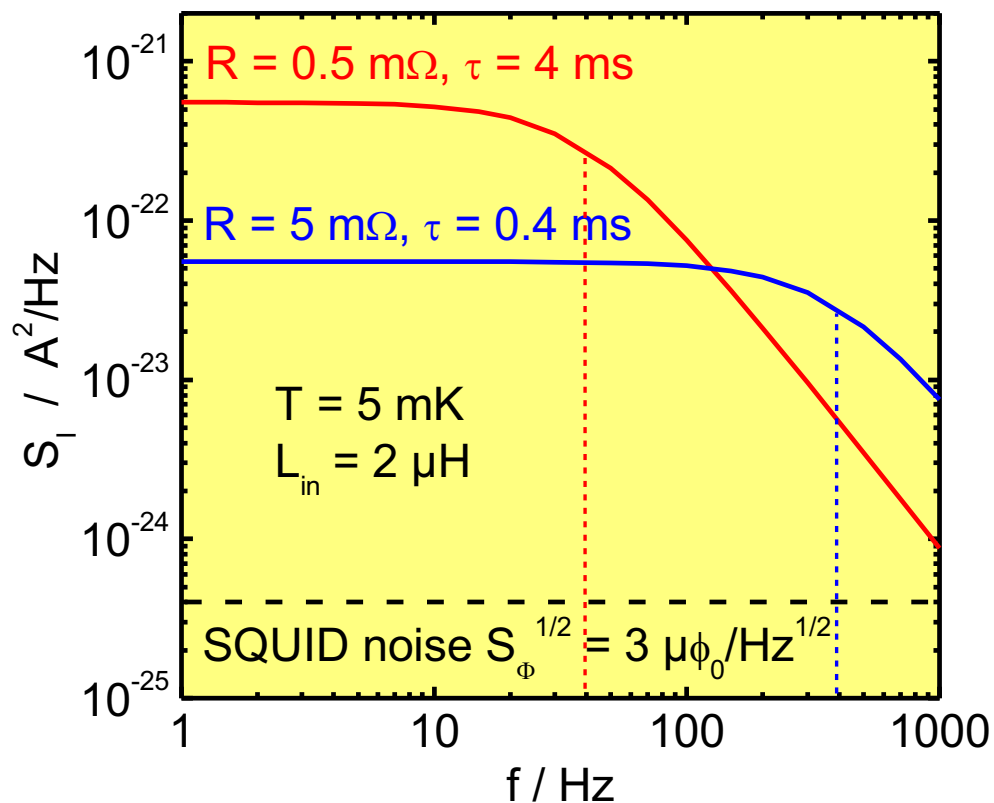
Current Sensing Noise Thermometer (CSNT)

⇒ direct measurement of noise current $I(t)$ and its spectral density $S_I(f)$



L - R circuit: first-order low pass

CSNT: Spectral Density S_I



L - R circuit: first-order low pass

$$S_I(f) = \frac{4k_B T}{R} \left(\frac{1}{1 + (f/f_c)^2} \right)$$

$$f_c = \frac{R}{2\pi L}$$

total energy: $\int_0^{\infty} \frac{L}{2} S_I(f) df = \frac{1}{2} k_B T$

\Rightarrow average magnetic energy stored in the coil (inductivity L) as expected for single degree of freedom

energy below f_c : $\frac{1}{4} k_B T$

\Rightarrow 50% for low pass of first order

CSNT Performance

SQUID with coupled energy resolution ϵ_C : $\epsilon_C = \frac{1}{2} L_{\text{in}} S_I = \frac{1}{2} L_{\text{in}} \frac{S_\Phi}{M_{\text{in}}^2}$

CSNT noise temperature: $T_N = \left(\frac{\epsilon_c}{2k_B} \right) \left(\frac{R}{L} \right)$

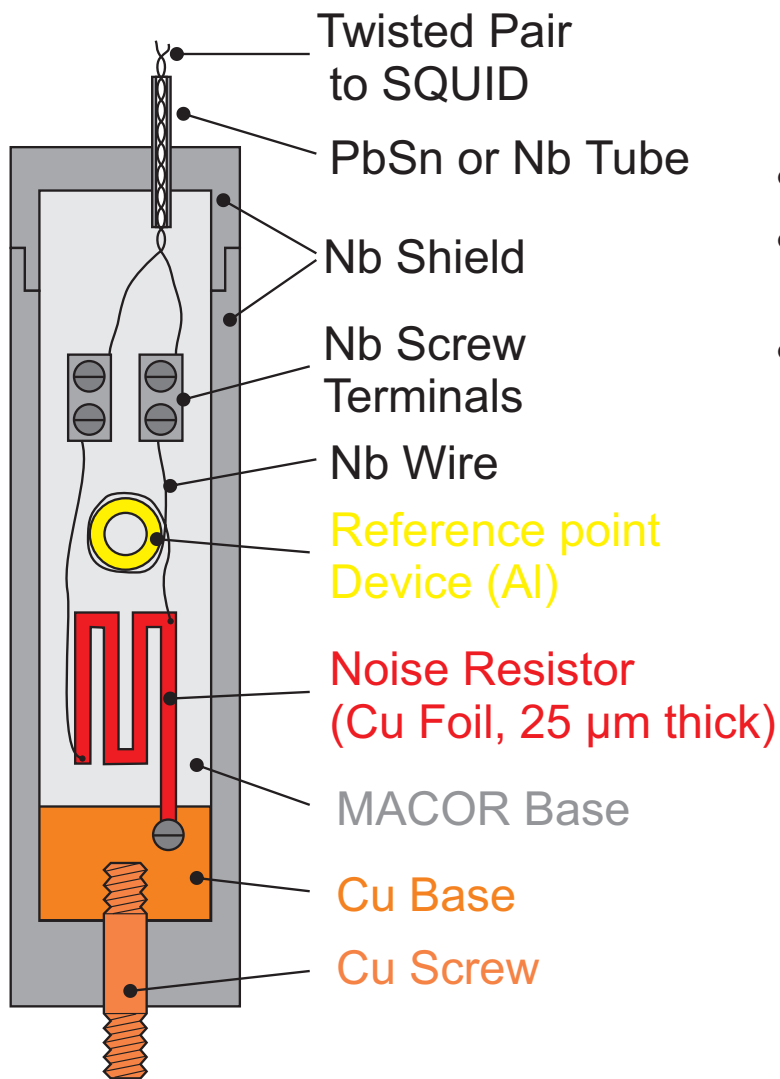
Speed of the thermometer: $\sigma = \frac{\Delta T}{T} \approx \left(\frac{2\tau}{t_{\text{meas}}} \right)^{1/2} = \left(\frac{2L}{t_{\text{meas}} R} \right)^{1/2}$

Figure of merit: $T_N \sigma^2 t_{\text{meas}} = \frac{\epsilon_C}{k_B} \Rightarrow$ only determined by SQUID sensor

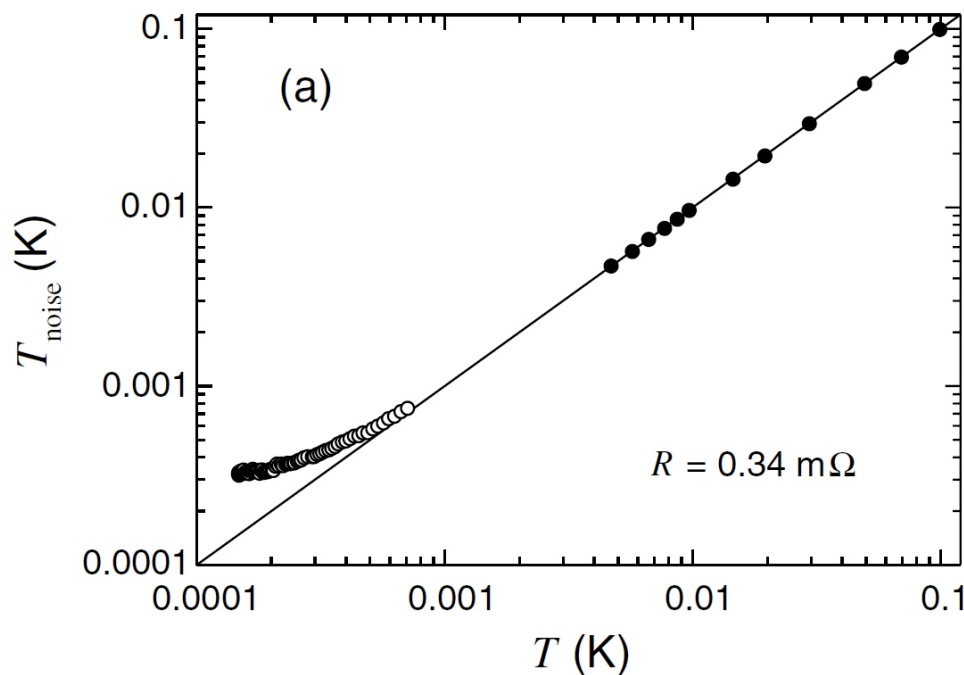
M.L. Roukes, R.S. Germain, M.R. Freeman, R.C. Richardson,
DC SQUID Noise Thermometry , LT-17 Proceedings, 1177 (1984)

CSNTs (I)

Lusher et al, Meas. Sci. Technol. 12 (2001) 1



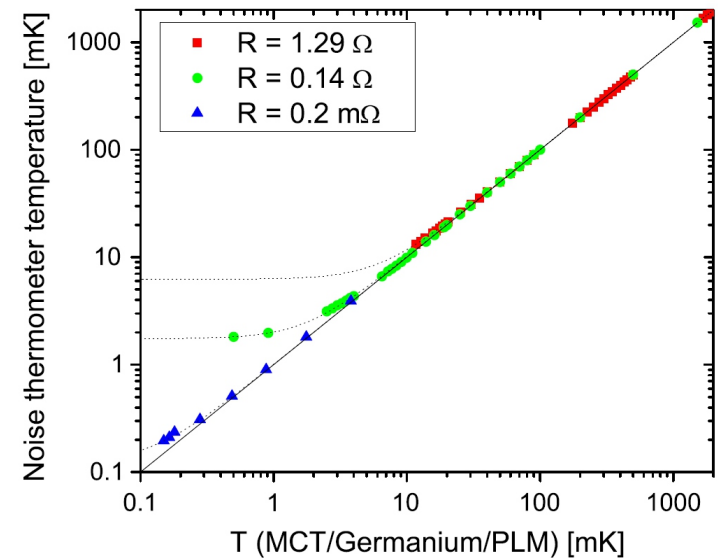
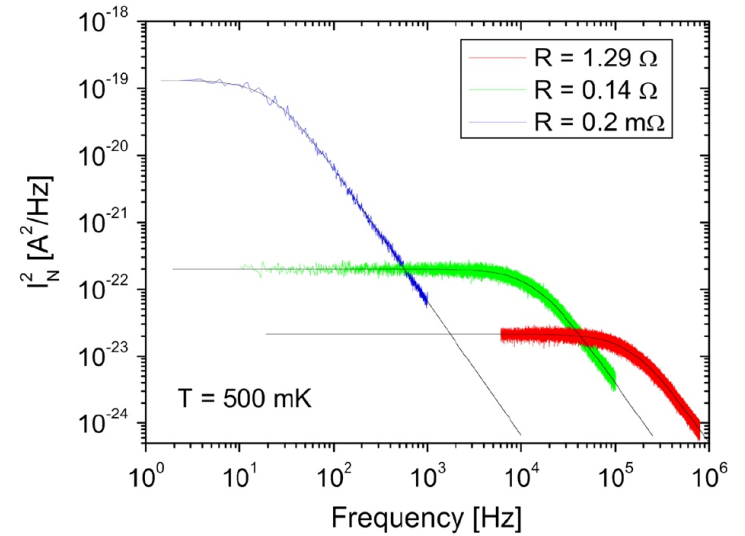
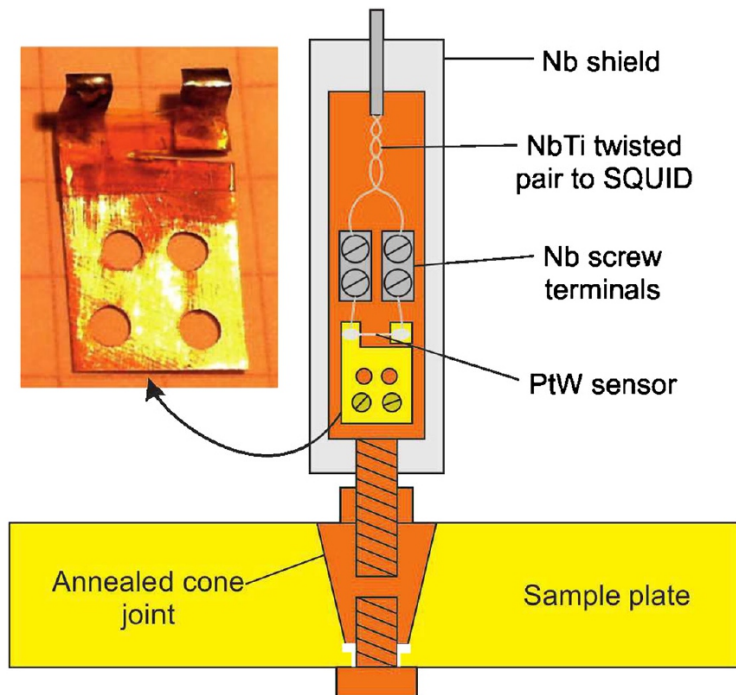
- $T_N = 1.8 \mu\text{K}$, $f_c \approx 24 \text{ Hz}$
- $T_{\text{min}} = 0.3 \text{ mK}$ due to temperature independent heat leak
- precision of 1% in 145 s



CSNTs (II)



Casey et al, J Low Temp Phys 175 (2014) 764:
Current Sensing Noise Thermometry: A Fast Practical Solution to Low Temperature Measurement



CSNTs (III)

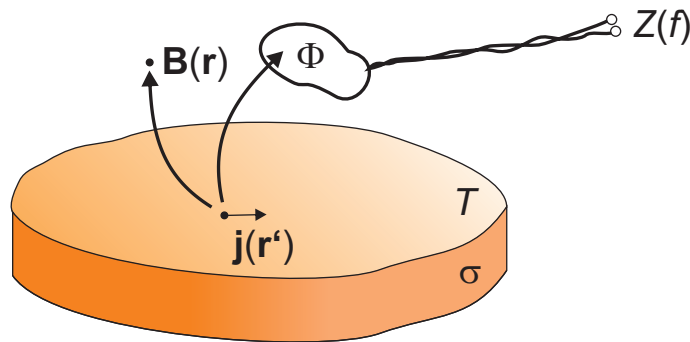
Comment on Casey's work:

- New implementation of former CSNTs developed at the Royal Holloway University of London, making the CSNT a fast and practical thermometer that can be used as standard thermometer.
- Better adaption to experimental conditions (temperature range) by choosing the optimal noise sensor from a wide range of resistances.
 - ⇒ This allows either **optimization for speed** (limited to higher temperatures) or **optimization for low noise temperatures** (at the cost of speed).

Magnetic Field Fluctuation Thermometer (MFFT)

Idea: A. Fleischmann, Universität Heidelberg, 2002 *

⇒ detect the **thermal magnetic flux noise** caused by thermally activated noise currents $\mathbf{j}(\mathbf{r}')$ in a conductor at T by means of a SQUID sensor



Power Spectral Density (PSD)

$$S_{\Phi}(f, T) = \frac{4k_{\text{B}}T\text{Re}(Z(f))}{(2\pi f)^2}$$

Different implementations:

- wire-wound coil on temperature sensor, connected to (distant) SQUID current sensor
- integrated multiloop SQUID gradiometer directly above the surface of the temperature sensor

Thermally robust:

- **good thermal contact** of a massive temperature sensor
- **large volume** for electron-phonon coupling

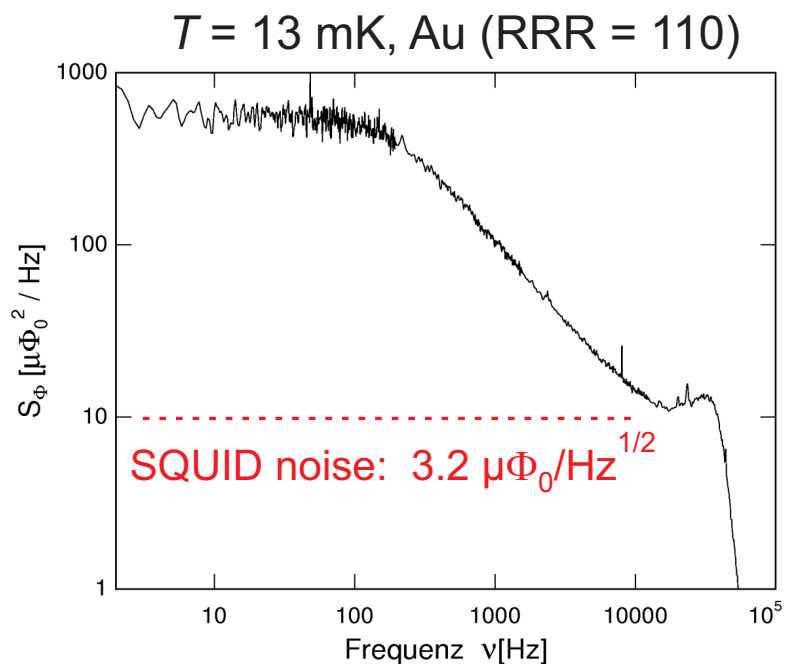
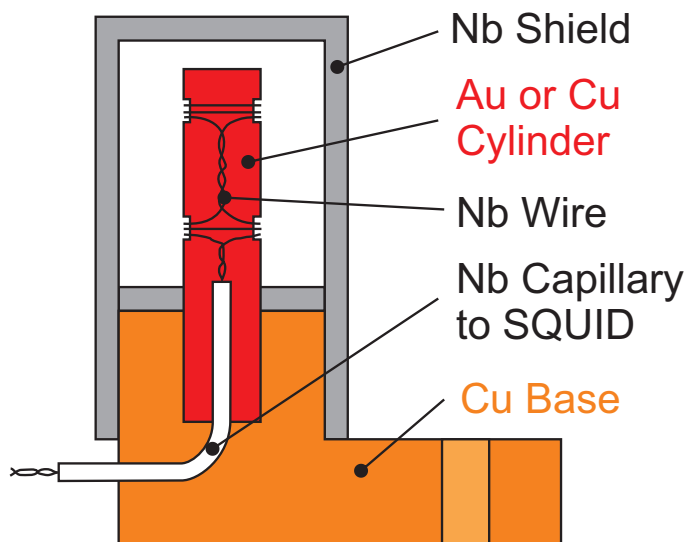
*Private communication, 2005. First paper on first implementation: A. Netsch et al, AIP **850** (2006) 1593

MFFT's (I)



A. Netsch et al, AIP 850 (2006) 1593

⇒ axial, wire-wound gradiometer around cylinder



noise sources:

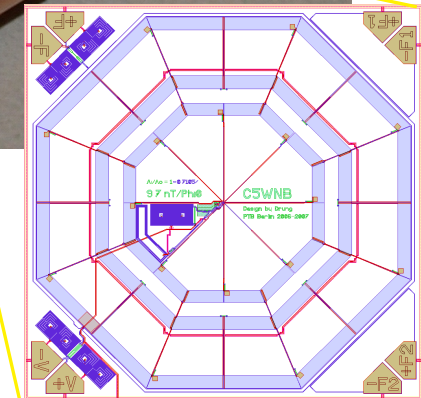
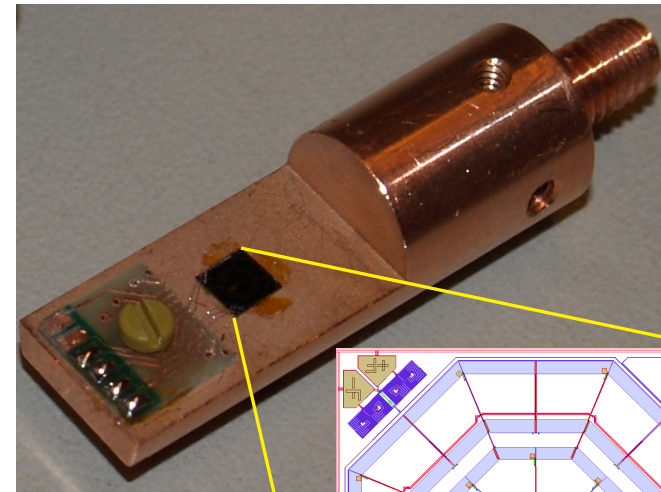
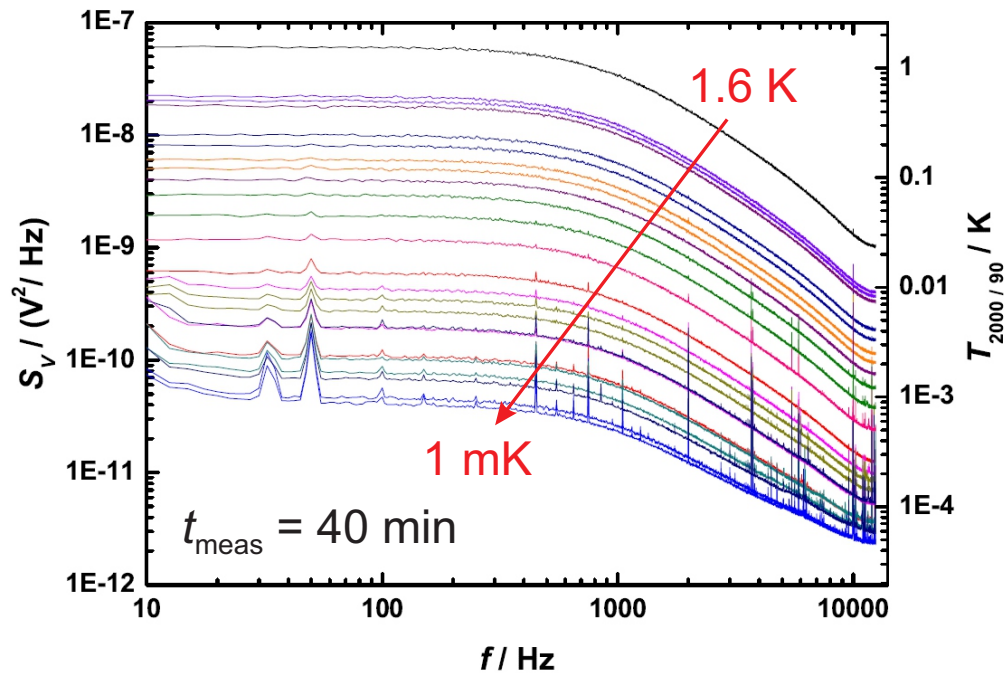
- Au (>99.999%), \varnothing 2 mm, RRR = 110
- Cu (>99.999%), \varnothing 2.5 mm, RRR = 1000

$\Delta T/T \cong 0.7\%$ in 25 s ($\Delta f = 500 \text{ Hz}$)

MFFT's (II)



Engert et al, Int J Thermophys **28** (2007) 1800
Beyer et al, Supercond. Sci. Technol. **26** (2013) 065010



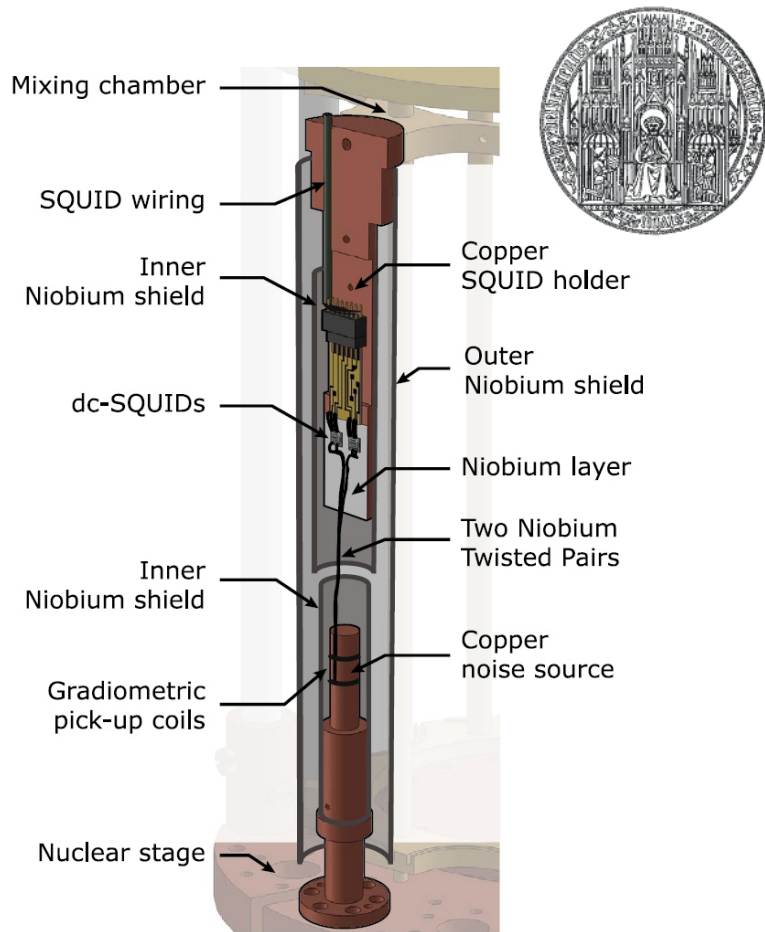
multiloop SQUID
gradiometer
(PTB type C5WN)

MFFTs (III)

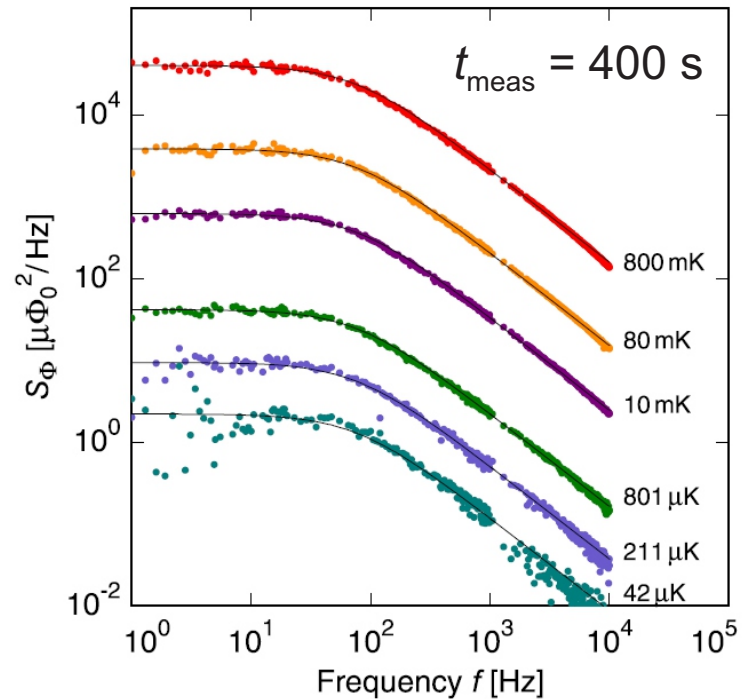
Cross-correlation technique to suppress non-thermal noise (e.g. SQUID noise)

⇒ cross-correlation of two independent channels measuring the same signal

Rothfuß et al, J Low Temp Phys 175 (2014) 776



Cross-power spectral density



⇒ resolution enhancement of ≥ 15 @ 45 μK

Conclusion

- further increasing number of **primary thermometers** (primary versions of CSNT & MFFT in development)
- **weakness of thin-film devices**: thermal decoupling at low temperatures due to the hot-electron effect
- active development of **SQUID based thermometers** (now and in the last decade)
- variety of **noise thermometers**: CSNT, MFFT, ...
- **cross-correlation technique** enhances resolution of noise thermometers (MFFT)

-
- ***Mise en pratique*** for the definition of the kelvin (MeP-K)

http://www.bipm.org/en/publications/mep_kelvin/

Scope:

„This document provides the information needed to perform a practical measurement of temperature in accord with the International System of Units (SI).“