

## CCA 2016

# Development of REBCO superconducting coils for MRI operating in subcooled LN<sub>2</sub> at 65 K

M. Iwakuma<sup>1</sup>, K. Nabekura<sup>1</sup>, K. Yun<sup>1</sup>, K. Yoshida<sup>1</sup>,  
A. Tomioka<sup>2</sup>, M. Konno<sup>2</sup>, A. Ibi<sup>3</sup>, T. Machi<sup>3</sup> and T. Izumi<sup>3</sup>

1) Kyushu University

2) Fuji Electric Co. Ltd.

3) AIST

Sept. 13, 2016, Aspen in US



KYUSHU UNIVERSITY



Fuji Electric



# Today's Contents

## 1. Introduction

Ac Loss Reduction by Scribing (AC)

in Transformers with REBCO tapes

in Motors with REBCO tapes (Trial)

= Magnetization Reduction by Scribing (DC)

## 2. Scribing effect in

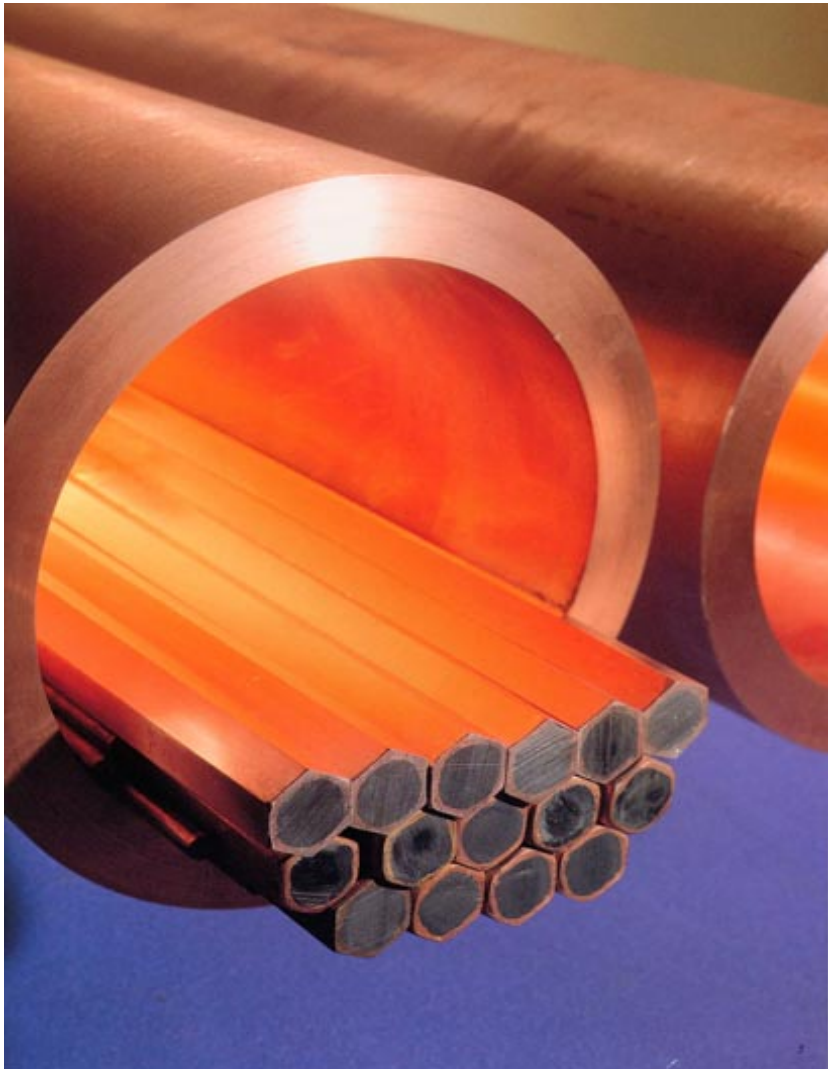
Small Test Coils with REBCO Tapes for MRI

## 3. Summary

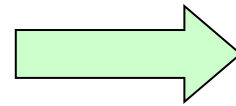
# Ac loss reduction for ac use by scribing

1. M. Iwakuma et al., “Development of a 3 $\phi$ -66/6.9kV-2MVA REBCO Superconducting Transformer”, IEEE Trans. Appl. Supercond., Vol. 25, No.3, 2015, Article No. 5500206.
2. M. Iwakuma et al., “Development of REBCO superconducting power transformers in Japan”, Physica C, Vol. 469, 2009, pp. 1726-1732.

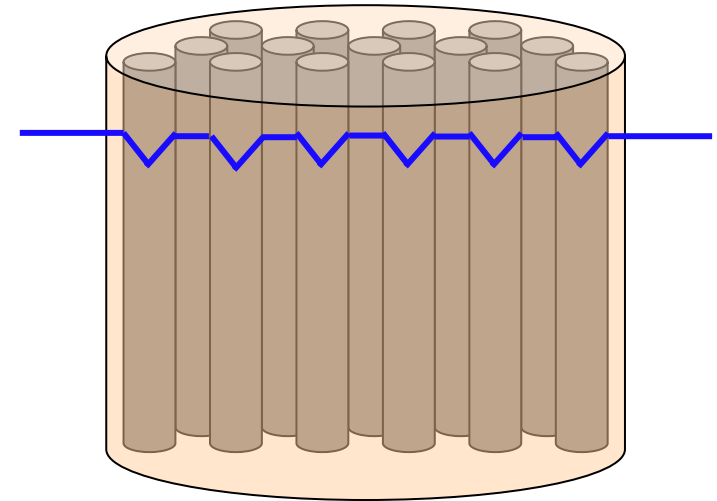
# Conventional Method for M & Ac Loss Reduction, i.e. Multifilamentization and Twisting, is not Applicable.



Fine filaments

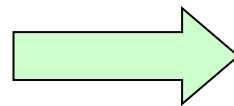


Reduction of pinning loss

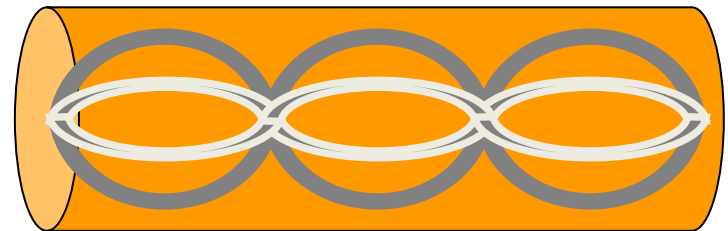


$$W = \int B dH = \int M dH \propto J_c d_f B_m \quad \text{for } B_m > B_{fp}$$

Twist & high-resistivity matrix

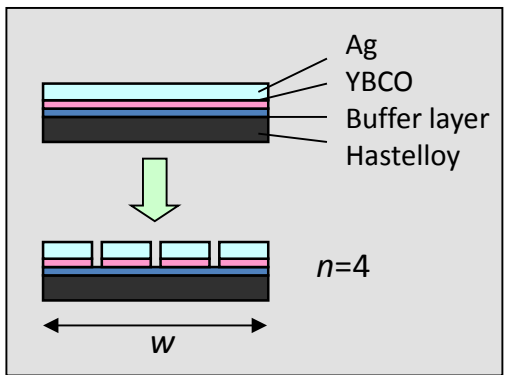
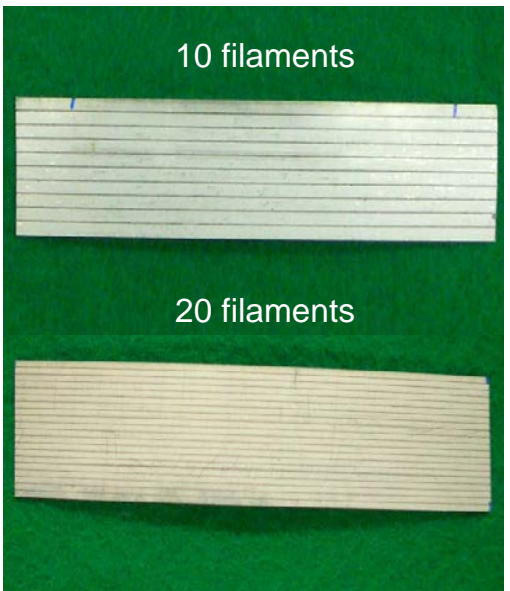
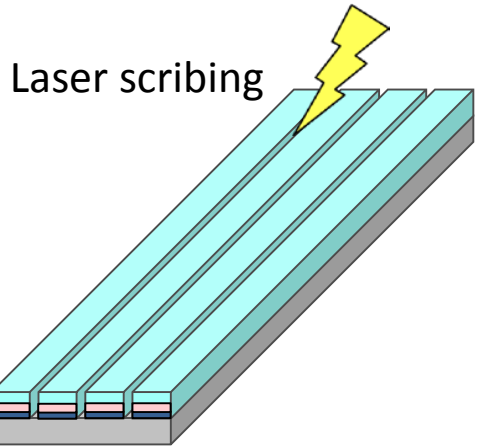


Reduction of coupling current loss

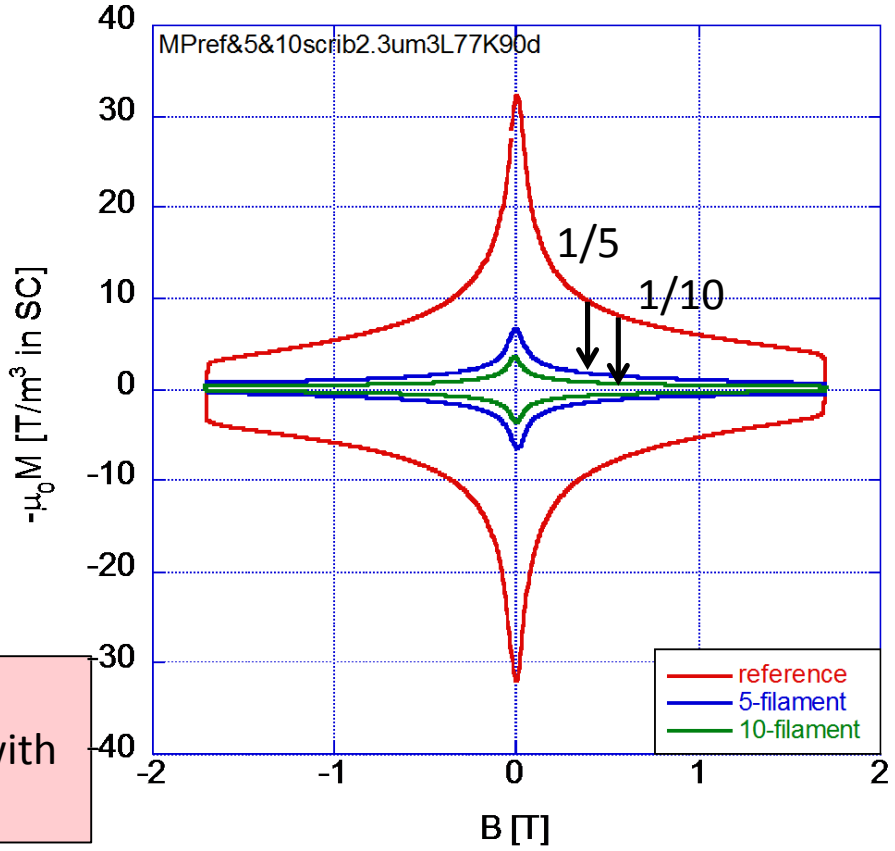


# Ac loss reduction of superconducting thin tapes

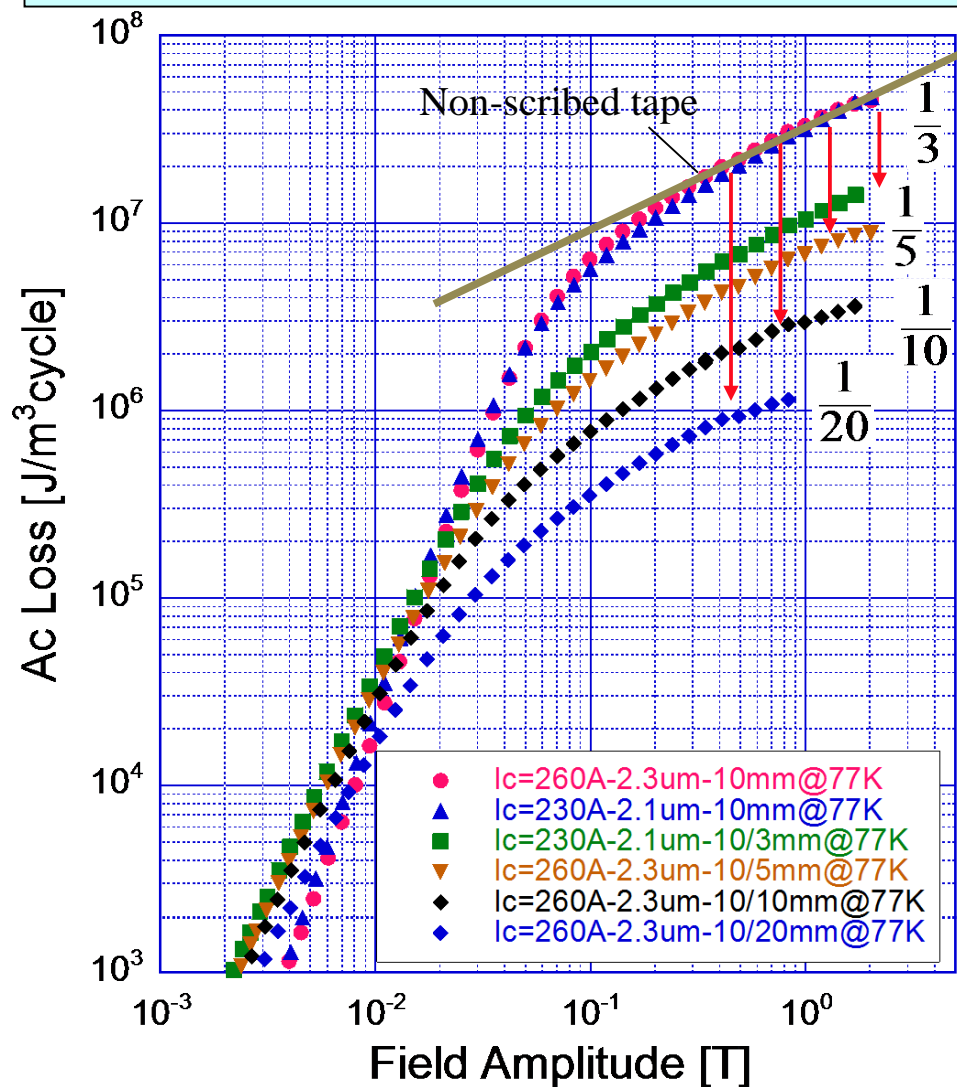
Combination { Multifilamentization by laser-scribing  
Special winding process



Buffer layer : Insulator  
⇒ Filaments are insulated with each other



# Ac losses in 1-, 3-, 5-, 10- and 20-filament short straight tapes



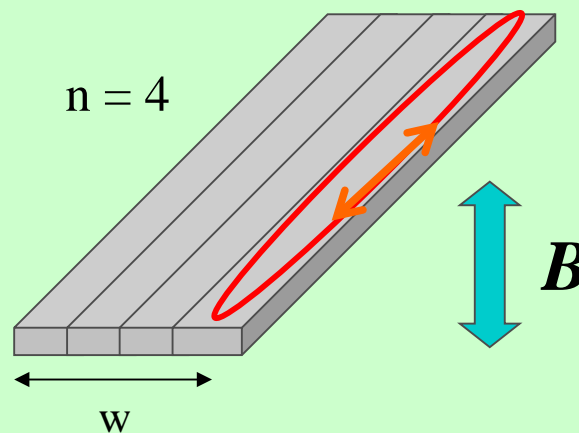
Approximate expression of ac loss

$$W = \frac{\alpha}{\gamma} B_m^\gamma \frac{w}{n}$$

Number of filaments

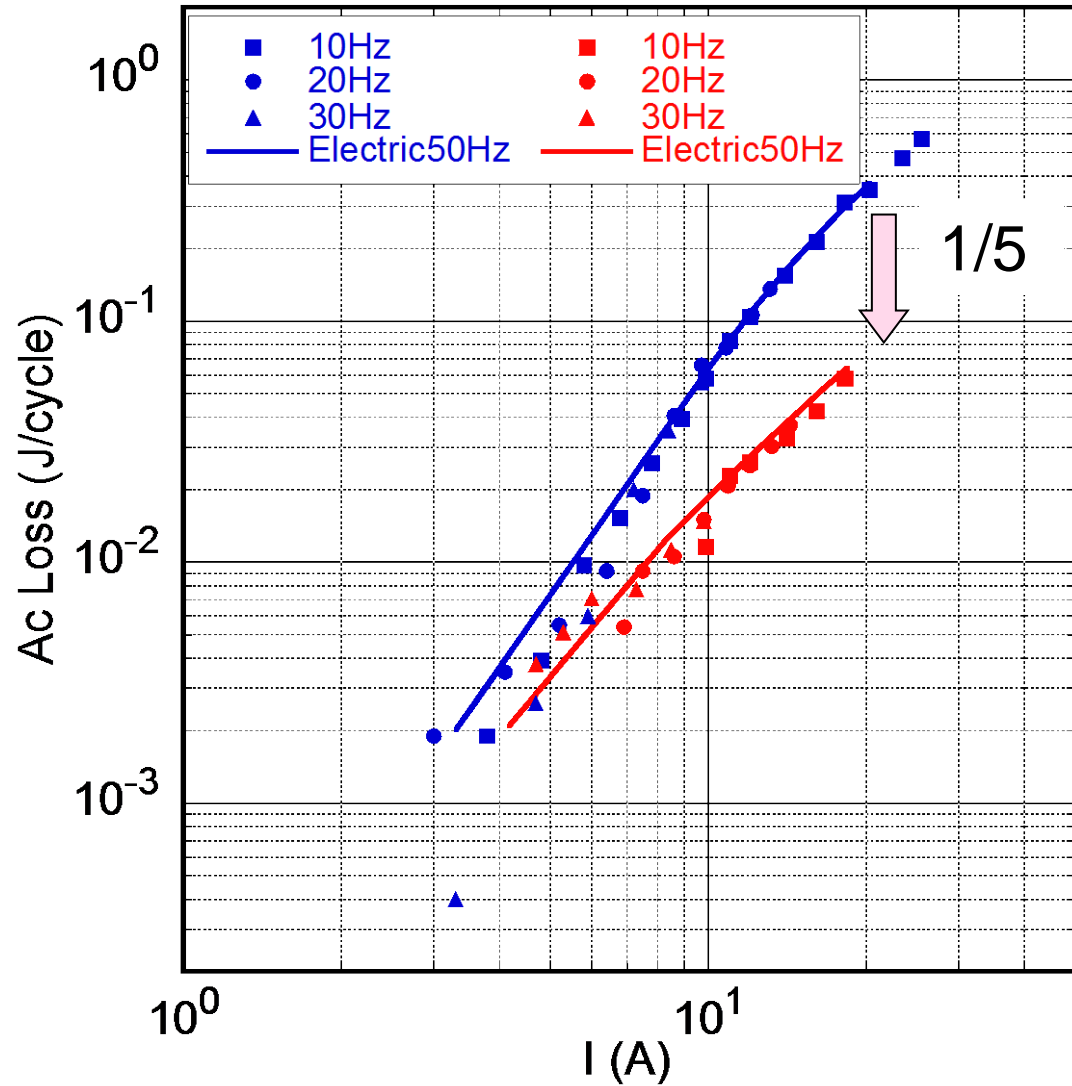
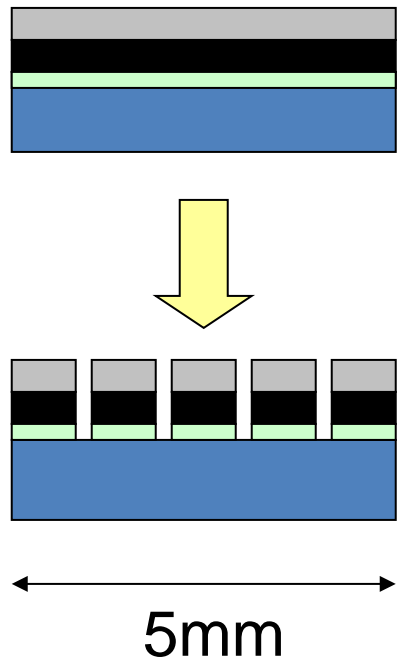
$\alpha, \gamma$ : pin parameter

$B_m$ : magnetic field amplitude



Ac loss in a short tape is reduced by scribing in inverse proportion to the number of filaments as theoretically predicted. → Nearly perfect insulation among the filaments

# 10-turn $\times$ 19-layer coil with 5mm wide 5-filament tape

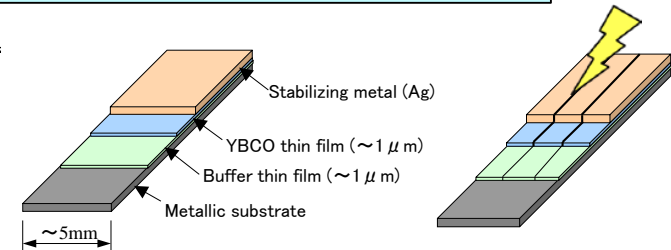




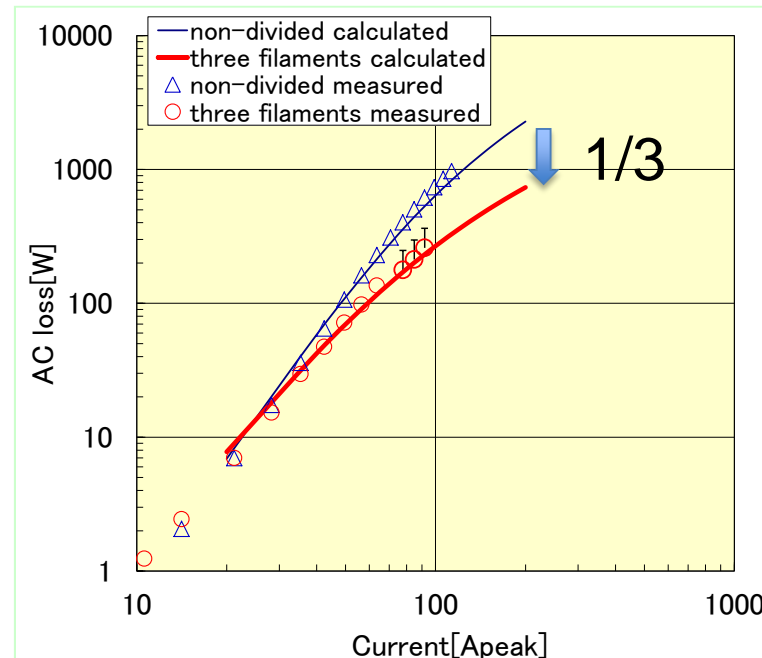
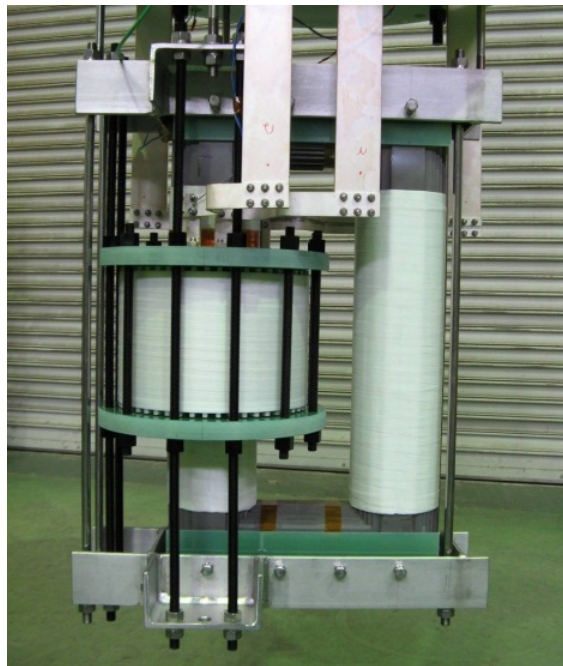
# Verification of ac loss reduction with small test transformers

## Parameters of Test Transformers for Ac loss Reduction

Capacity	215 kVA
Number of phase	1
Rated Voltage (Pri./Sec.)	1075 V / 1075 V
Rated Current (Pri./Sec.)	200 A / 200 A
Load	5.4 W
Inner diameter (Prim. /Second.)	183 mm / 128 mm
Outer diameter (Prim. /Second.)	226 mm / 171 mm
Height (Prim. /Second.)	107 mm
Turn number of each winding	20 turn x 20 layer = 400
1turn voltage	2.69
Total length of GdBCO tapes	445 m



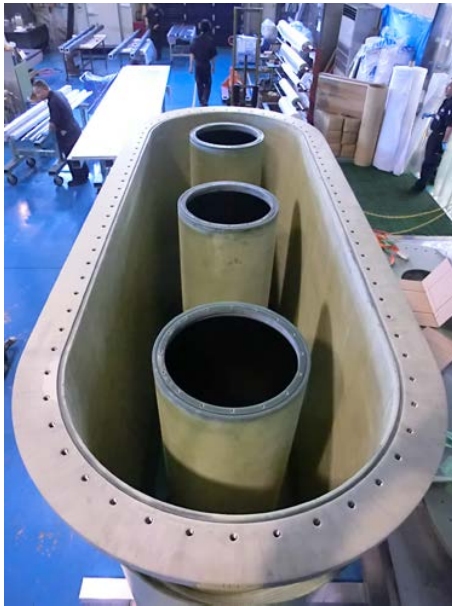
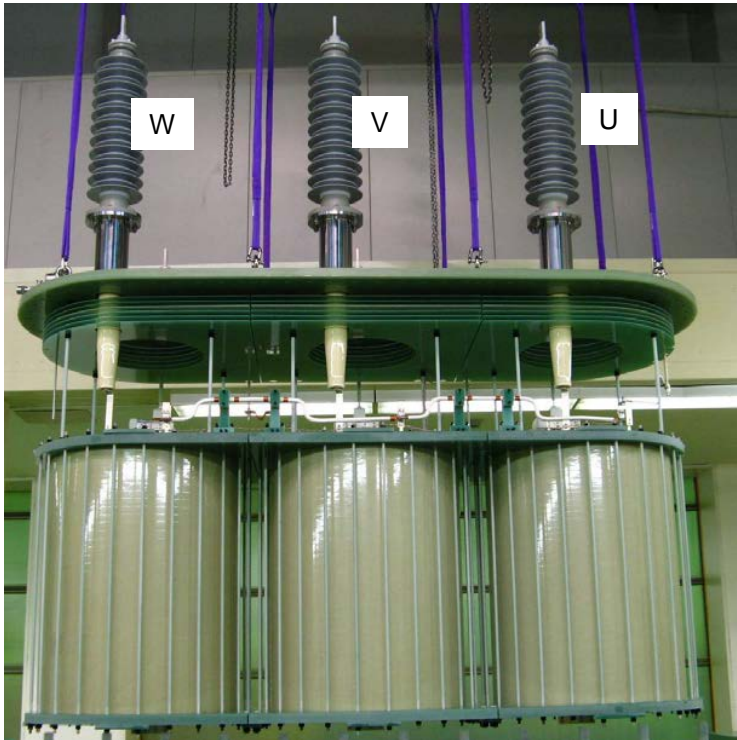
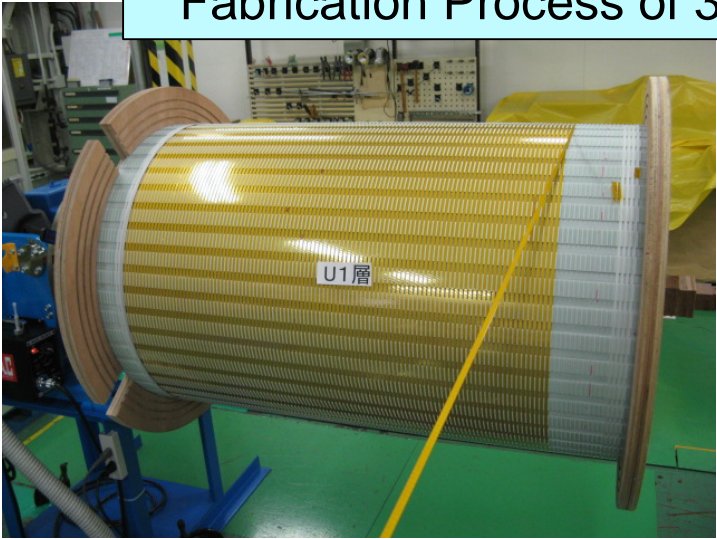
The present 1/10 model transformer was reduced only in current capacity as compared with the designed 20 MVA one. So the applied magnetic field was lower than the penetration field of the GdBCO tape. Hence we made small test transformers and verified the ac loss reduction by our technique.



3φ-66/6.9kV-  
2MVA SC Tr.



# Fabrication Process of 3 $\phi$ -66/6.9kV-2MVA superconducting transformer





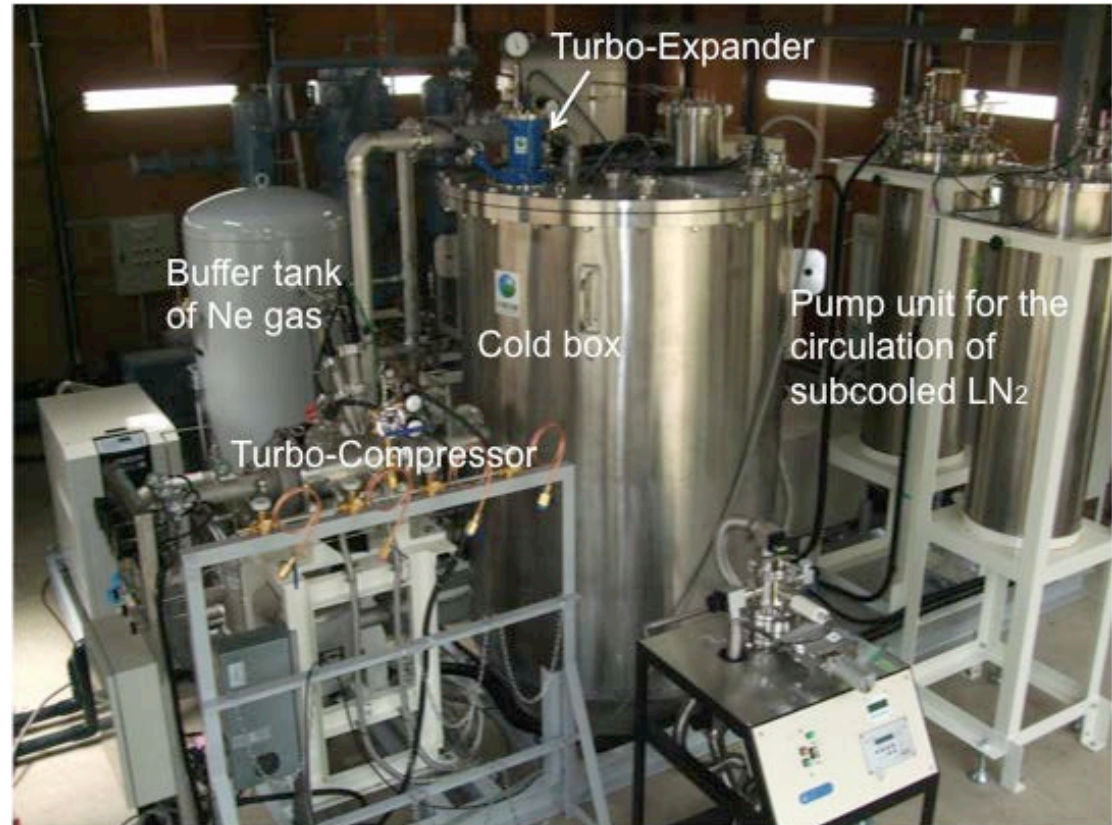
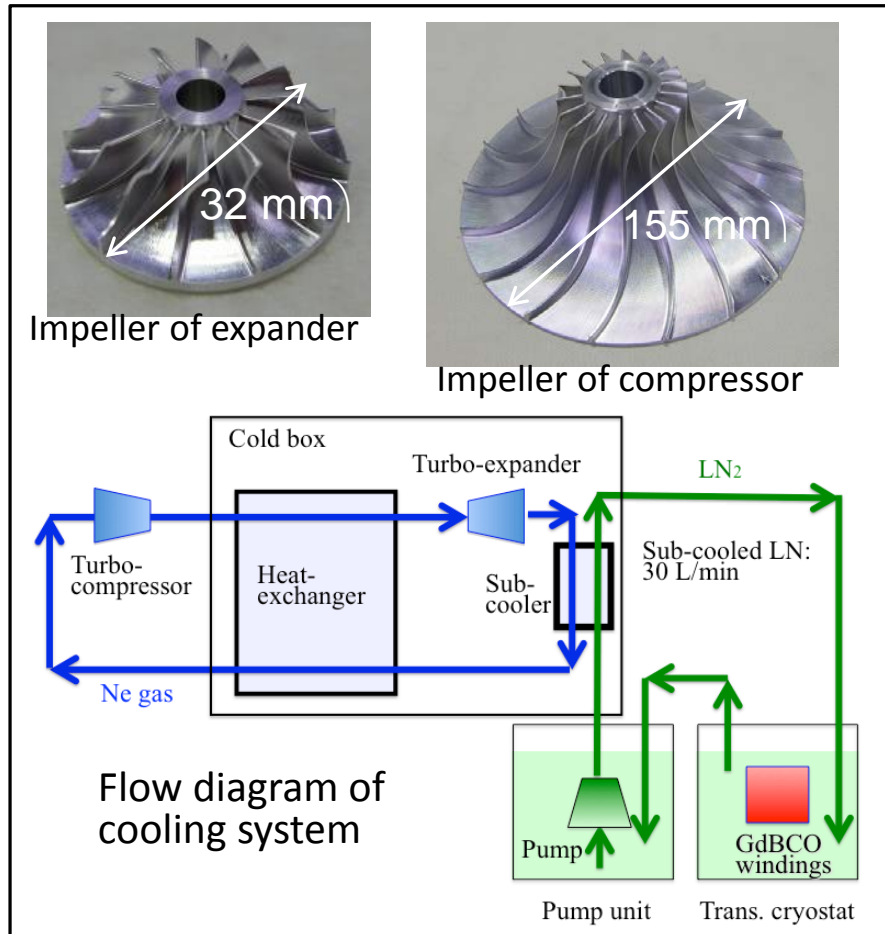
### 3) -66/6.9kV-2MVA superconducting transformer system



3) -66/6.9kV-2MVA  
GdBCO transformer

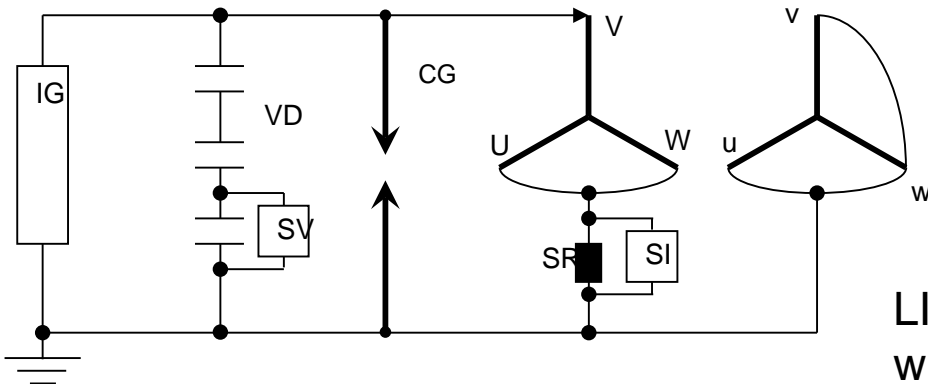
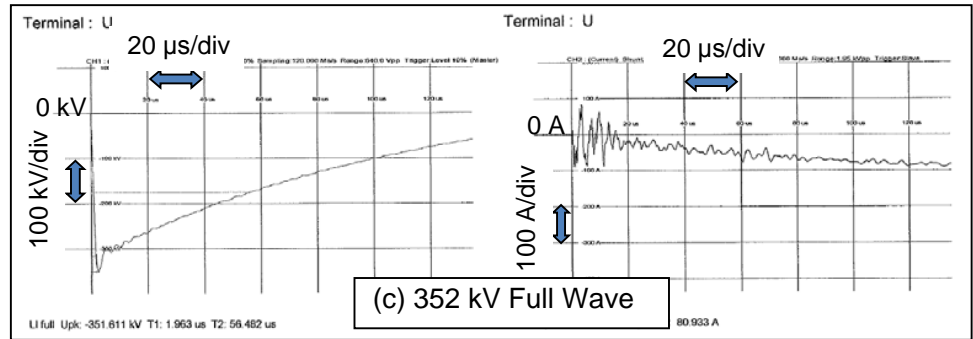
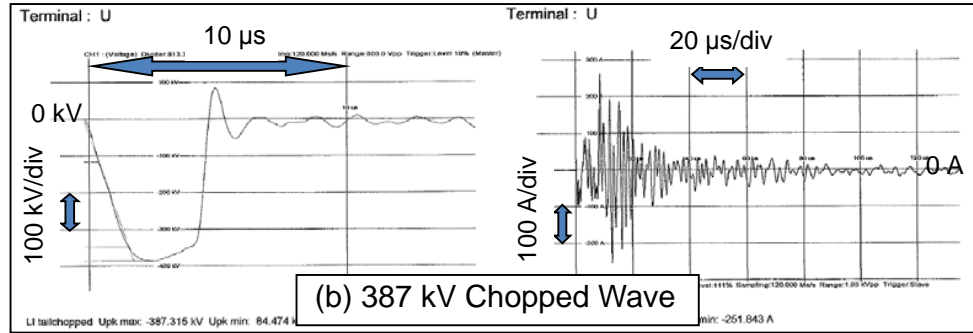
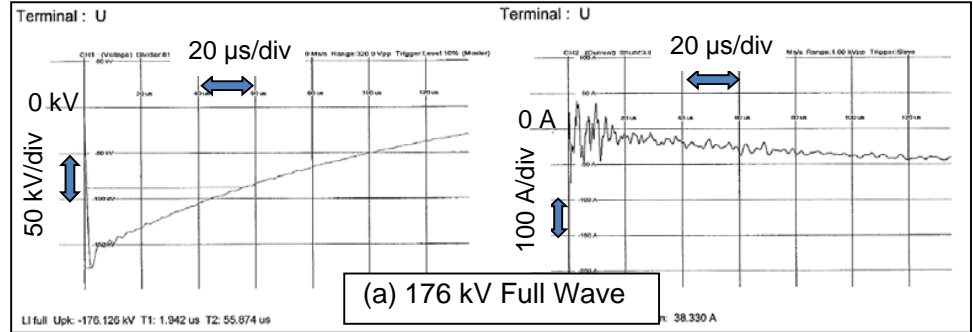
Ne turbo-Brayton  
refrigerator system

# Ne turbo-Brayton refrigerator system



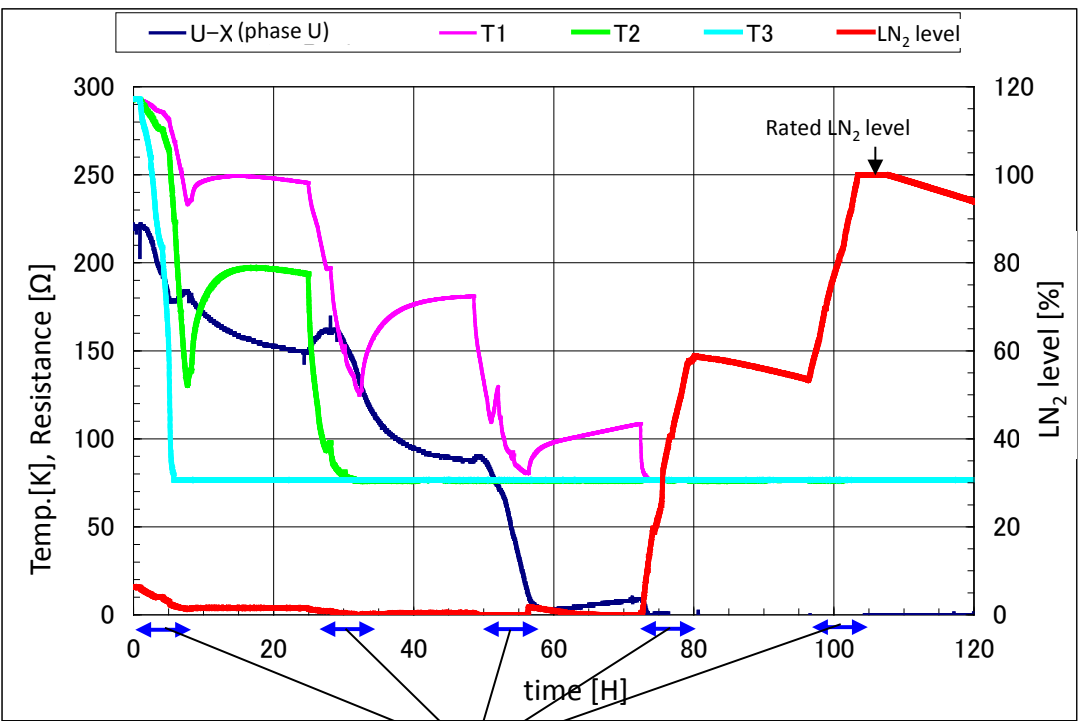


# Insulation test: 350kV Impulse, 140kV AC excess voltage

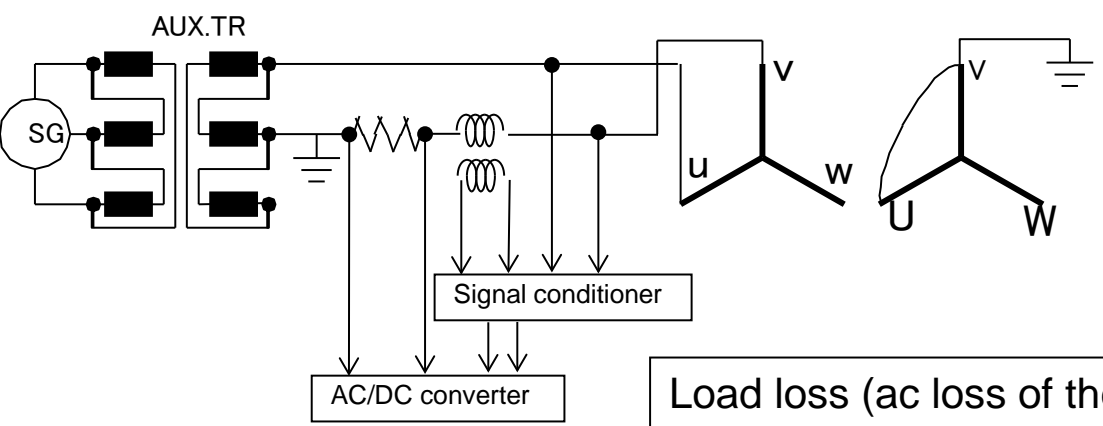
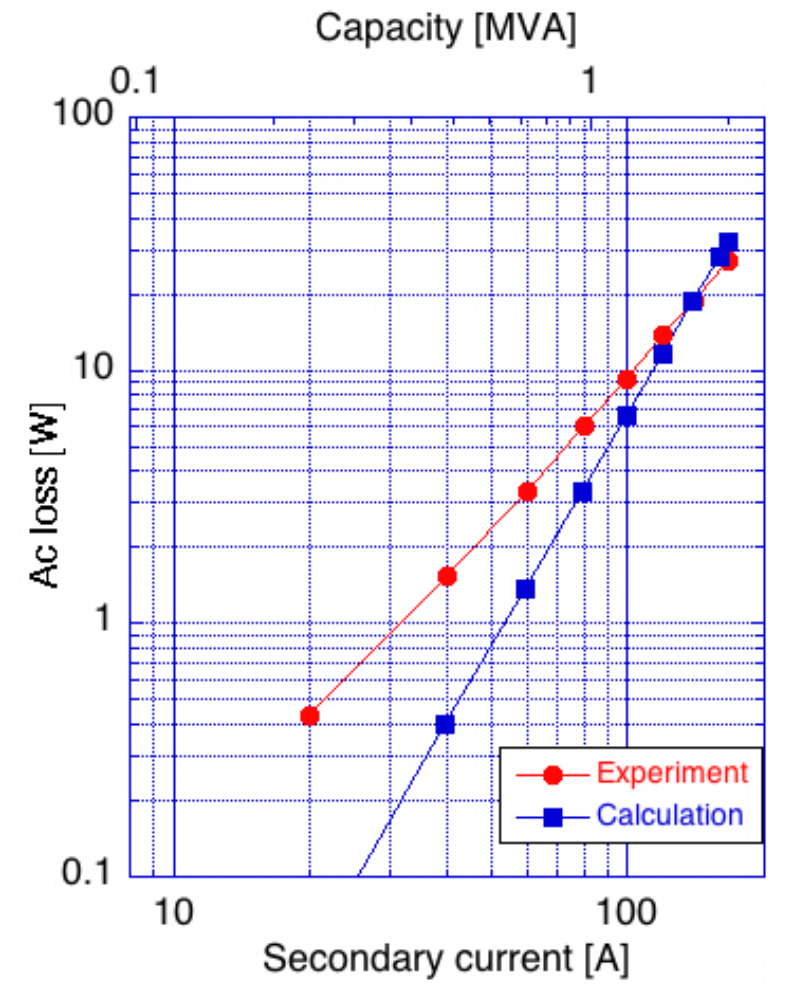


LIWL:350kV, Power frequency AC excess voltage  
 withstand level:140kV for 1 min.

# Bath-cooled with LN<sub>2</sub> at 77K and rated operation



Injecting time was 39 hours.  
 Injected LN<sub>2</sub> 4450 L, reserved LN<sub>2</sub> 2800 L

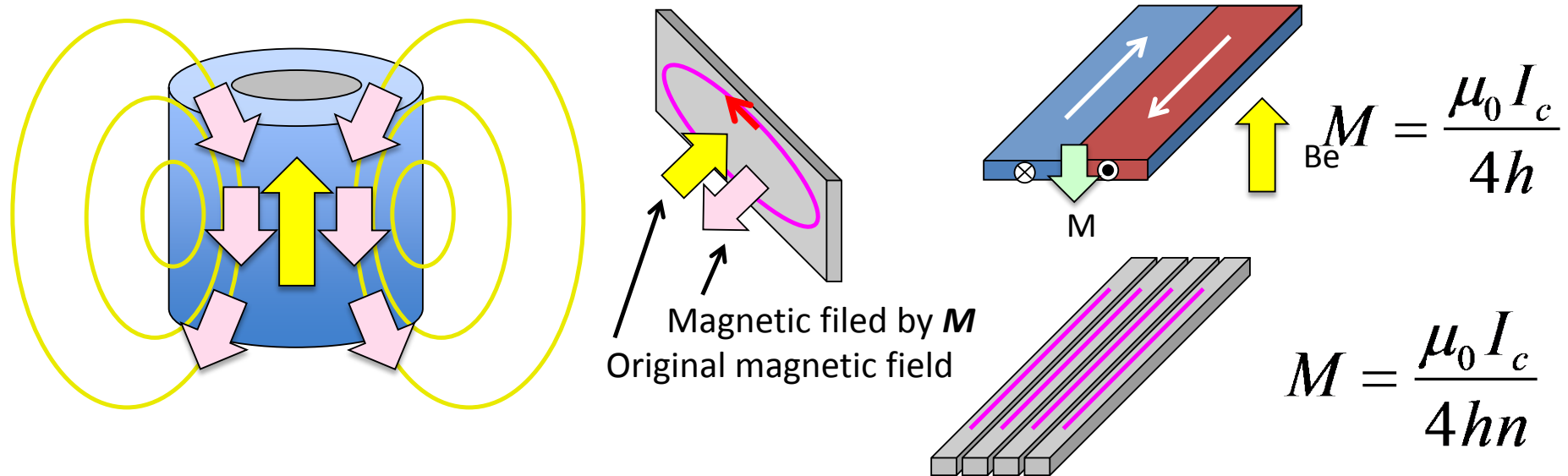


Load loss (ac loss of the windings) : 27W; No load loss (iron loss) : 8kW

# Magnetization reduction for dc use by scribing

1. M. Iwakuma et al., “New Method for Quick Decay of Shielding Current in REBCO Superconducting Coils”, IEEE Trans. Appl. Supercond., Vol. 26, No.4, 2016, Article No. 4403209.
2. M. Iwakuma et al., “Relaxation of Shielding Current in Test Coils for MRI with REBCO Superconducting Scribed Tapes”, IEEE Trans. Appl. Supercond., Vol. 26, No.3, 2016, Article No. 4401505.

# Uniformity of magnetic field under ppm order is required



Produced magnetic field by the induced shielding current disturbs the uniformity of original magnetic field in space.

Shielding current decays due to flux creep and/or flux flow.

Here magnetization,  $M$ , is defined as the magnetic moment,  $m$ , due to the induced shielding current per unit volume.

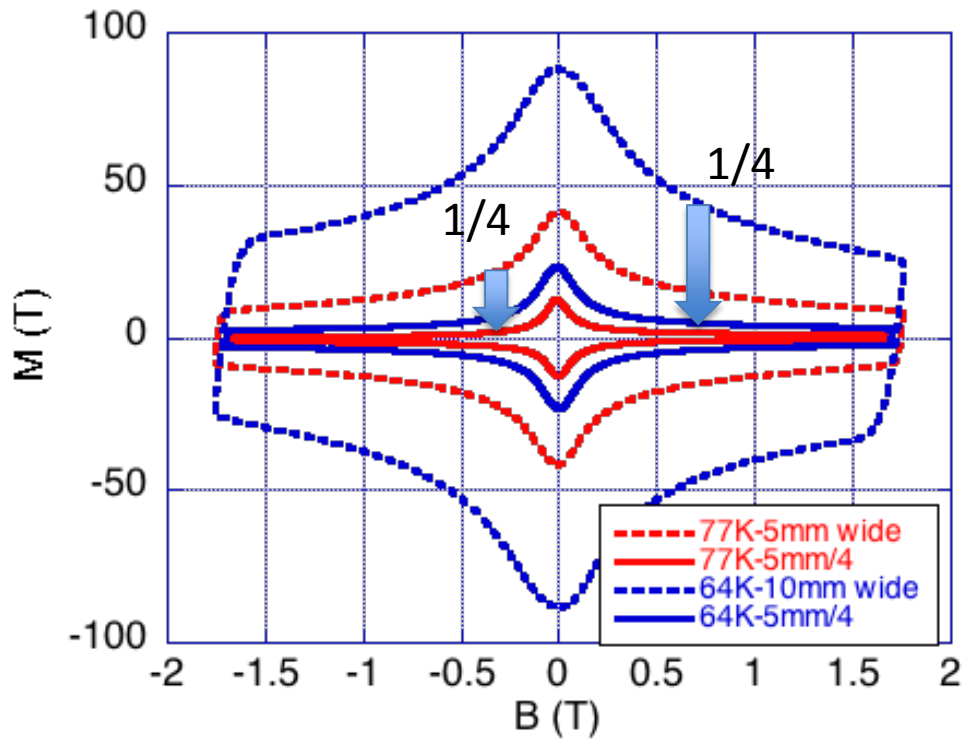
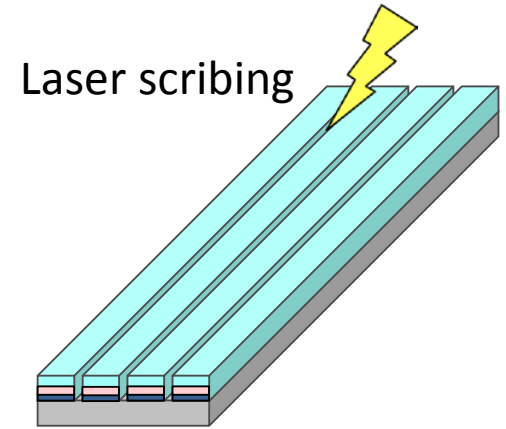
⇒ We can say  $M$  disturbs the uniformity of magnetic field in time and space.

⇒ It is necessary to reduce  $M$  itself for the uniformity of magnetic field.

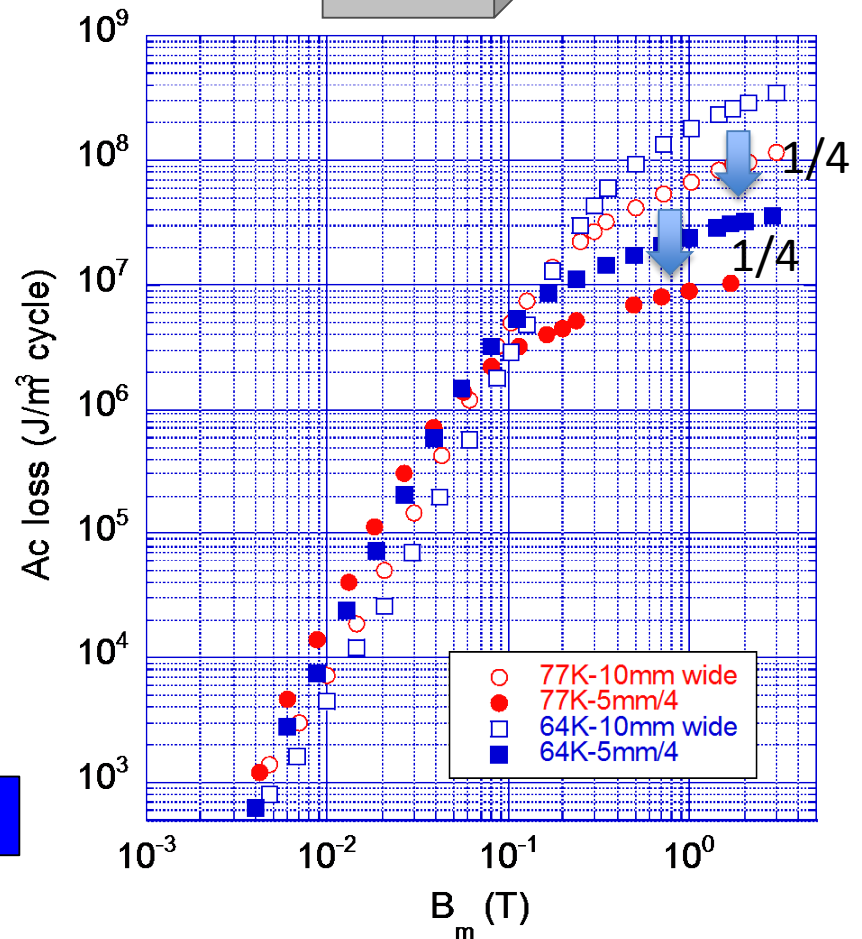


# M reduction = Ac Loss Reduction

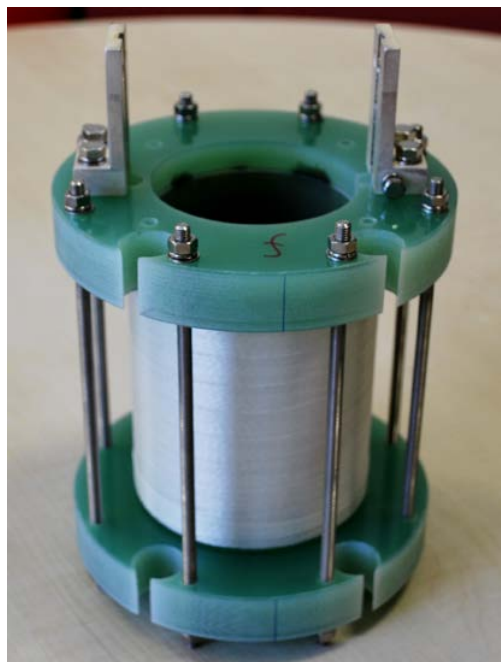
$$W = \oint H dM = -\oint M dH$$



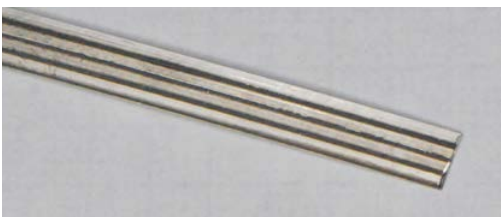
M reduction is made by scribing & special winding.



# Test Coils with Non-scribed GdBCO and Scribed EUBCO



19 turn x 6- or 20-layer Solenoid



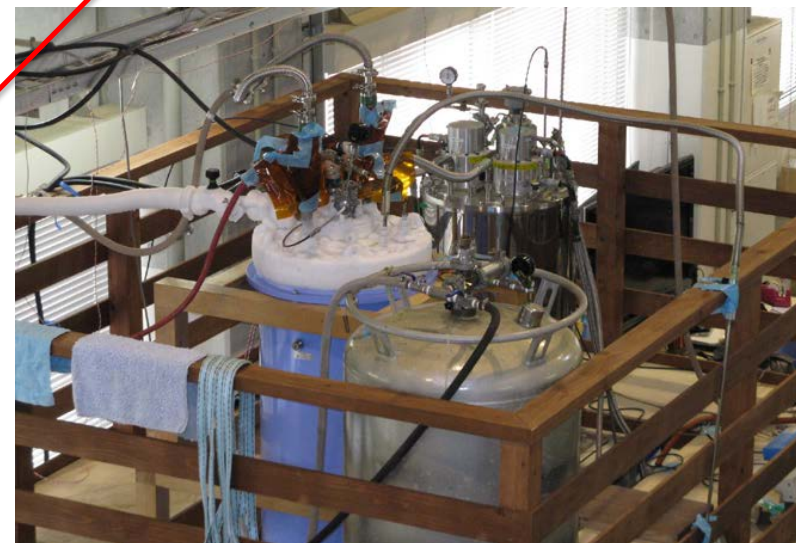
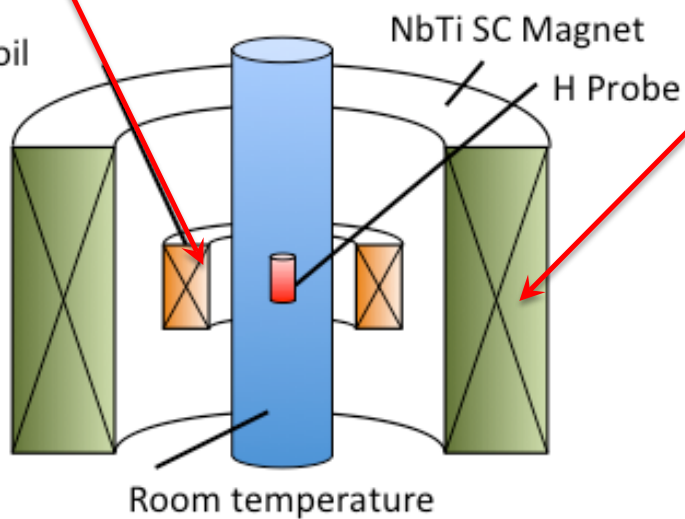
Scribed EuBCO Tape

Width of tape	5 mm
Thickness of tape	112 $\mu\text{m}$
Length of tape	100 m, 30 m
Substrate	Hastelloy (100 $\mu\text{m}$ )
Buffer layer	$\text{CeO}_2 + \text{LaMnO}_3 + \text{MgO} + \text{Y}_2\text{O}_3 + \text{Gd}_2\text{Zr}_2\text{O}_7$
Superconducting layer	GdBaCuO (1.6 $\mu\text{m}$ ), EuBCO+BaHfO <sub>3</sub> (1.52 $\mu\text{m}$ )
Number of filaments	1, 4
Ic of tape (@77K, s.f.)	219.5 A, >300 A
Winding	Solenoid (19 turn / layer, 20 or 6 layers)
Hight of winding	102 mm
Inner diameter of winding	80 mm
Outer diameter of winding	86.0 , 81.8 mm
Bobbin	GFRP
Produced magnetic field	3.42 mT/A, 1.14 mT/A
Ic of coil (@77K)	75A, 140A

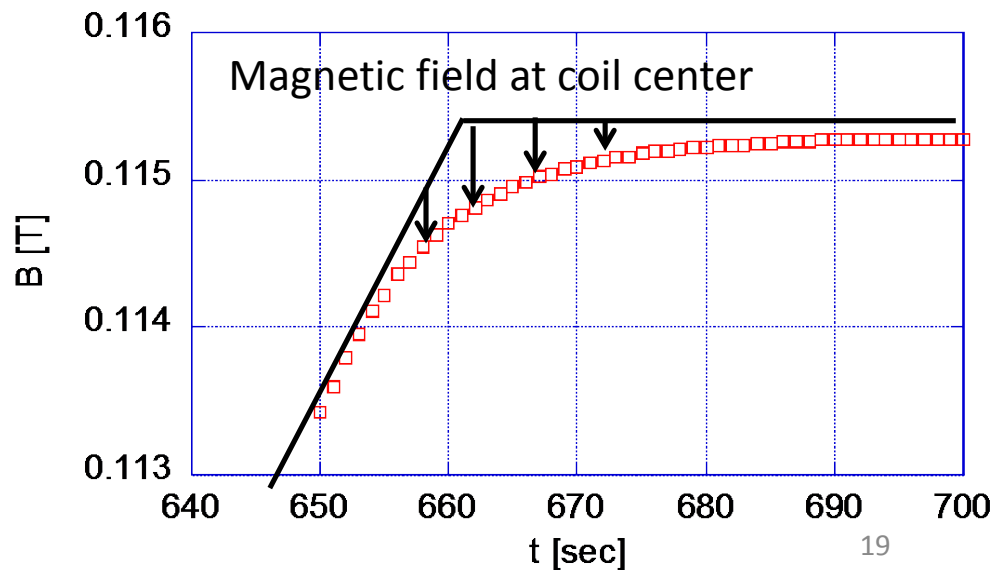
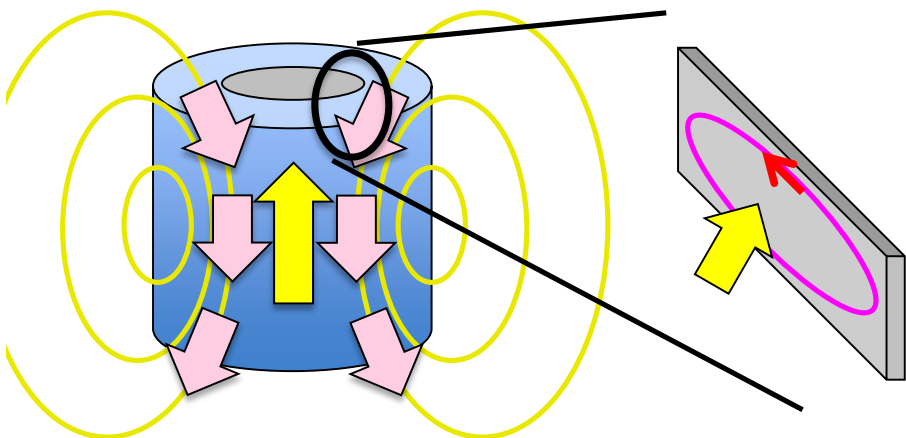
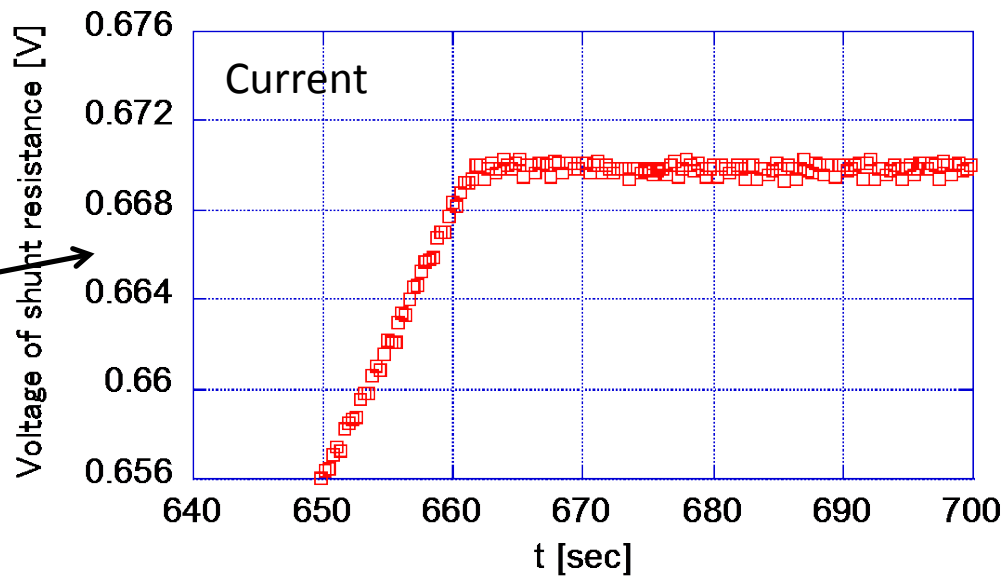
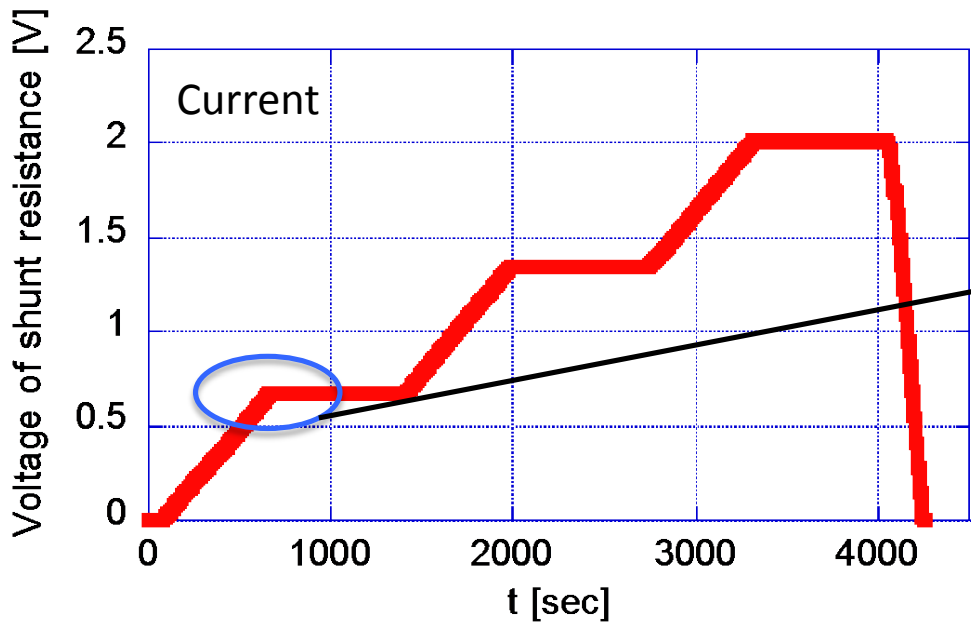
# Experimental Setup (in background field by NbTi Magnet)



REBCO Sample Coil

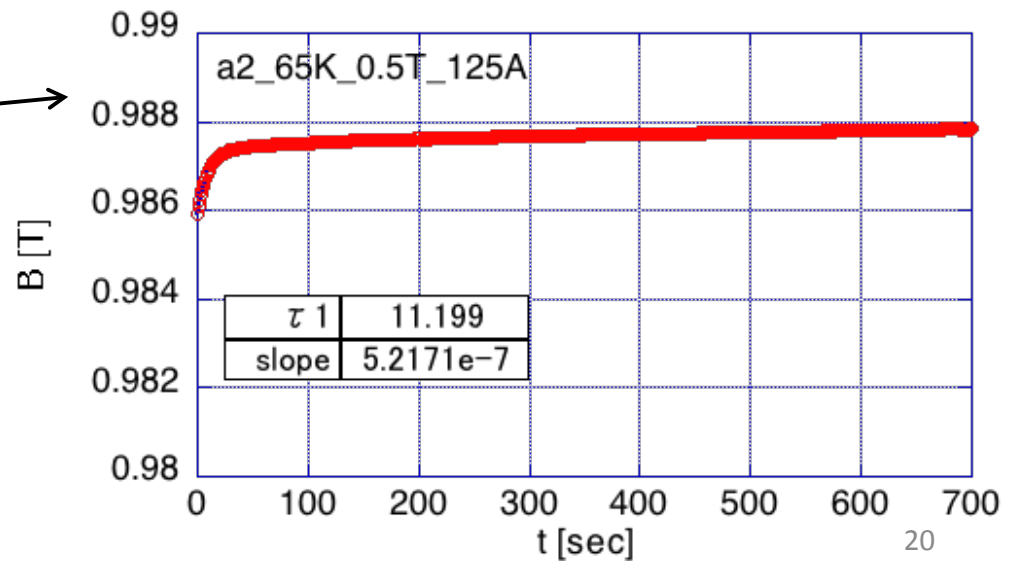
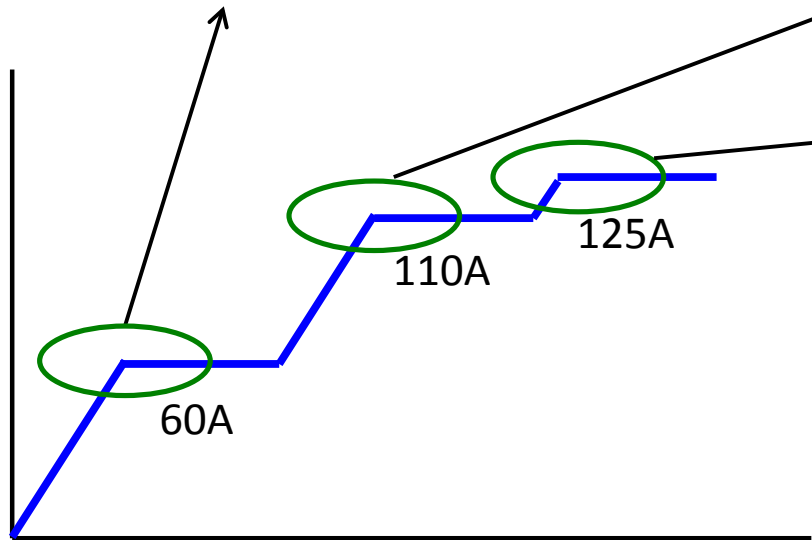
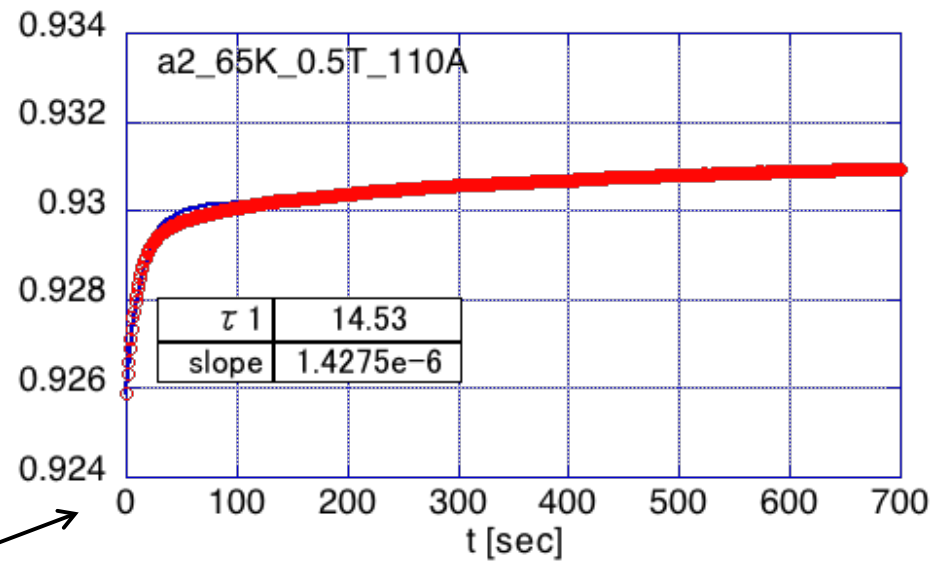
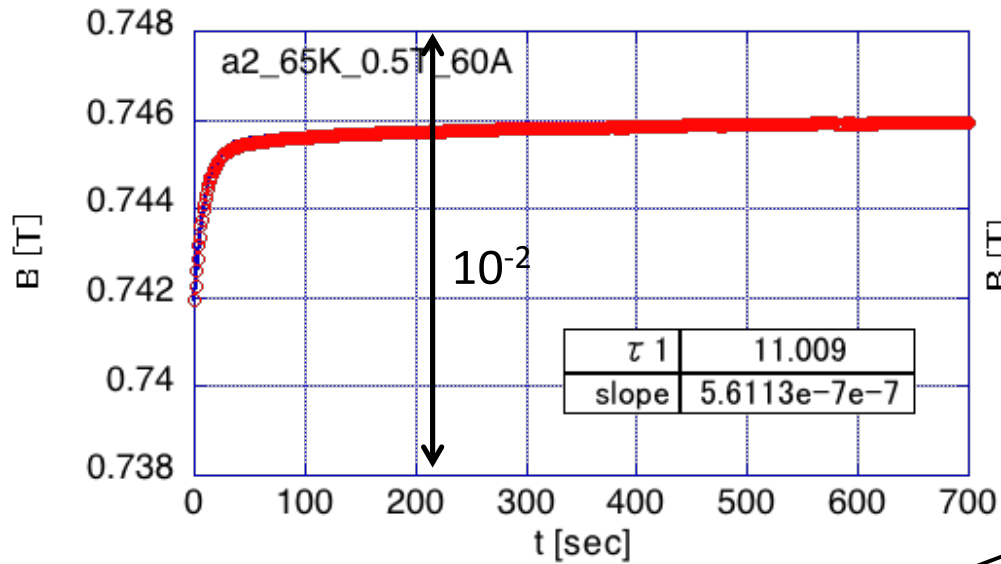


# Variation of Current and Magnetic Field

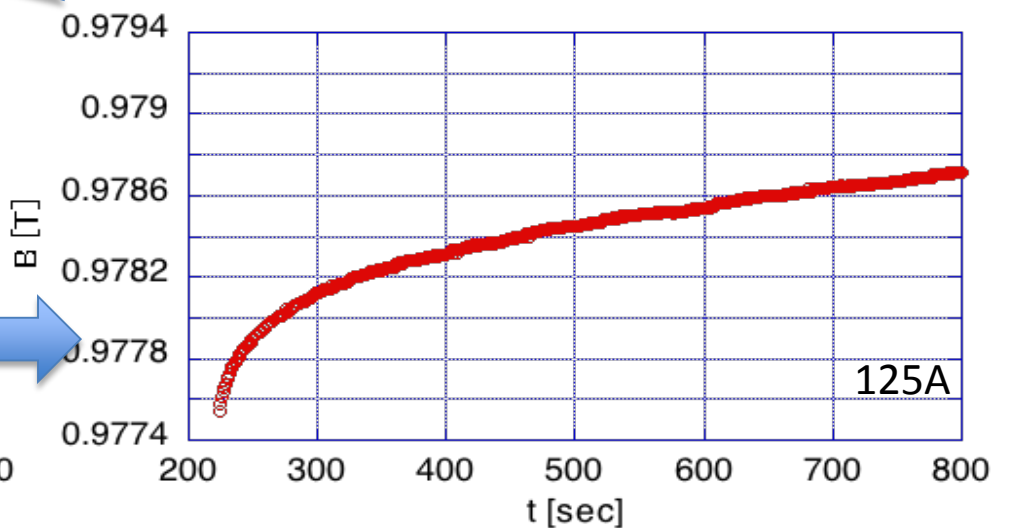
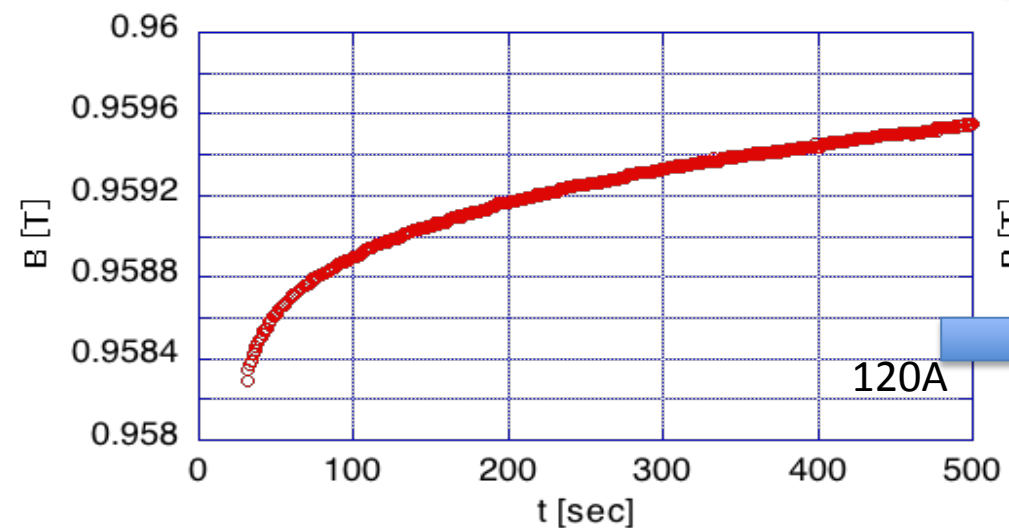
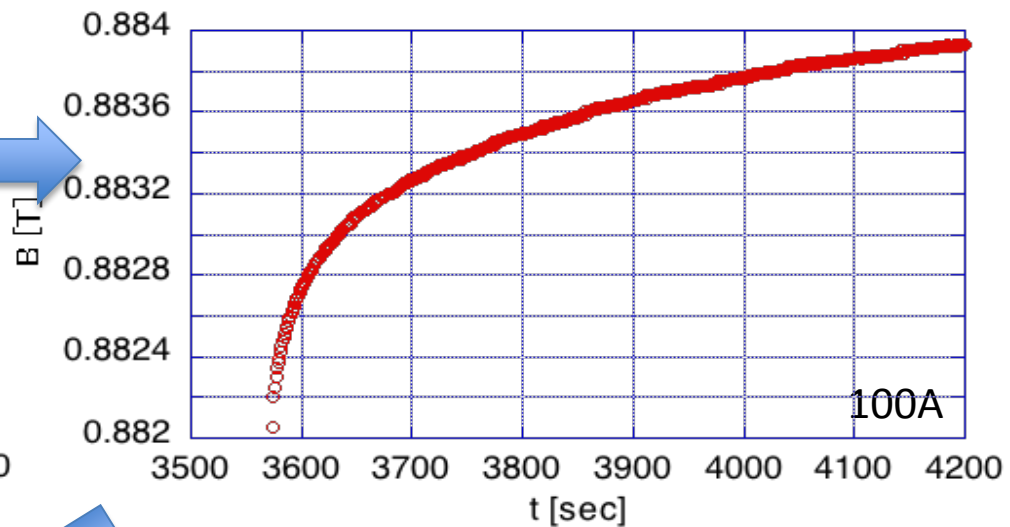
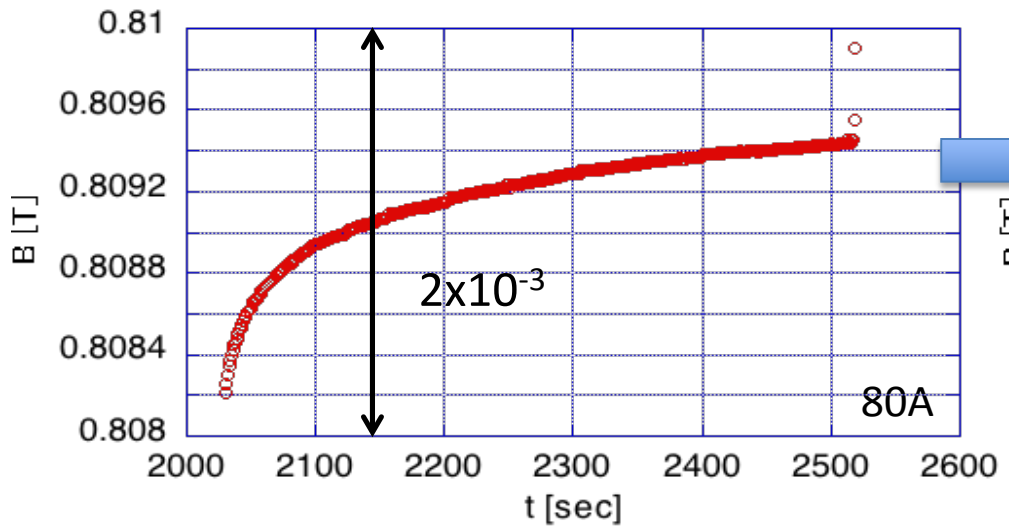




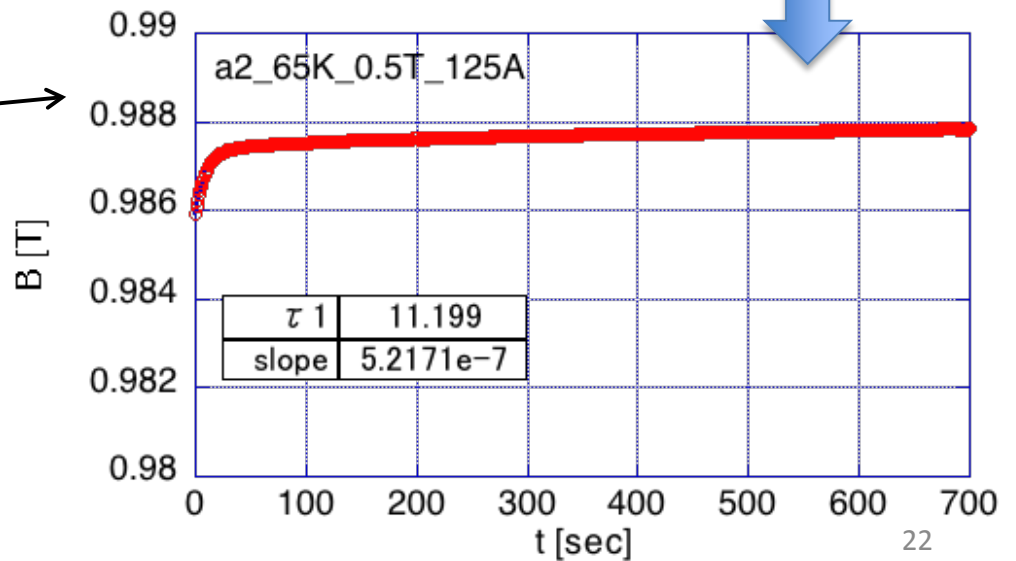
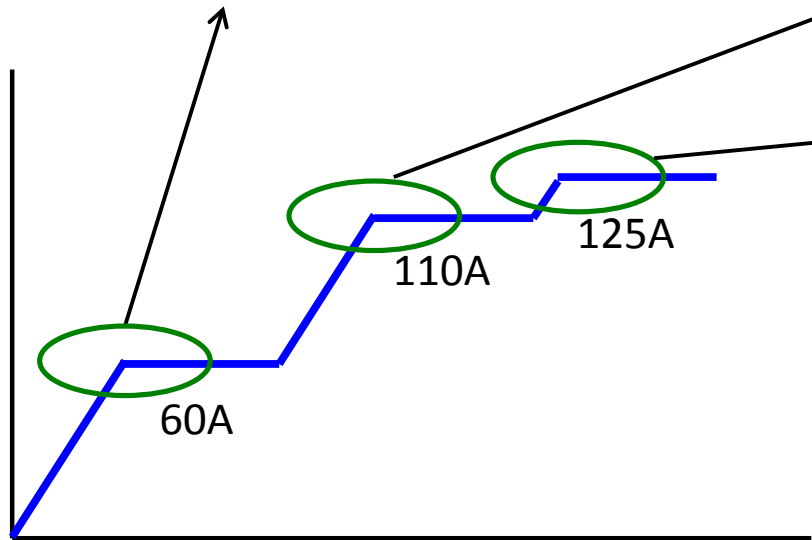
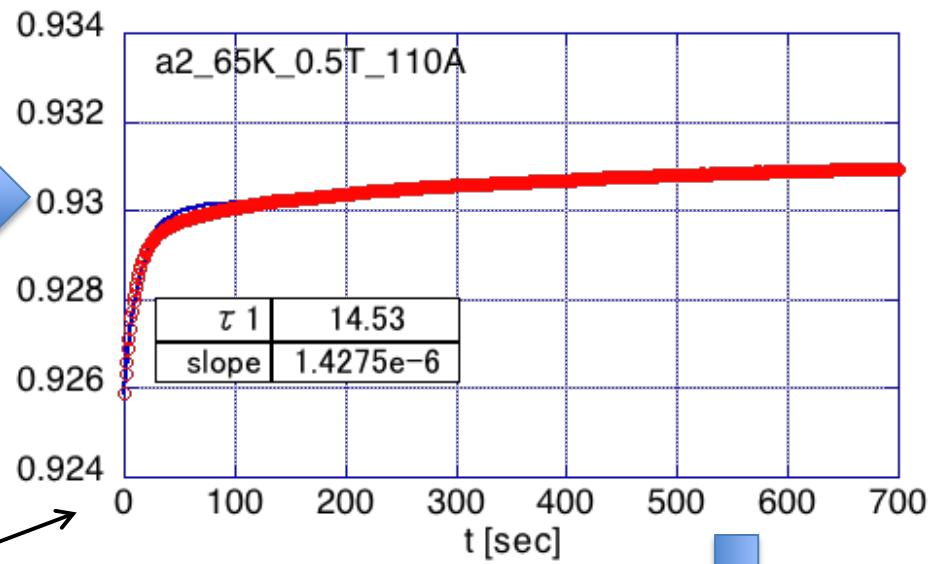
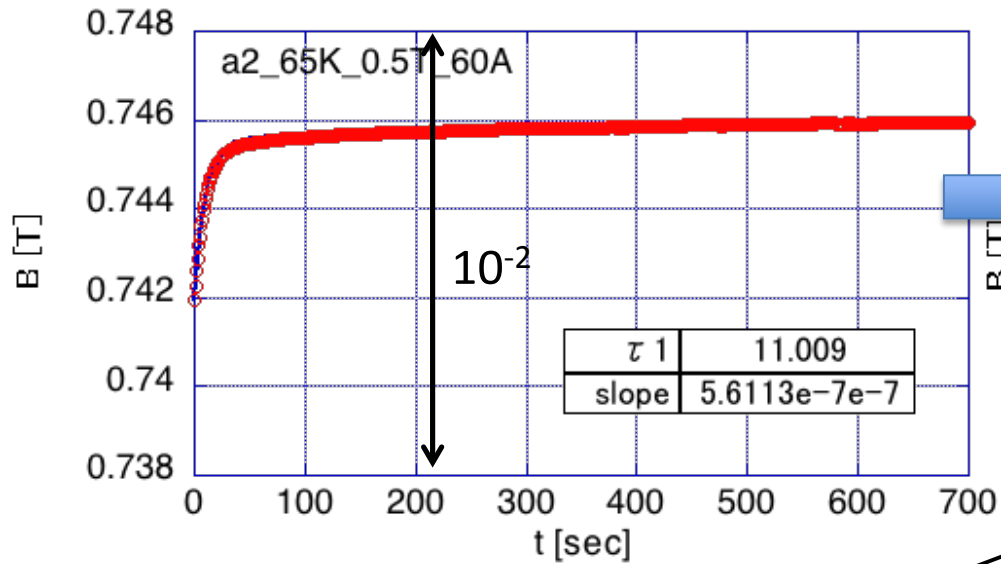
# 65K, 0.5T (GbBCO 100m, 19-turn, 20-layer)



# 65K, 0.5T (GbBCO 100m, 19-turn, 20-layer)

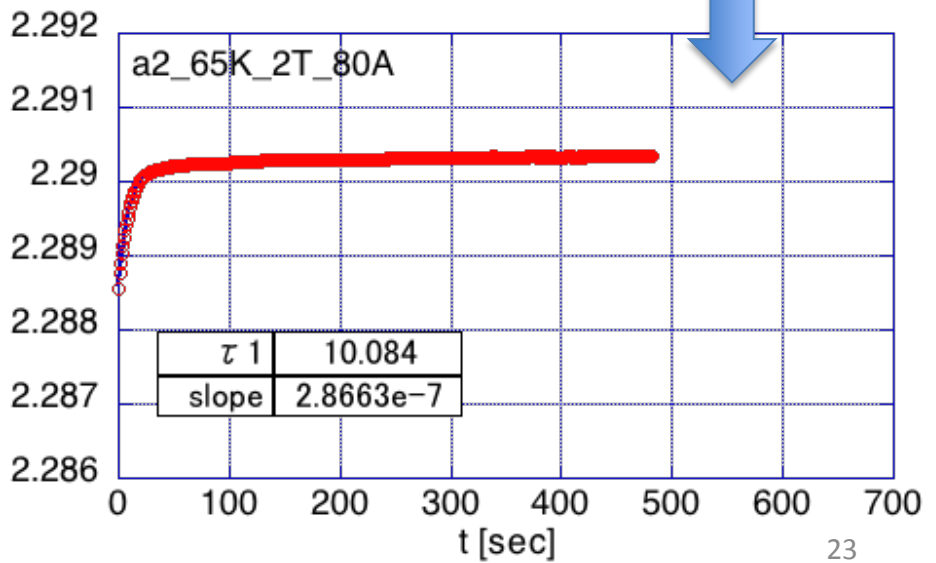
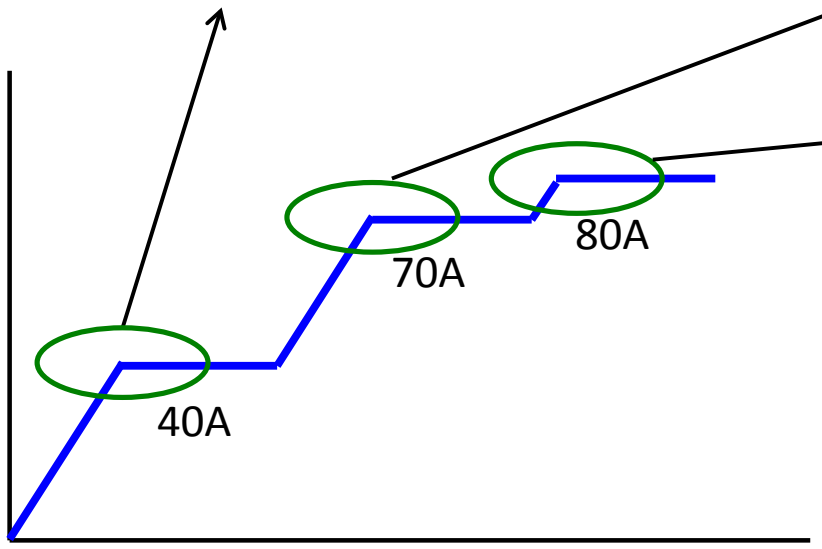
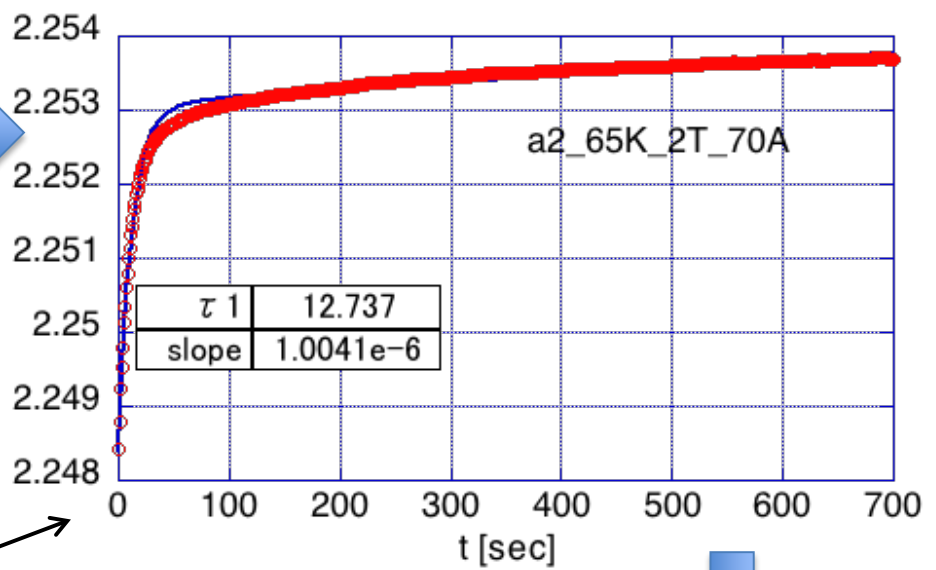
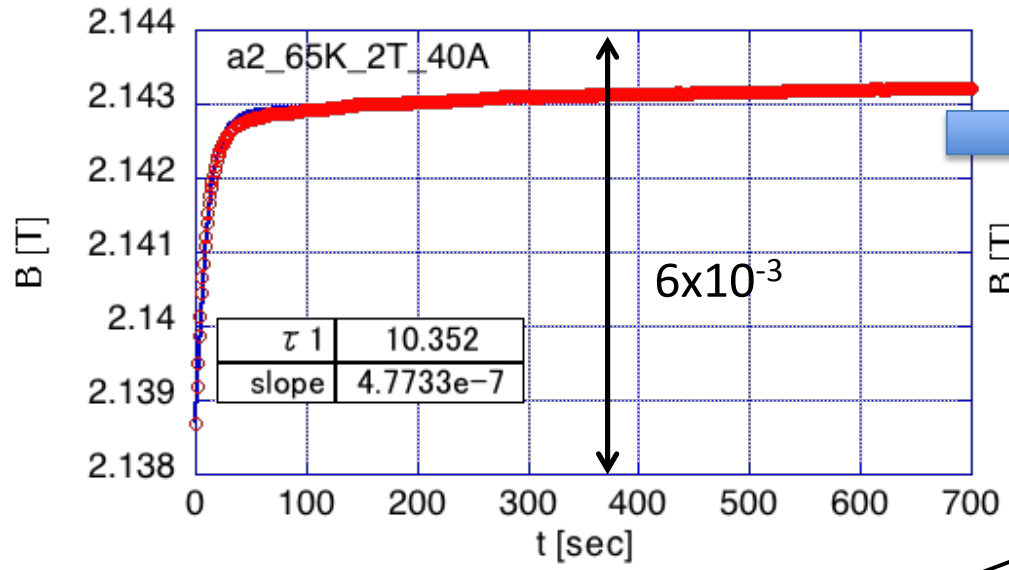


# 65K, 0.5T (GbBCO 100m, 19-turn, 20-layer)





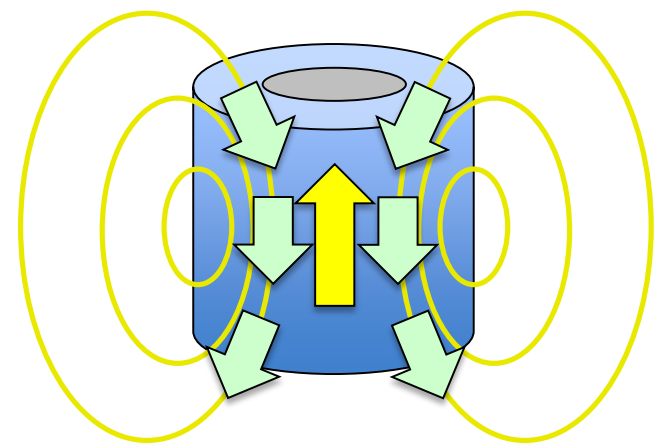
# 65K, 2T (GbBCO 100m, 19-turn, 20-layer)



# Analysis

$$B_{center} = B_0 + B_1 \left( 1 - e^{-\frac{t}{\tau_1}} \right) + B_2 \left( 1 - e^{-\frac{t}{\tau_2}} \right) + \dots$$

Contribution by each turn or each part



In the case of decay time constant  $\tau \gg t$

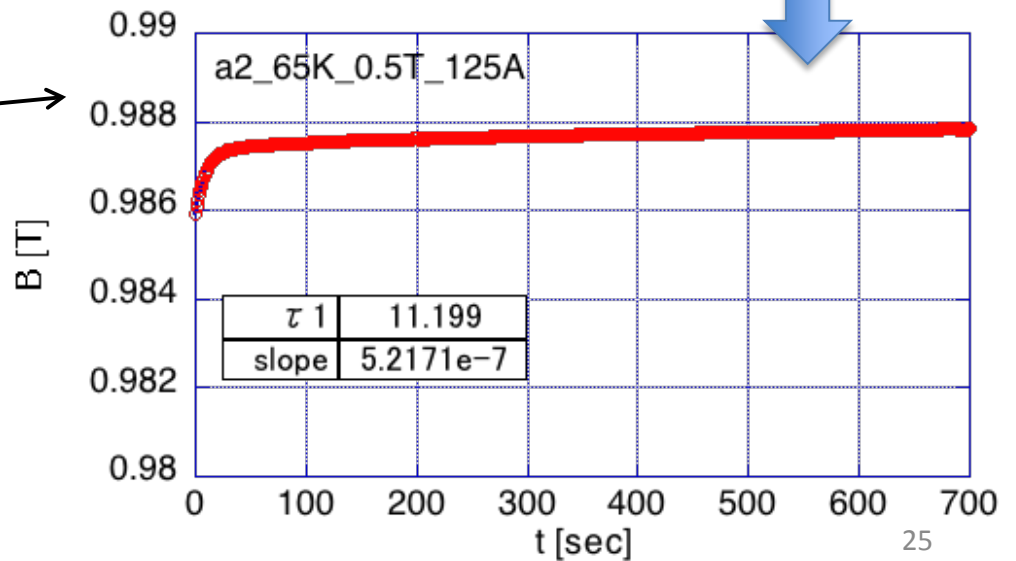
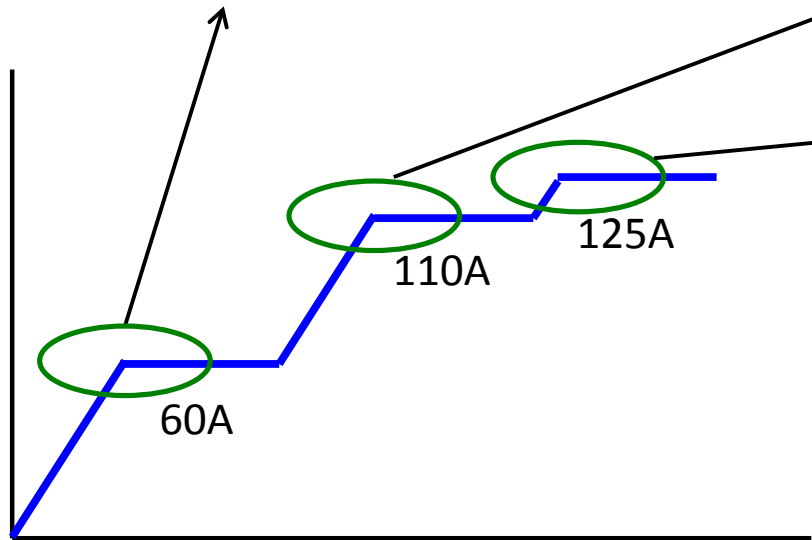
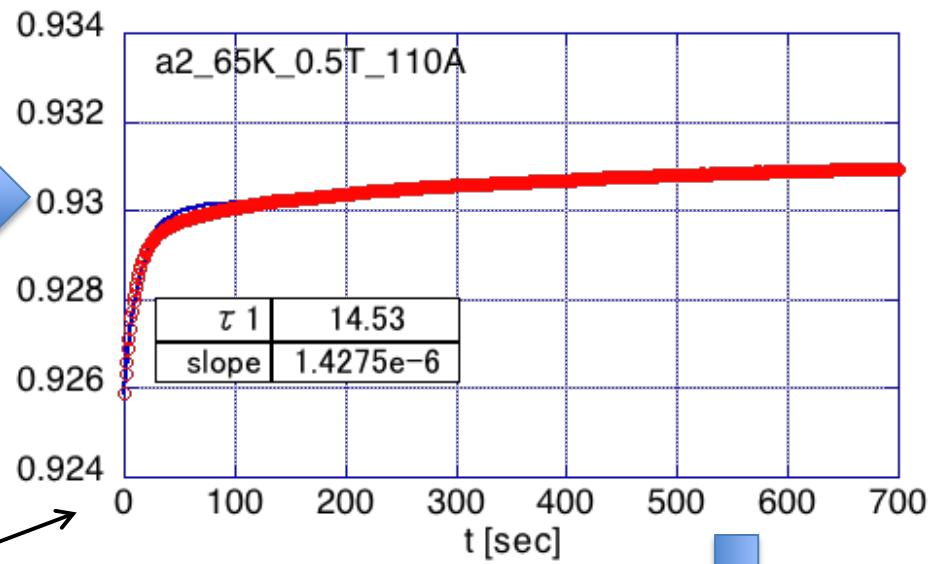
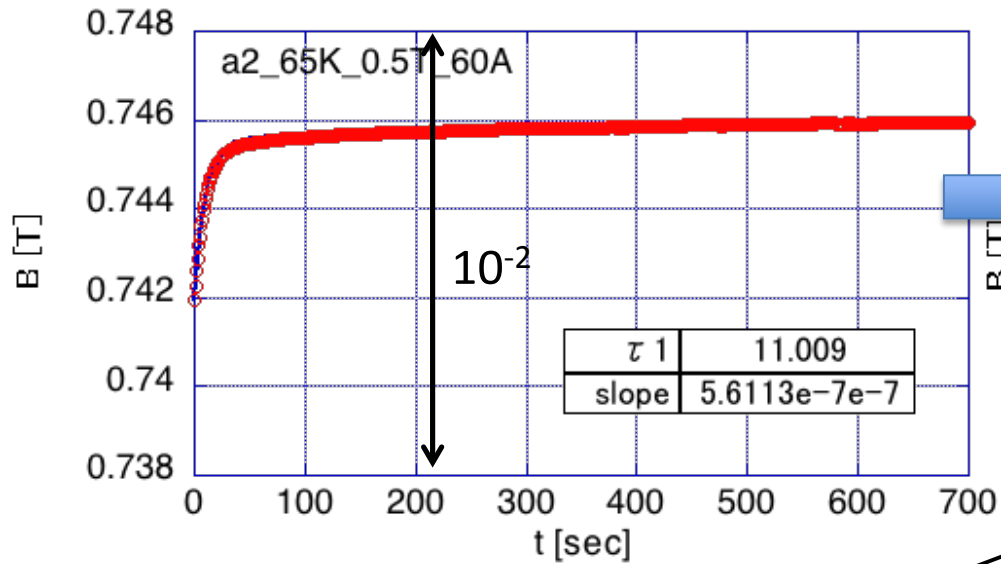
$$B_i \left( 1 - e^{-\frac{t}{\tau_i}} \right) = B_i \left( 1 - \left( 1 - \frac{t}{\tau_i} + \frac{1}{2!} \left( \frac{t}{\tau_i} \right)^2 - \frac{1}{3!} \left( \frac{t}{\tau_i} \right)^3 + \dots \right) \right)$$

$$= B_i \frac{t}{\tau_i}$$

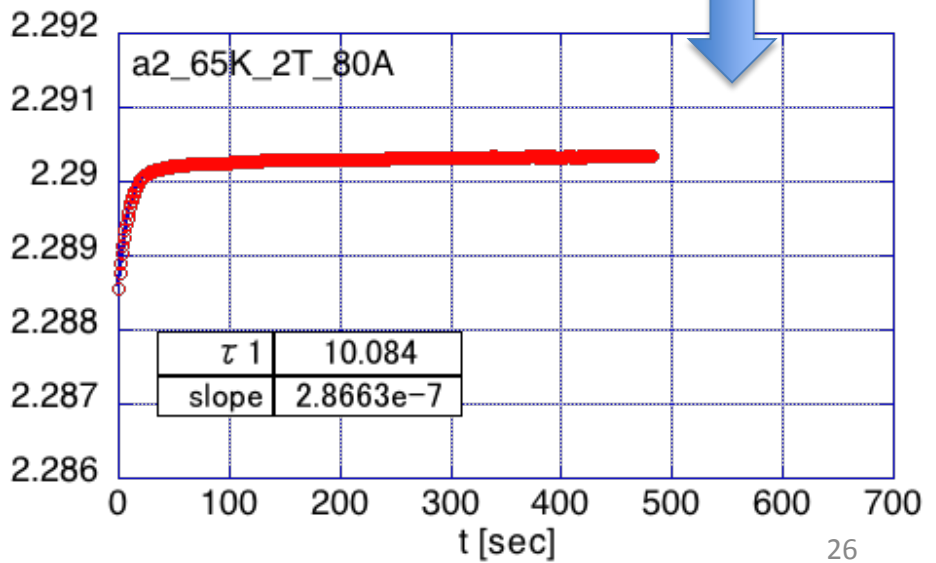
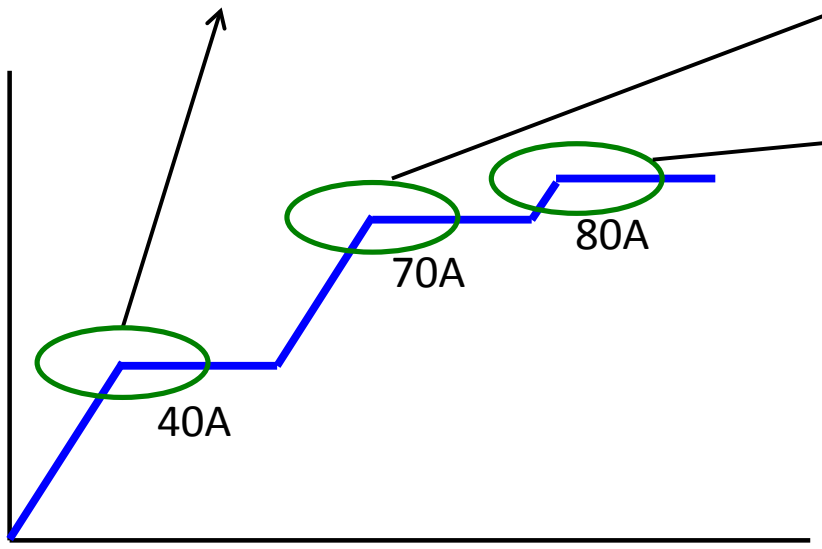
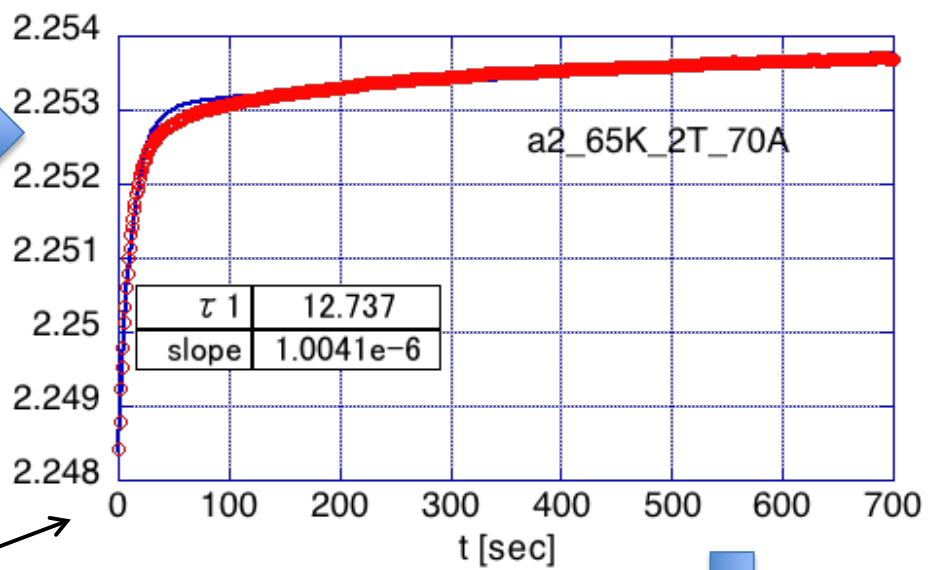
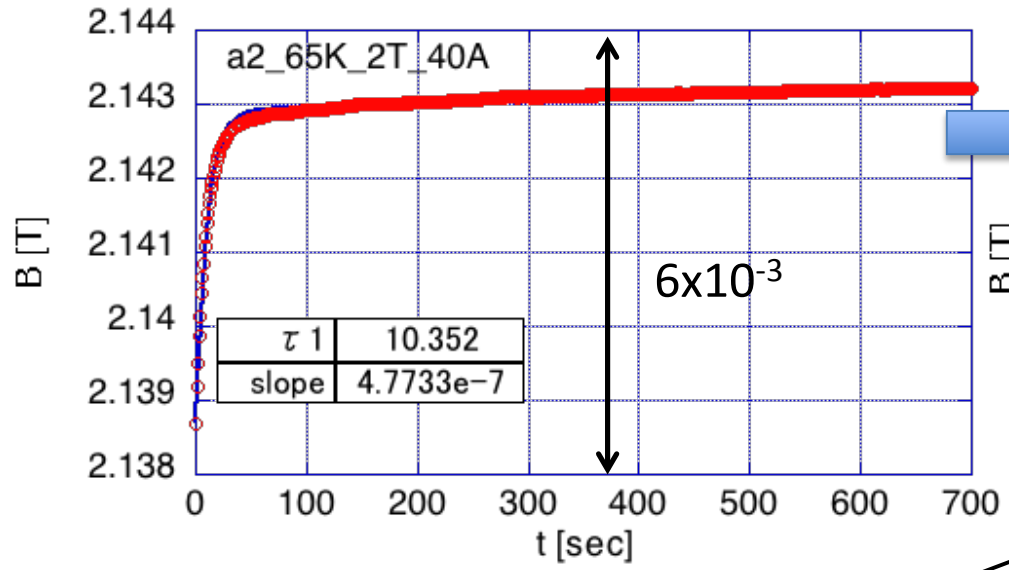
$$B_{center} = B_0 + B_1 \left( 1 - e^{-\frac{t}{\tau_1}} \right) + B_2 t$$

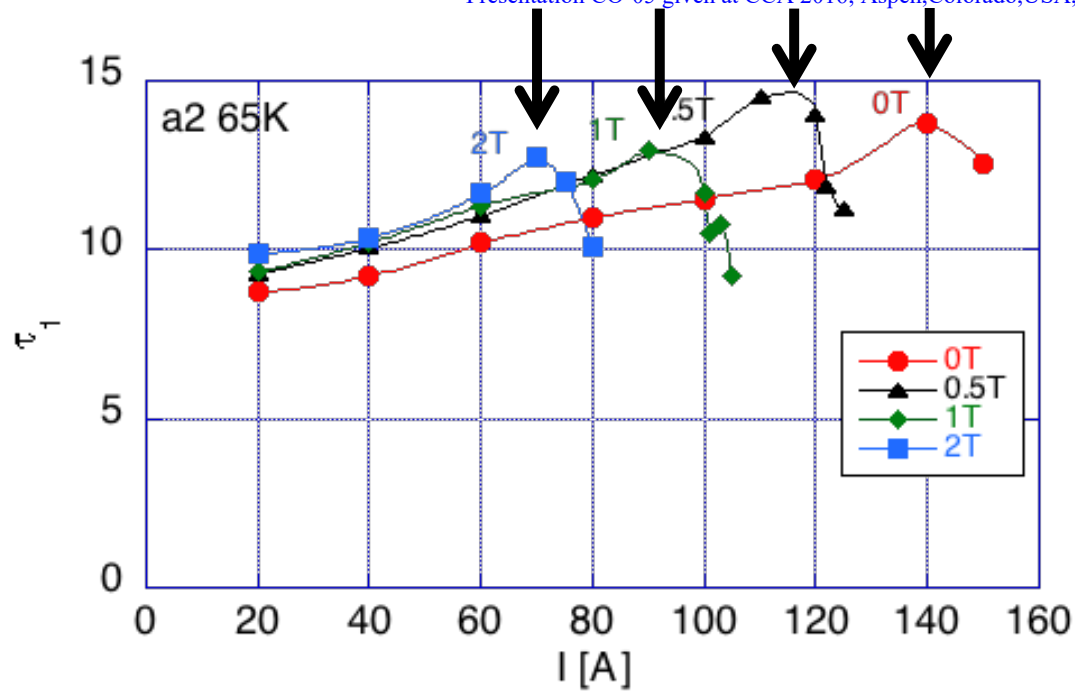
Let us pay attention to decay time constant,  $\tau_1$ , and gradient of linear part,  $B_2$

# 65K, 0.5T (GbBCO 100m, 19-turn, 20-layer)



# 65K, 2T (GbBCO 100m, 19-turn, 20-layer)

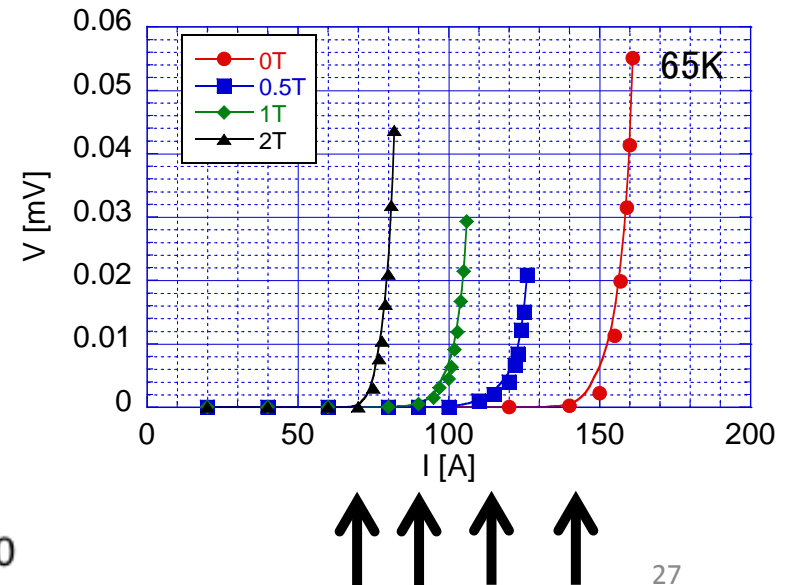
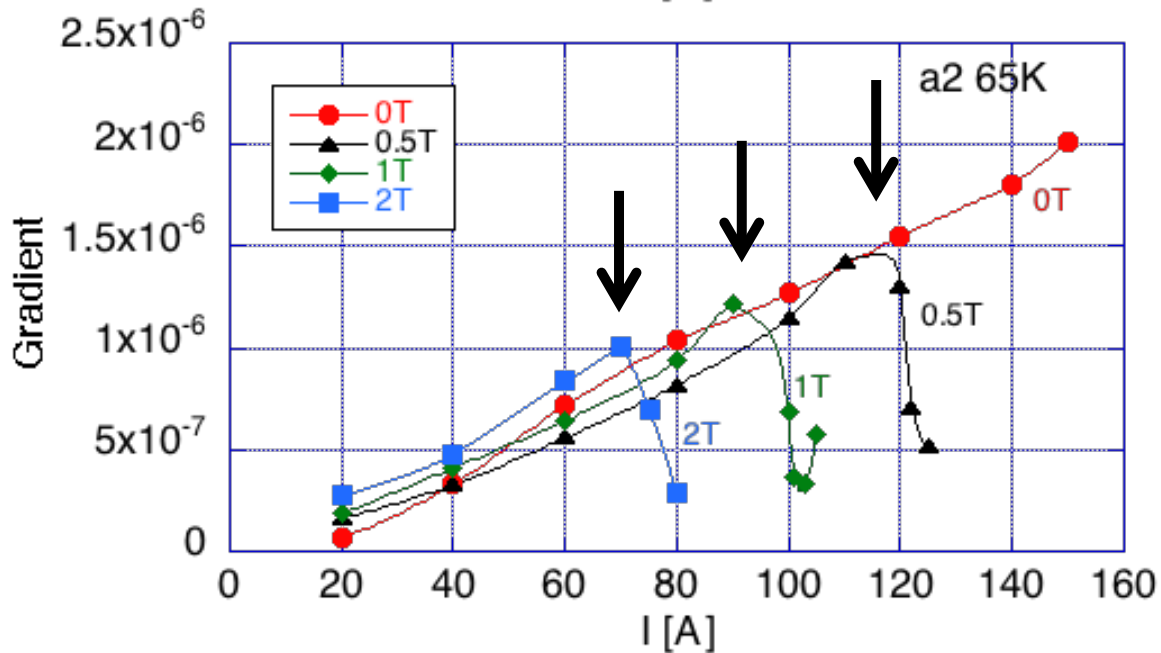




$$B_{center} = B_0 + B_1 \left( 1 - e^{-\frac{t}{T_1}} \right) + B_2 t$$

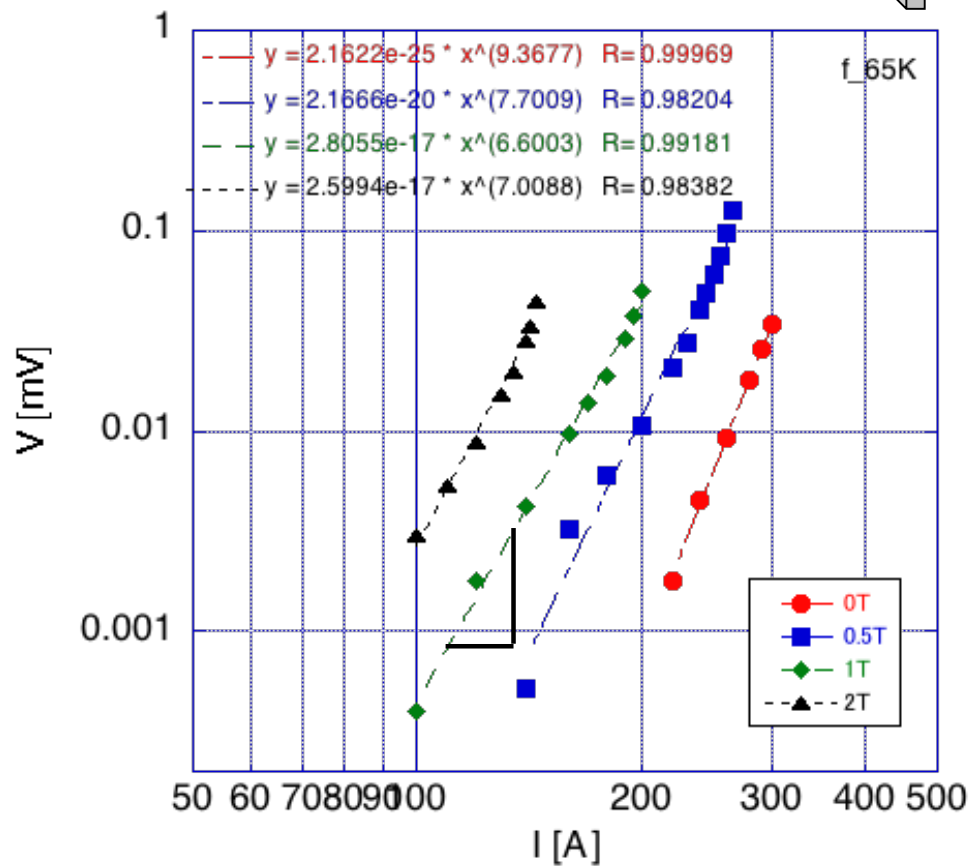
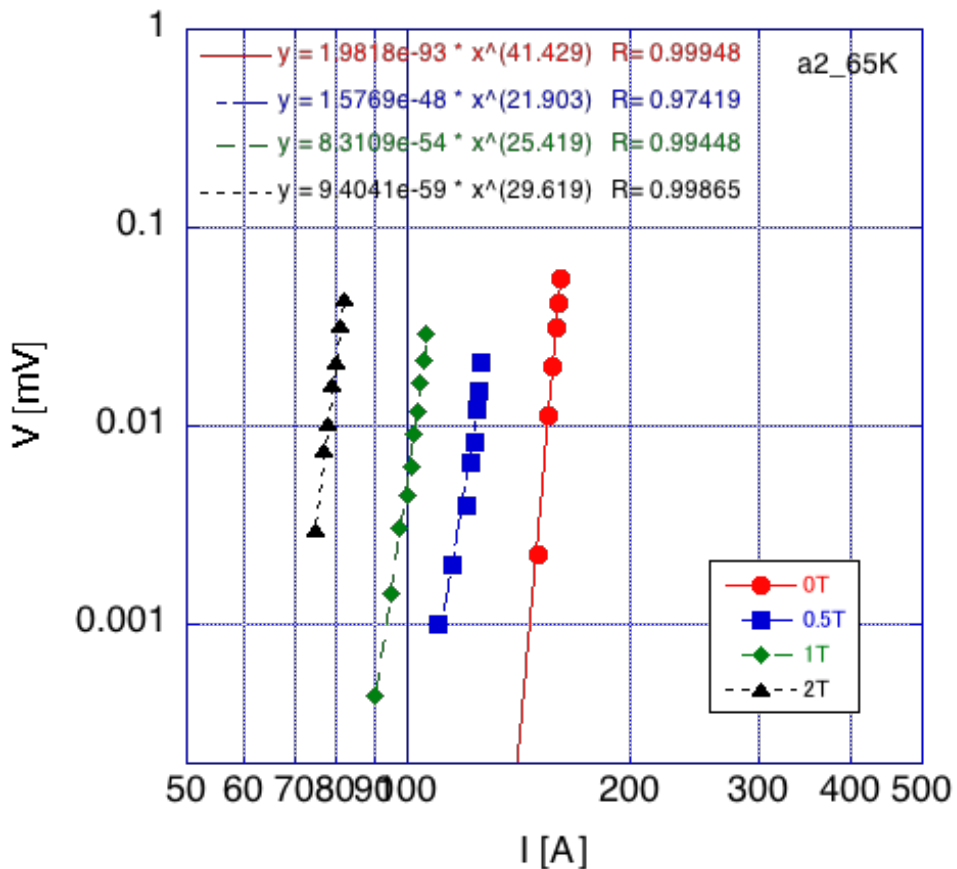
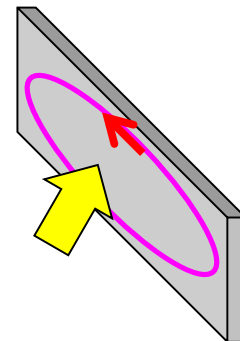
$T_1$  and  $B_2$  do not depend on  $B$  and increase with  $I$  for  $I < I_{th}(B)$ .

$T_1$  and  $B_2$  start to decrease for  $I > I_{th}(B)$ .  
 $I_{th}(B)$  is proportional to  $I_c(B)$ .



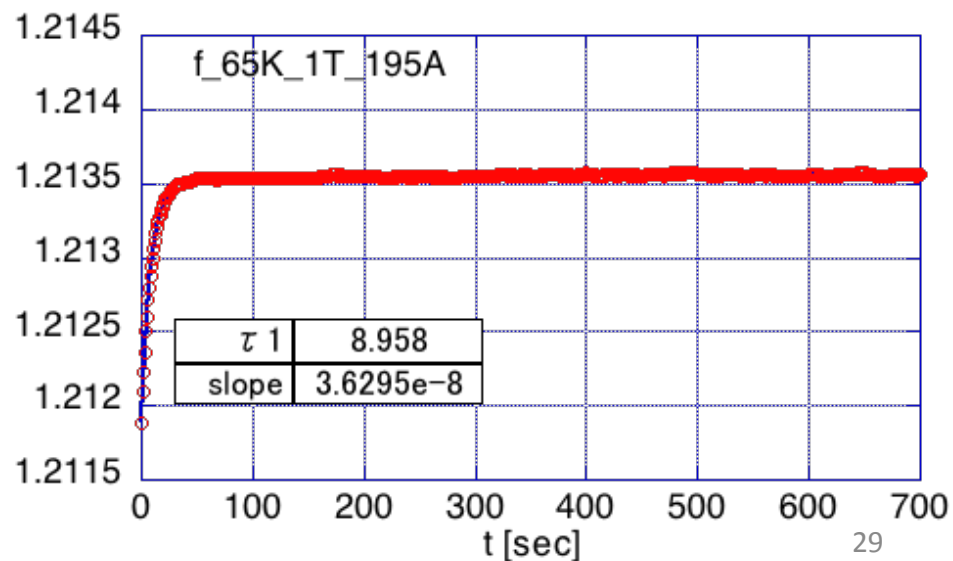
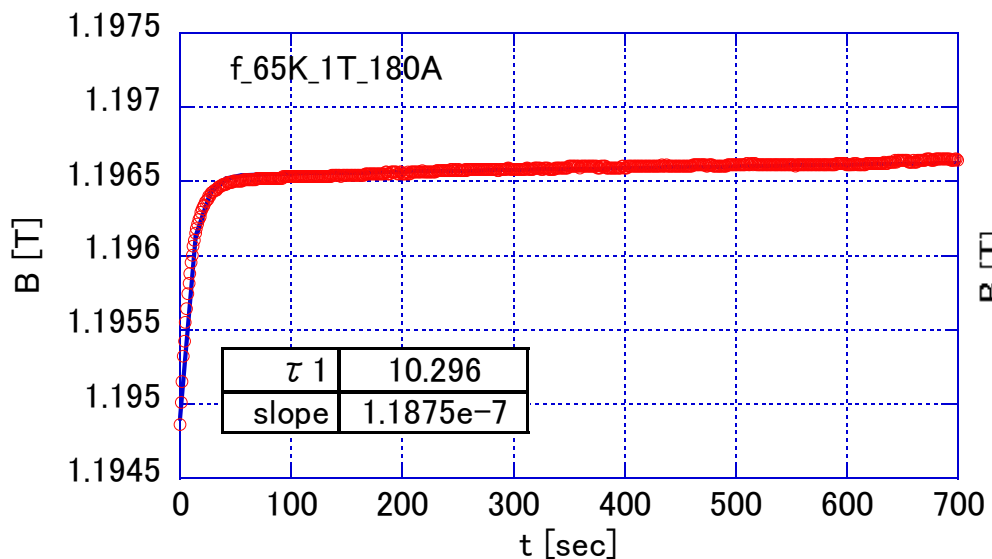
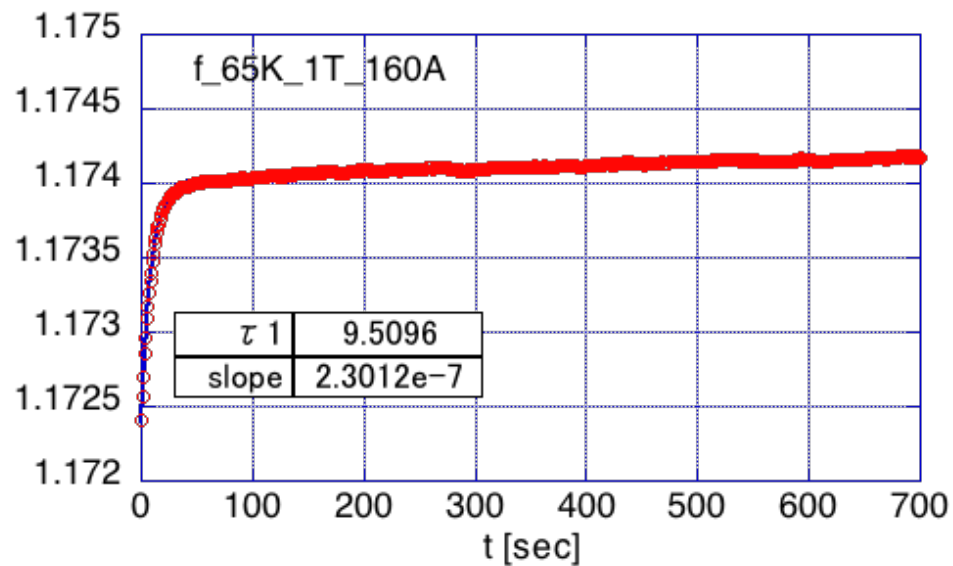
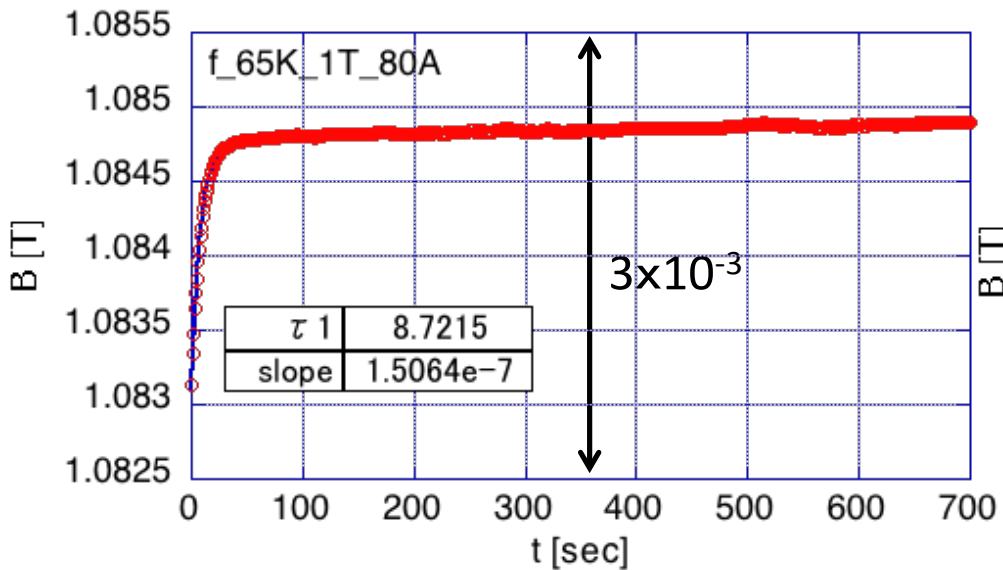
# I-V curve

$$B_{center} = B_0 + B_1 \left( 1 - e^{-\frac{t}{\tau_1}} \right) + B_2 t \quad \tau = \frac{L}{R} \quad R = \frac{V}{I} = \frac{V_c}{I_c} \left( \frac{I}{I_c} \right)^{n-1}$$

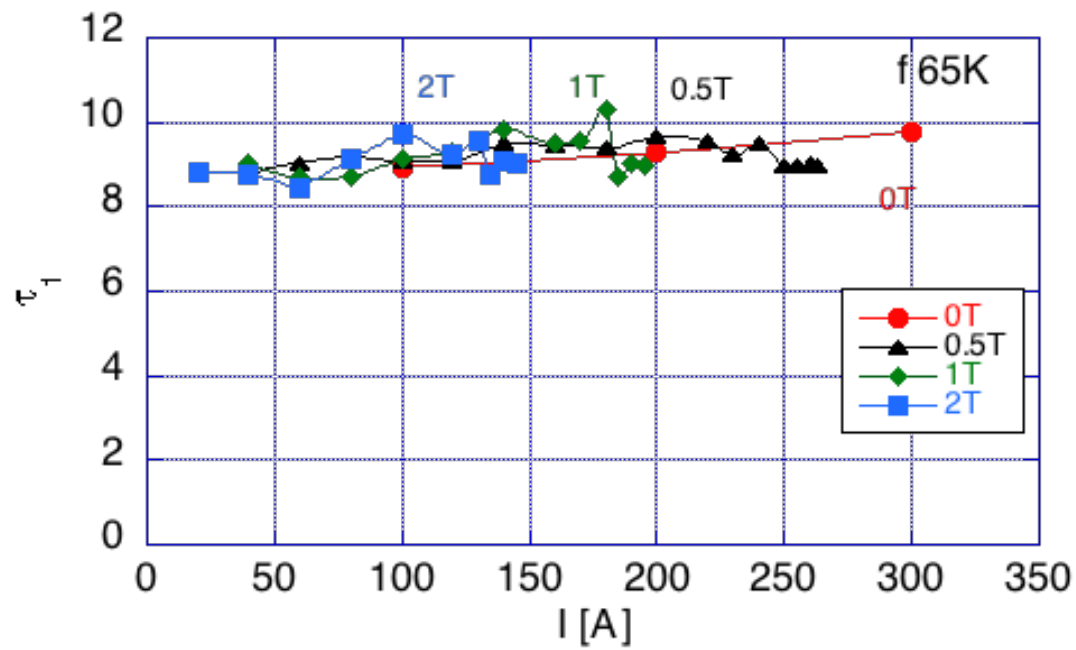


Equivalent resistance becomes larger with current and then decay time constant becomes small.

# 65K, 1T (Scribed EuBCO 30m, 19-turn, 6-layer)

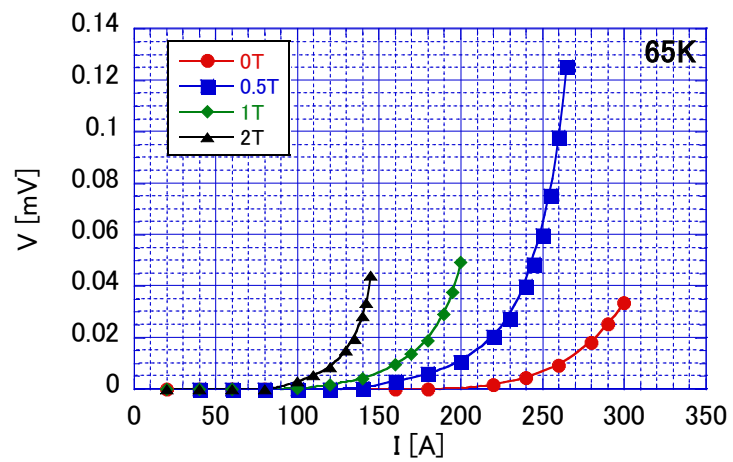
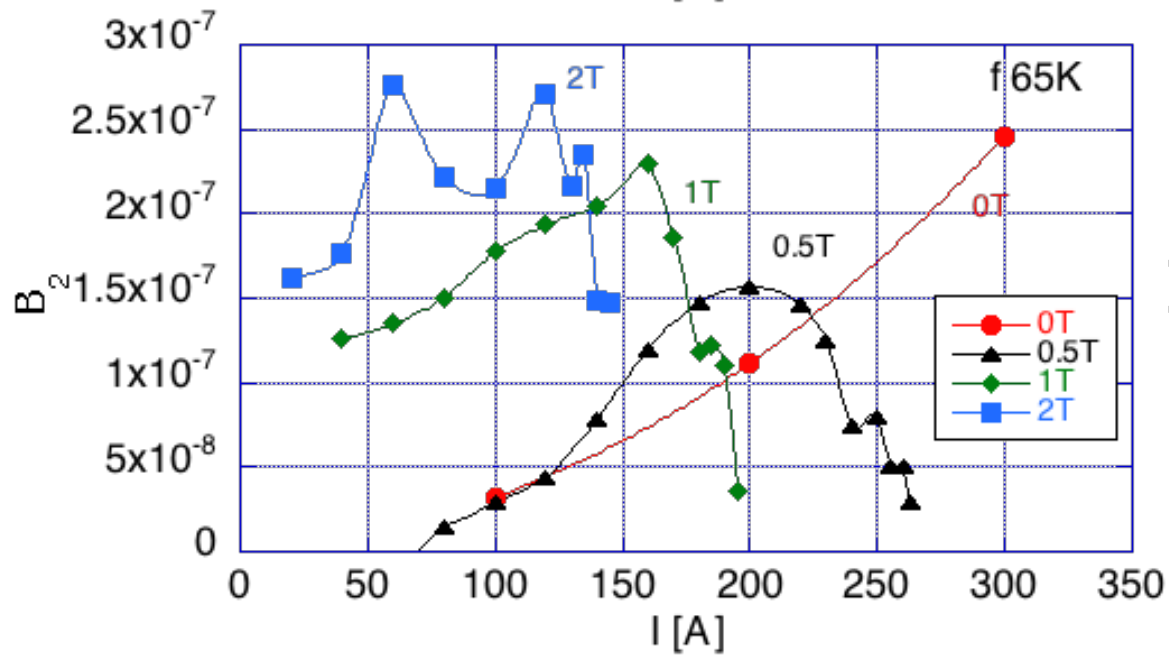


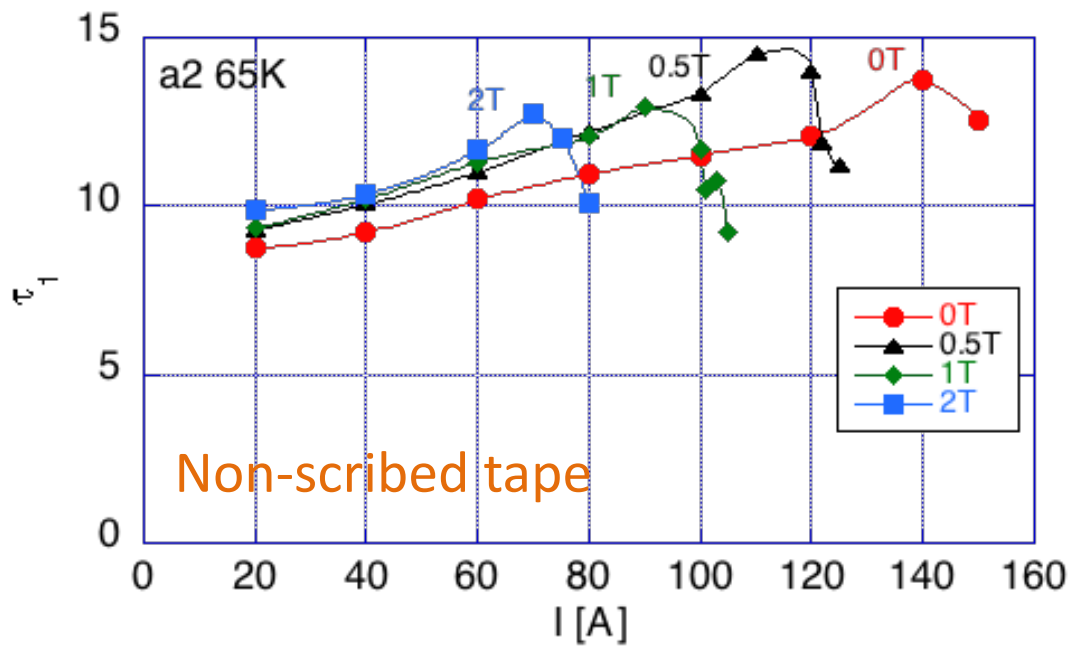




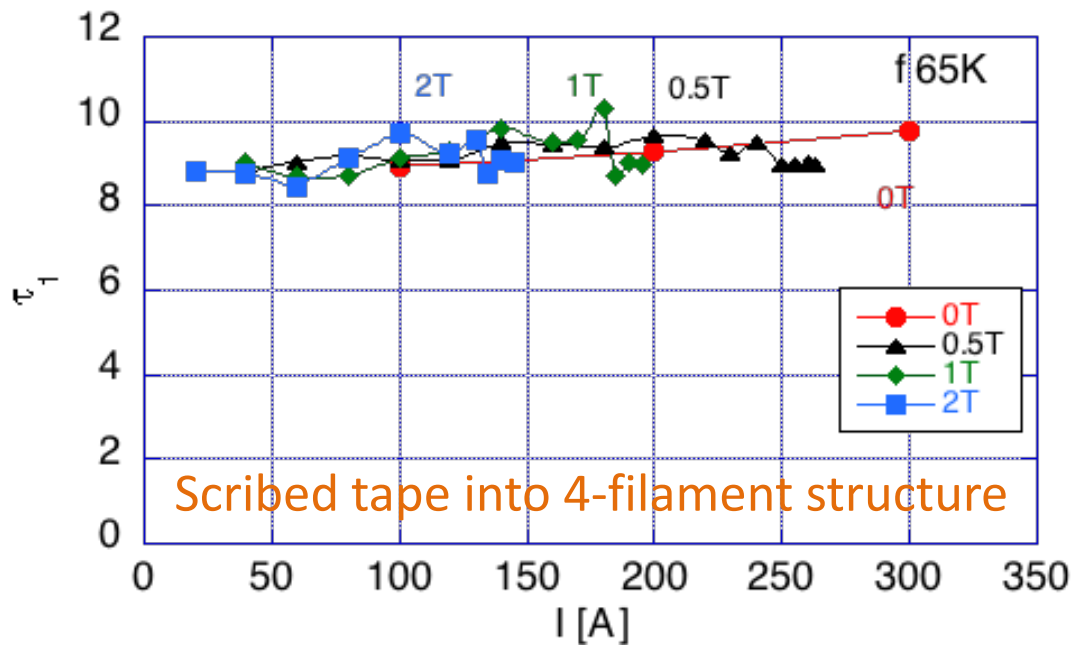
$T_1$  and do not depend on  $B$ .  
 $B_2$  increase with  $I$  and  $B$  for  $I < I_{th}(B)$ .

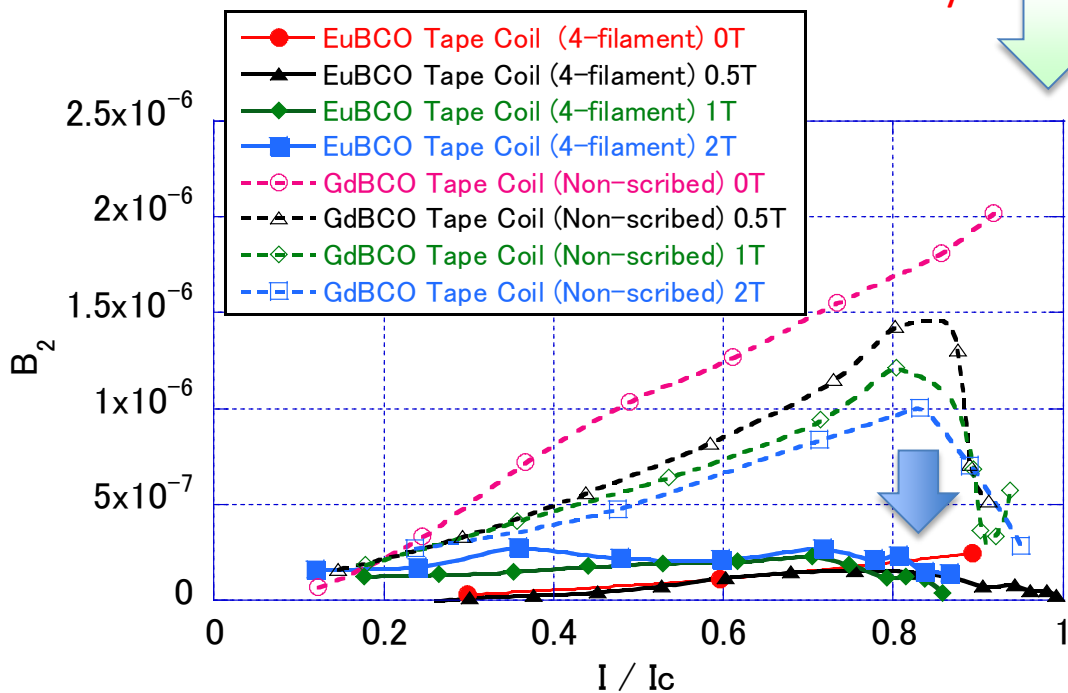
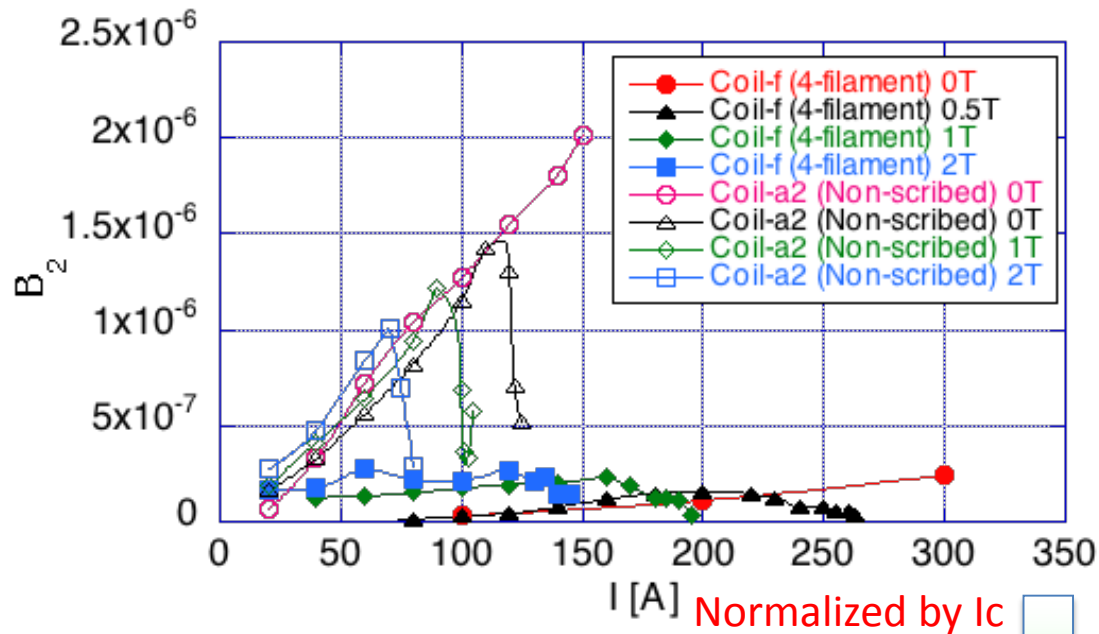
$T_1$  and  $B_2$  start to decrease for  $I > I_{th}(B)$ .  
 $I_{th}(B)$  is proportional to  $I_c(B)$ .



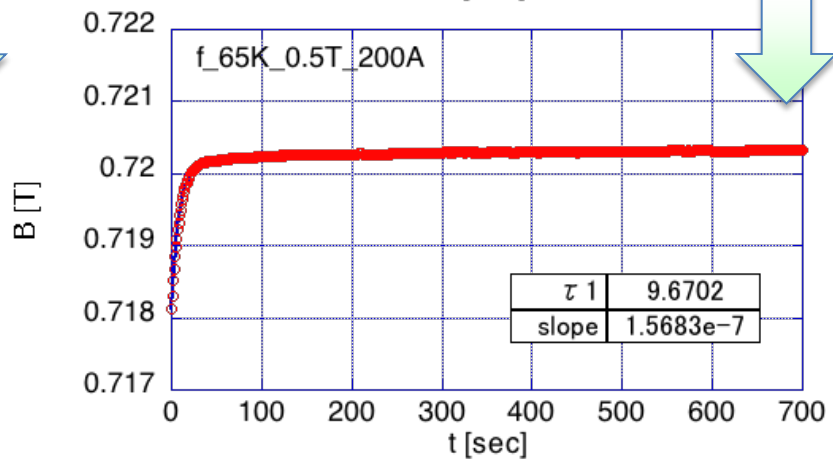
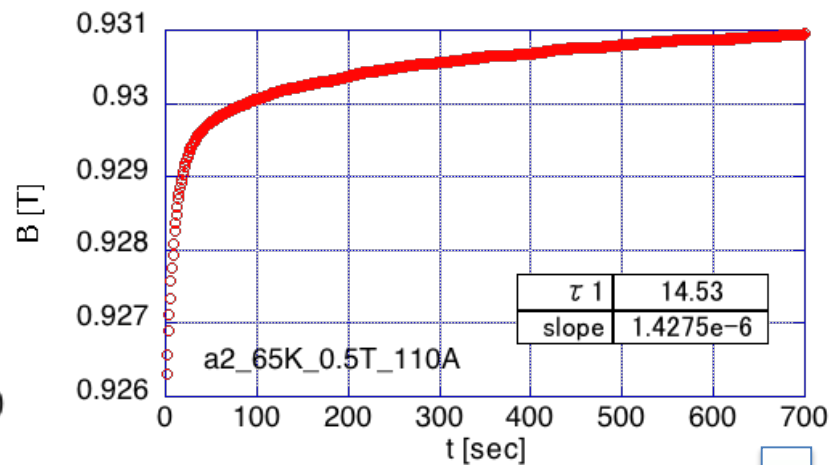


Comparison of  $\tau_1$   
↓  
Little difference





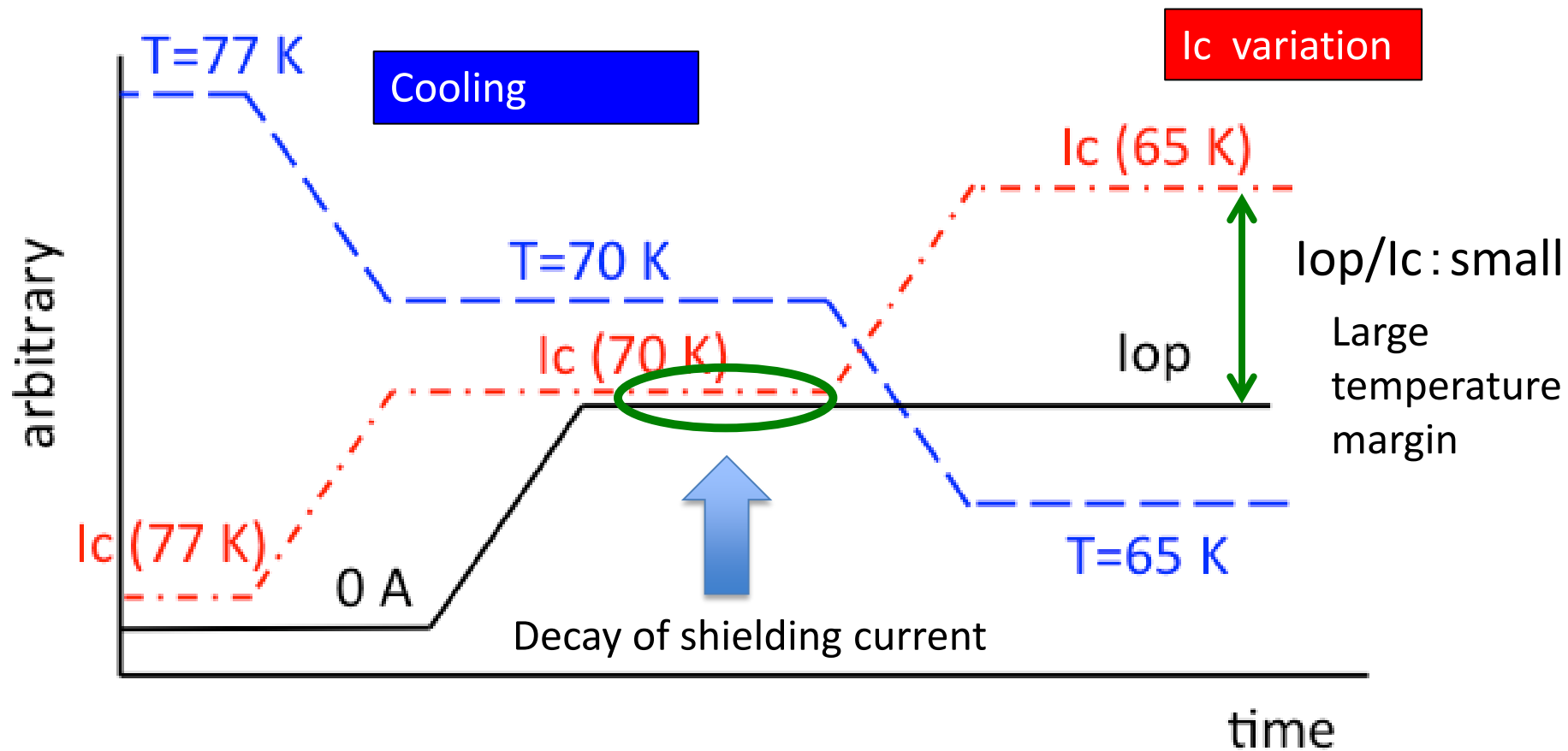
# Comparison



Gradient was much reduced by scribing.

Scribing brings about benefit for DC use.

# Operating pattern of MRI magnets to enhance the decay of shielding current



## 3. Summary

- (1) Magnetization and ac loss of REBCO SC tapes can be reduced by scribing & special winding.
- (2) It brings about benefits for both of ac and dc uses.
- (3) Improvement in superconducting property of REBCO tapes will realize operation in subcooled LN<sub>2</sub> at 65 to 77K.
- (4) It brings about very good cooling condition and high stability.