

Coated Conductors and HTS Magnets for Compact Fusion

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PPPL Team

T. Brown, J. Menard, M. Zarnstorff, P. Titus, C. Kessel (now with ORNL)

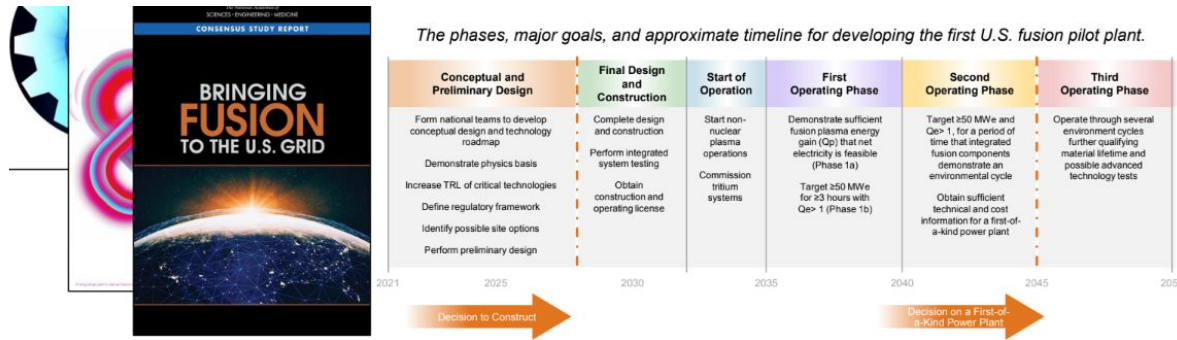
Collaboration Team

D. van der Laan, Advanced Conductor Technologies, D. Larbalestier & D. Davis, FSU-ASC-NHMFL

Coated Conductor Application Workshop at University of Houston April 4-6, 2023



- **Goal:** Make 50-100 MW net electricity, extended to long pulses
- **Road Map:** Design in 2020s, Construct in 2030s and Operate in 2030s-2040s
- **NAS Report:** Bring Fusion to U.S. Grid -> **30 GW of additional generation resources needed annually from '40 to '50 based on reference case analysis**

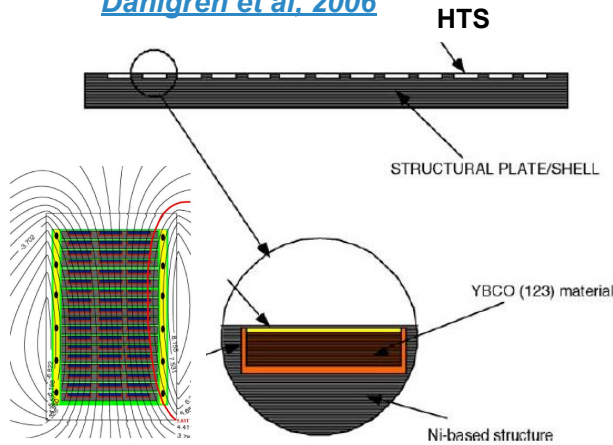


- Establish scientific and technical basis for a fusion pilot plant by 2040s
- Next step test facilities (tokamaks and compact stellarators)
 - Establish mission need to close integration & magnet R&D gap(s)



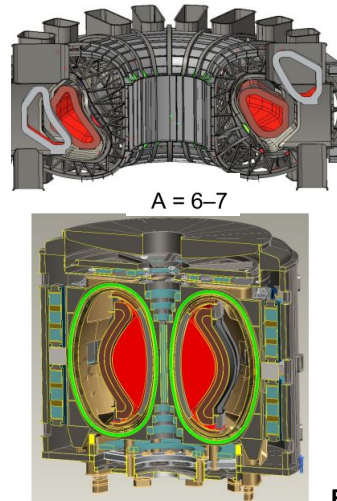
- Establish scientific and technical basis for a fusion pilot plant by 2040s
 - Integrate self-driven current with high core confinement, pressure, heat flux
- Steady-state to reduce disruptions, cyclic fatigue and need for pulsed power systems to enhance reliability and more compact to reduce size & cost

[Dahlgren et al., 2006](#)

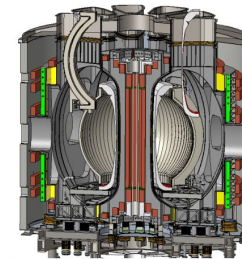


First HTS magnet system was proposed in **ARIES AT** studies (Fusion Eng. Des., 2006)

2014-2016



2016-2022

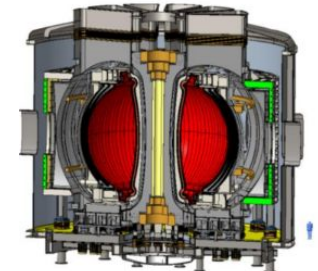


Sustained high power-density (SHPD) tokamak $A = 2-2.5$

$R=1-1.6m$, HTS TF SHPD and EXhaust and Confinement Integration Tokamak Experiment (EXCITE)

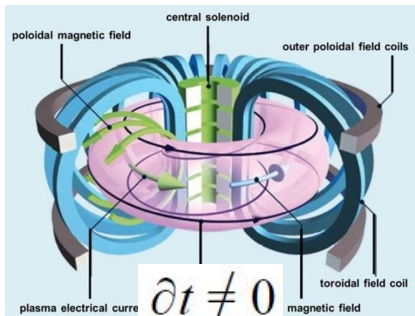
FNSF & FPP $A=2, R=3m$ HTS TF / $P_{net} = 50-100$ MWe

2021-2022

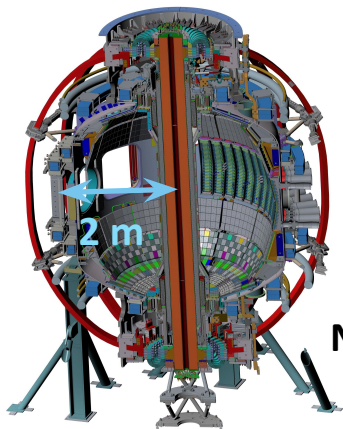


ST Advanced Reactor (STAR) Fusion Power Plant
 $A=2-2.2, R=4-4.5m$, HTS TF
 $P_{net} = 200-500MWe$

Two Different Magnetic Configurations

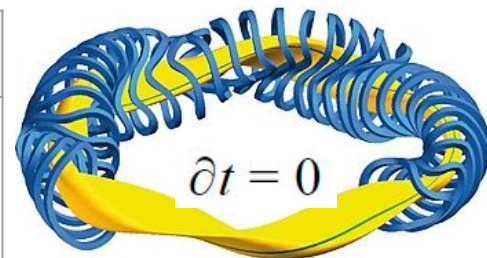


Plasma disruption drives engineering design!

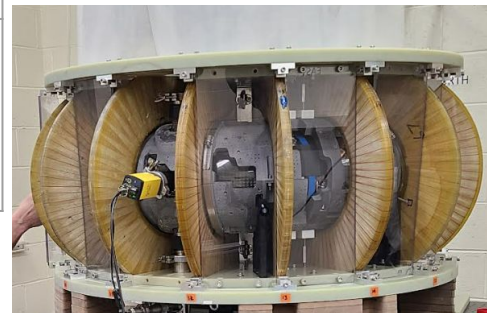


NSTX-U, PPPL

HTS Conductors	HTS Magnets
Ideal - isotropic, low cost, low loss, high J_c & high strength, rad. resistant, flexible design & easy integrate into coil design	Conduction or 10-20 K gas cooled, 16-20 T on coils, high winding pack J_e
YBCO - anisotropic, high cost, large losses, high strength, screening current; high risk CICC, no heat treatment	High field, compact steady state TF coils, >10 kA cables, quench and stress management
Coated Conductor application - High current cables Different specs for diff. coils	High current density, high field OH coils for plasma startups (>kA/s or 1-3 T/s ramp rate)

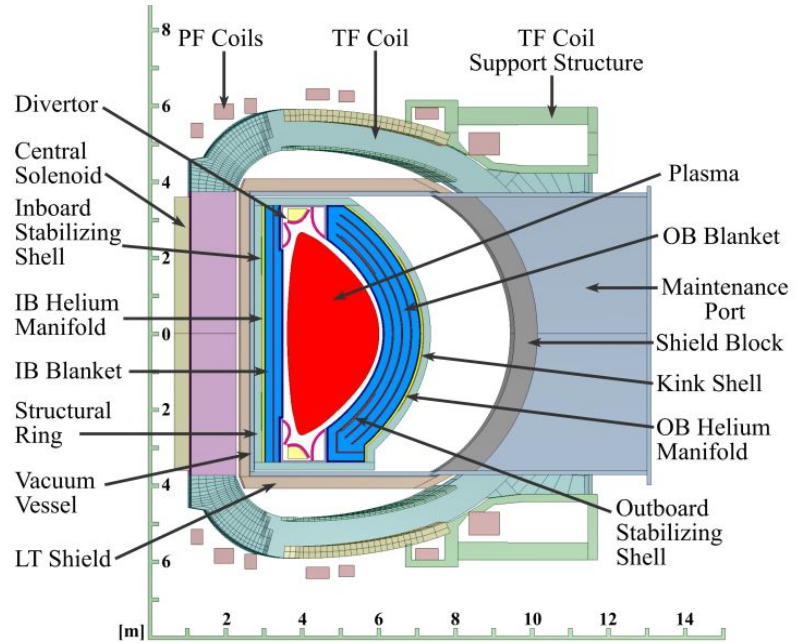


No disruptions & driven plasma currents & Typ. static B field



MUSE, PPPL

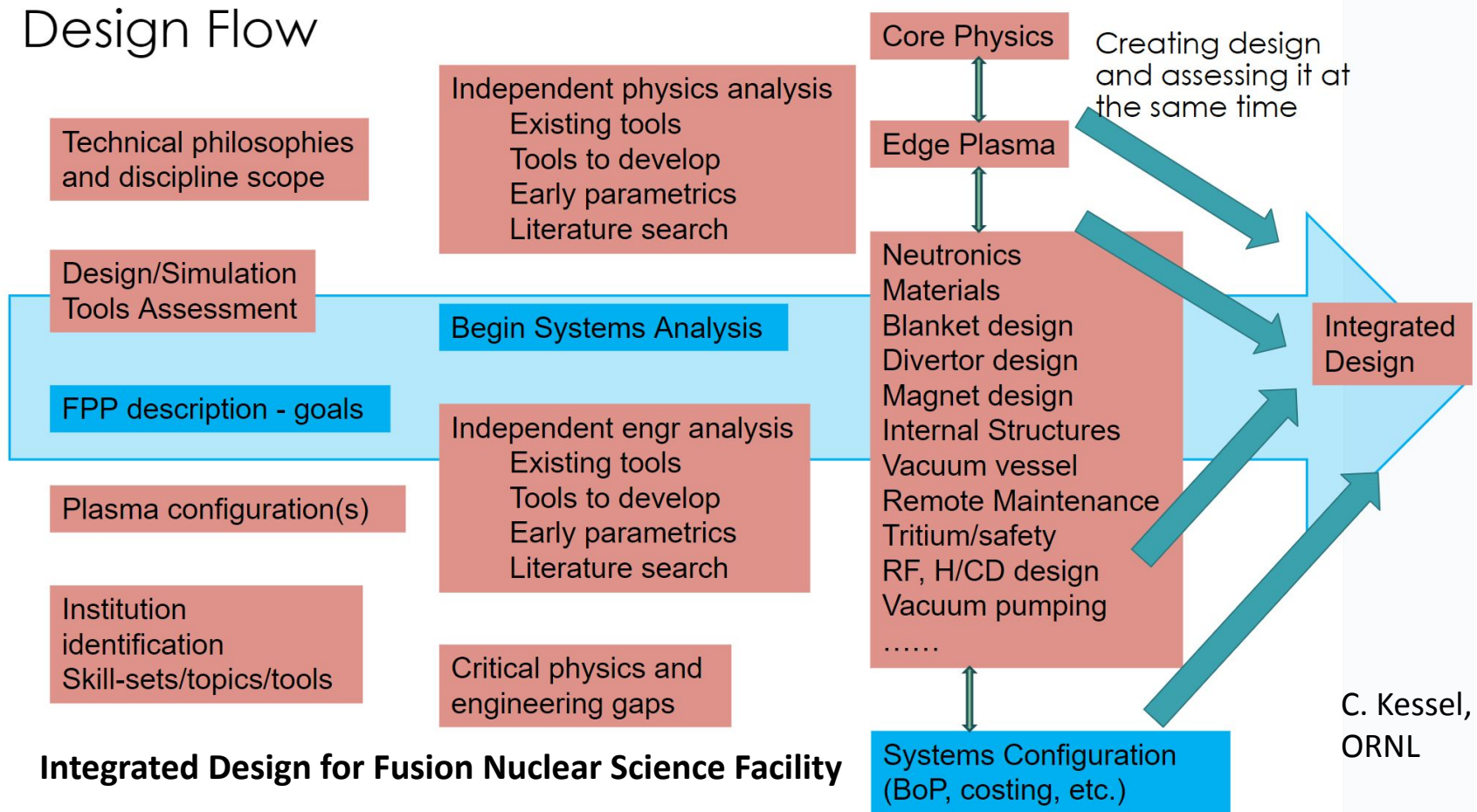
- Missions established in FNSF study for any intermediate device (ITER -> Power Plant)
 - Advance fusion neutron exposure of all core components toward the FPP level
 - Routinely operate plasma for very long durations (hours, days to weeks)
- Advance enabling technologies
 - Develop power plant relevant subsystems including high field magnet system



Total Stored energy 2x of ITER per TF coil

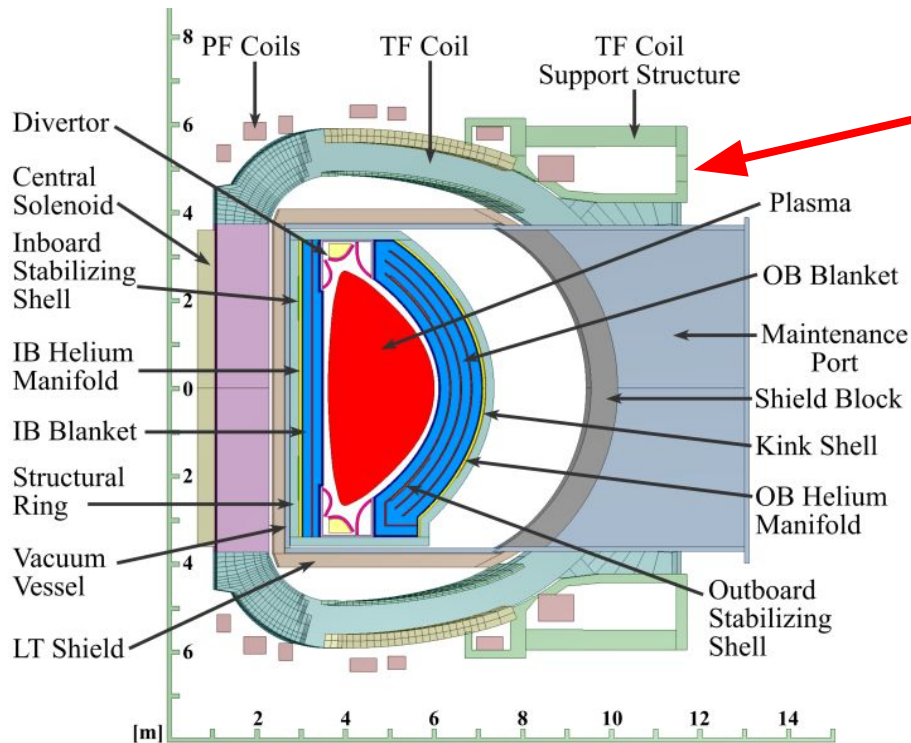
Total centering & vertical forces are 2~2.5x of ITER per TF IB leg

Design Flow

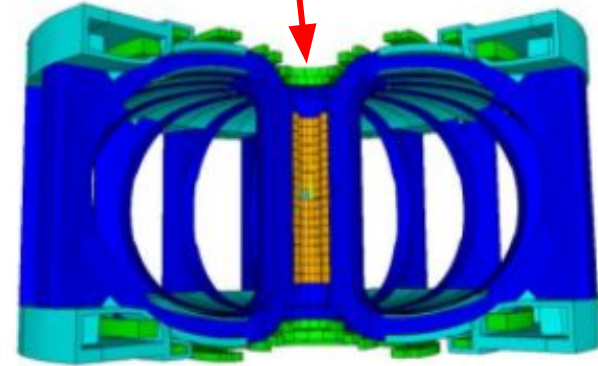


Integrated Design for Fusion Nuclear Science Facility

C. Kessel,
ORNL

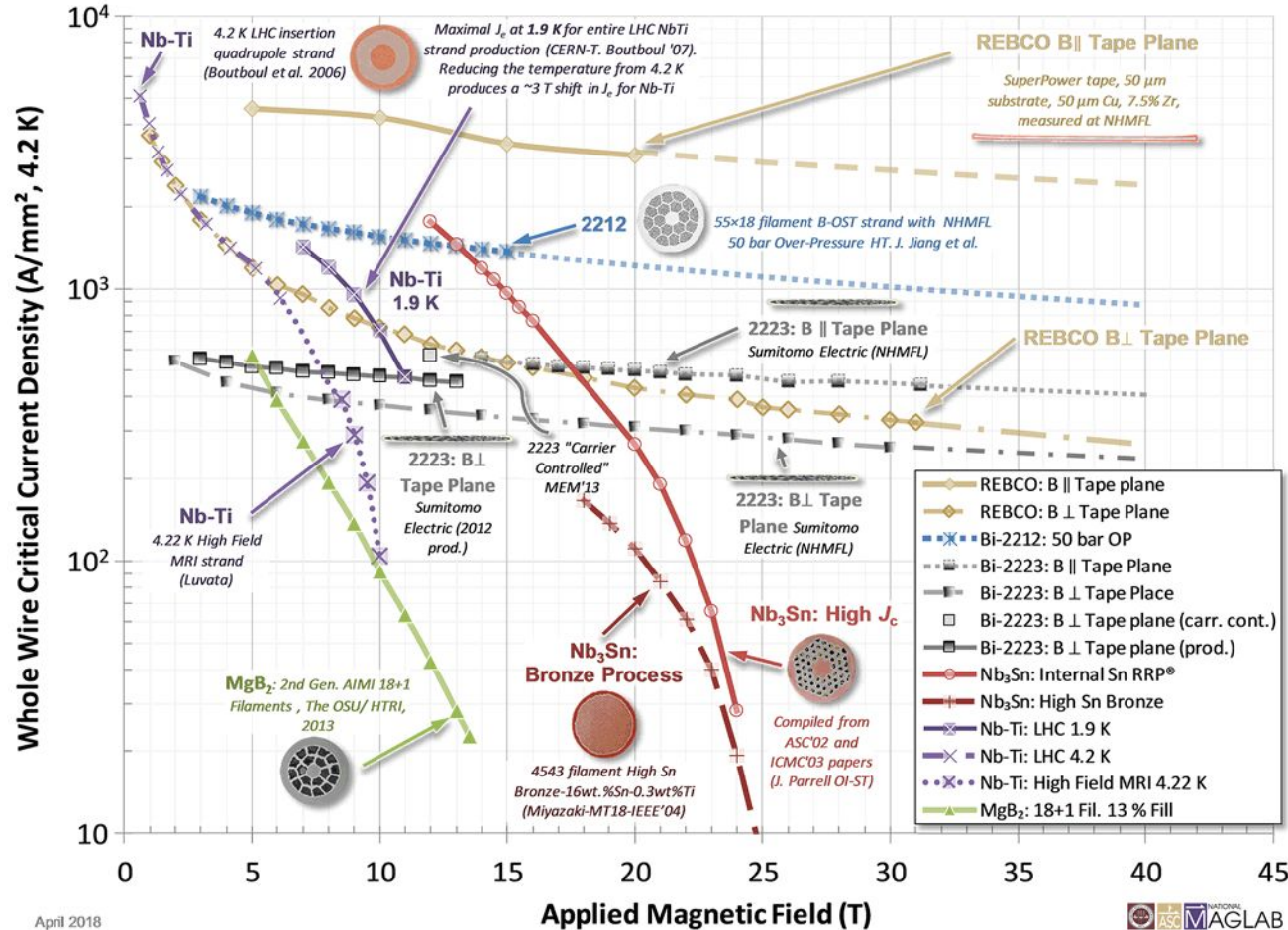


inter coil support structure to react OOP bending



Magnet integration for WP optimization

Zhai et al., Conceptual design of HTS magnets for FNSF, *Fusion Eng. Des.*, 168 (2021) 112611 ([here](#))

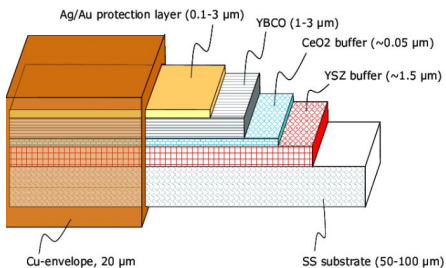


Coated conductor with attractive properties for Fusion Nuclear Science Facility magnet design and optimization!

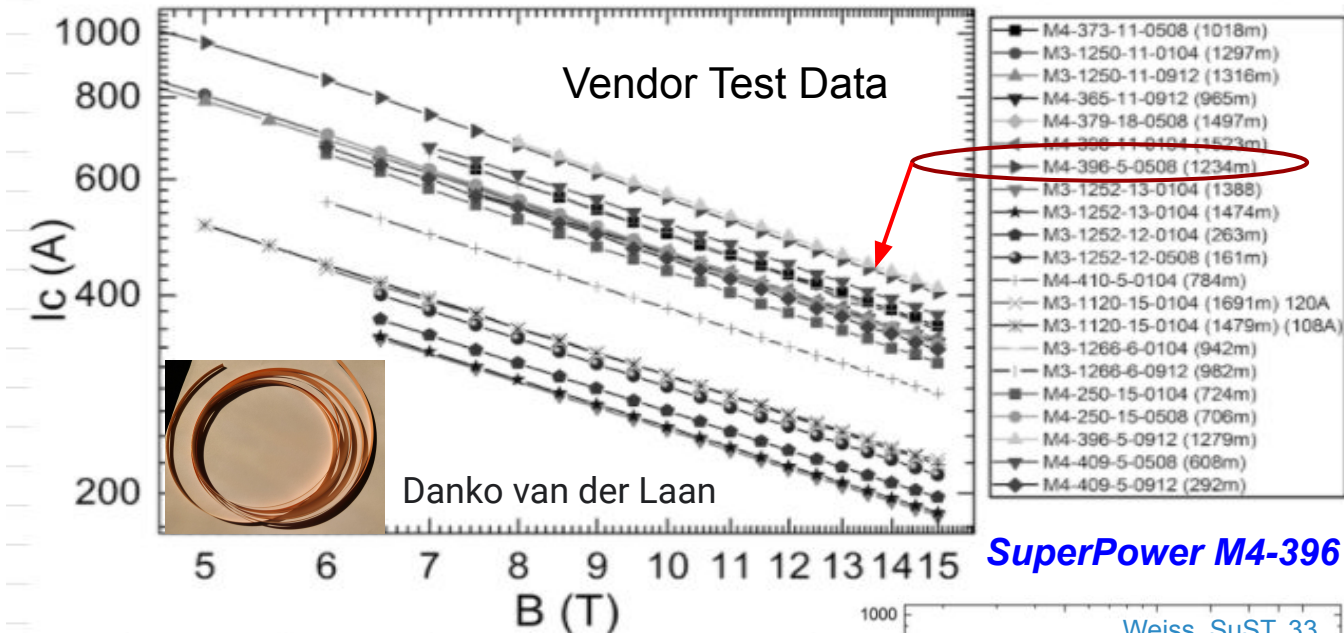


ReBCO tape (Superpower M4-396) performance - min
 I_c (6T) = 800 A

I_c (77K, s.f.) = 137.14 A
 I_c (4.2K, 20T) = 305 A

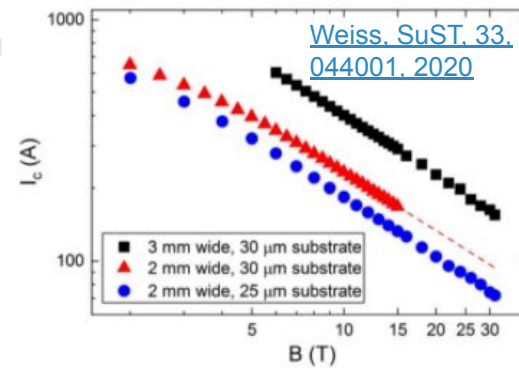


High current density cables consisting of multiple coated conductors are essential for engineering design of the next step configuration studies to allow space for interior plasma components.



SuperPower M4-396

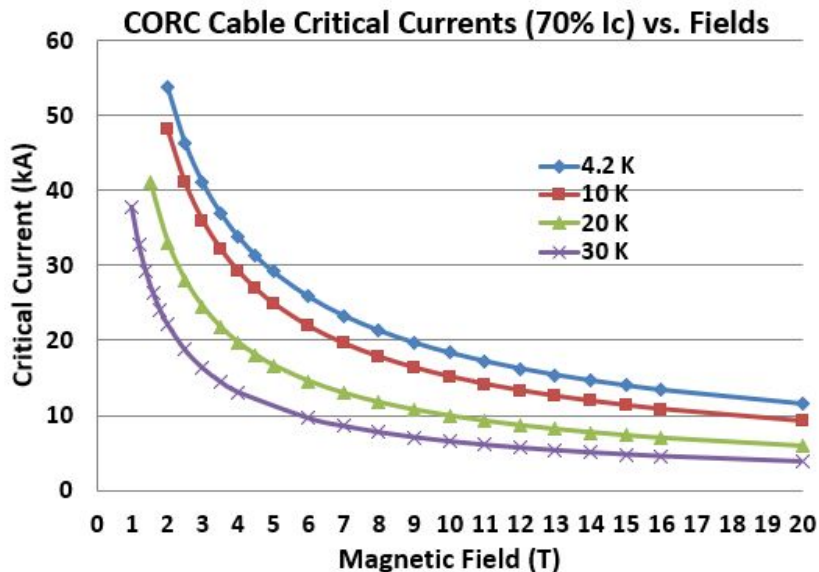
Tape used to construct **CORC®**





6-around-1 CORC® CICC with performance up to >60 kA at (4.2K, 20T)

CORC® cable	I_c (4.2 K) 70 %	Diameter (mm)
HF - 50 tape 50 micron	305 A/tape - 20 T	8
MF - 38 tapes	406 A/tape - 14 T	7.2
LF - 24 tapes	635 A/ tape - 8 T	6.375



ReBCO tape (superpower M4-396)
performance - min I_c (6T) = 800 A

I_c (77K, s.f.) = 137.14 A
 I_c (4.2K, 20T) = 305 A

CORC® cable performance

I_{op} (70% I_c) = 10.67 kA @ (4.2K, 20T)

CORC® current density > 150 A/mm²

FNSF TF WP, 4.2 K performance with force flow LHe cooling

IEEE-CSC & ESAS SUPERCONDUCTIVITY NEWS FORUM (global edition), Issue 53, July 2023.

Presentation given at Coated Conductors for Applications Workshop, Houston, TX, USA, April 2023.



	ITER	FNSF
Conductor	Nb ₃ Sn CICC	6-around-1 CICC
Major Radius (m)	6.2	4.8
Minor Radius (m)	2	1.2
Plasma Current (MA)	15	8.0
Plasma Center B (T)	5.3	9.3
TF Operating Current (kA)	68	64
TF Max B Field (T)	11.8	20.3
WP Je (A/mm ²)	17	39
TF A-Turns (MA)	9.1	14.0
# of Turns	134	218
# of TF Coils	18	16
Fusion Power (MW)	500	450

	ITER	FNSF
TF WP IB Radius (m)	2.78	2.2
TF WP outer radius (m)	10.75	10.5
Centering force per IB leg (MN/m)	54	142-153
VSF per half coil (MN)	205	488-530
VSF per inboard leg (MN)	103	244-265
Length of Coil Centerline (m)	34.1	33.1
Winding Pack volume (m ³)	12.4	11
Inductance per Coil (H)	1.0	2.5
Total Stored Energy (GJ)	41	80

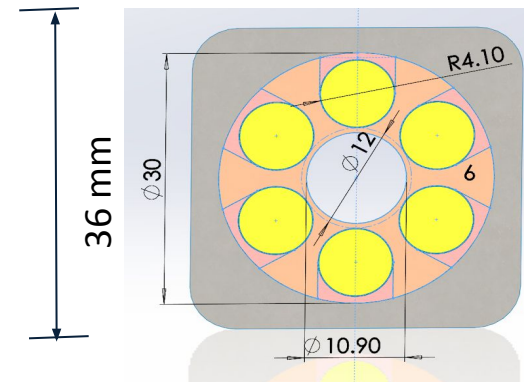
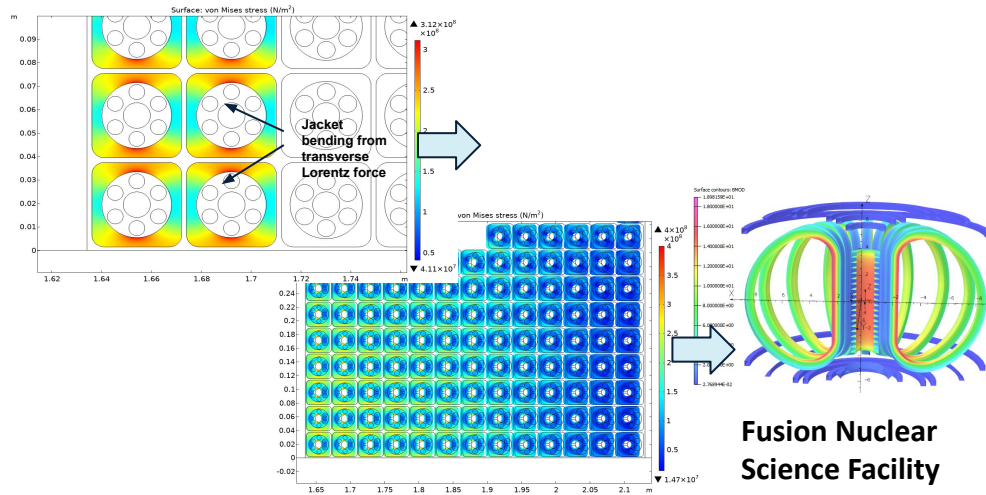
Total Stored energy 2x of ITER / TF coil
 Total centering & vertical forces are 2~2.5x of ITER per TF IB leg
 Inductance per TF coil drops to 2.5 H if 6-around-1 CICC is used

Parameter per TF Coil	ITER	FNSF	
		Single CORC	6-around-1
Stored Energy (GJ)	2.3	3.5	5.0
Inductance (H)	1.0	61.2	2.5

TF Coil Design - 6-around-1 CORC® CICC with conductor grading

- 36 mm square conductor (5 mm corner radius)
- Adjusted CORC cable dimension from high to low field regions

Jacketed conductor in TF winding pack



HF CICC	30 mm diam	50 tapes
MF CICC	28 mm diam	38 tapes
LF CICC	26 mm diam	24 tapes

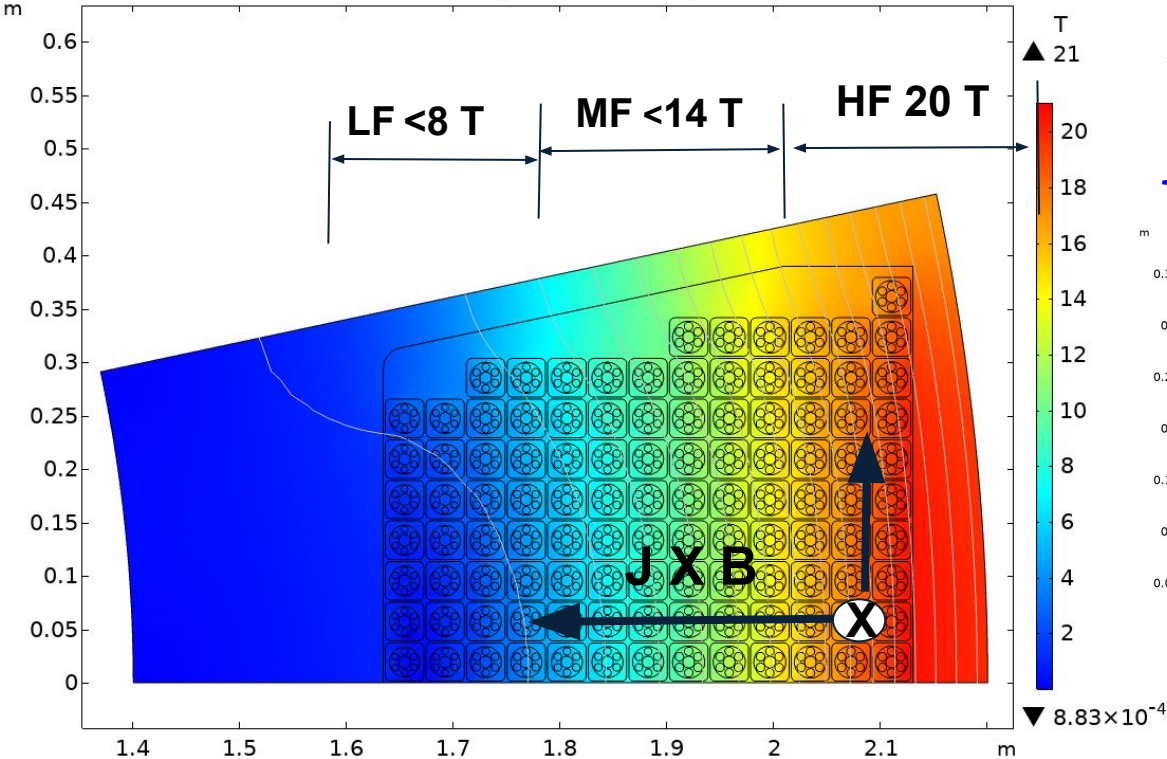
more consistent and systematic studies are needed to de-risk FPPs!

6-around-1 CORC® fits into TF winding pack with **218** turns with 2 mm turn insulation

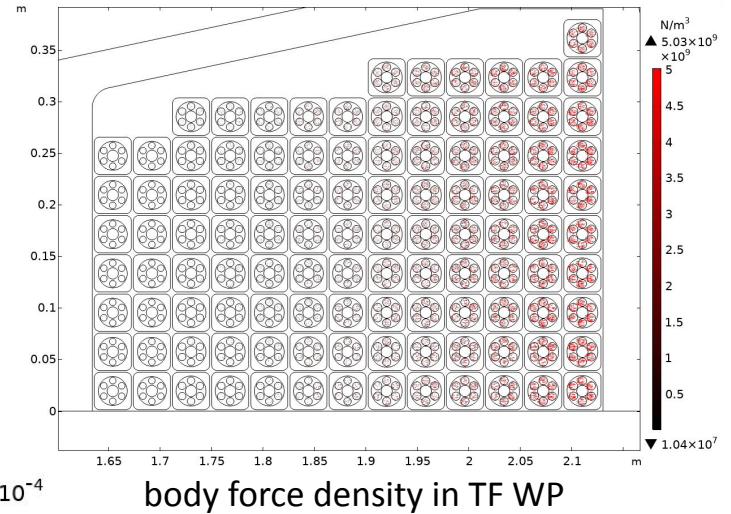


Conductor grading based on field distribution in inboard leg winding pack

Surface: Magnetic flux density norm (T)

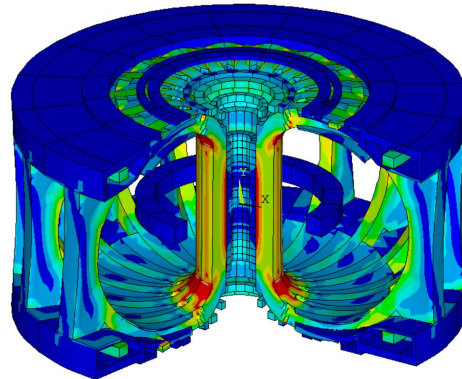
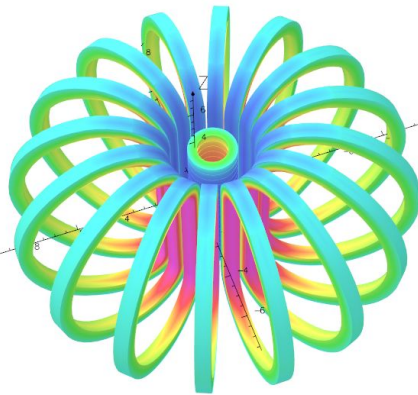


A thicker cable (w more tapes) in HF region; less tape thicker jacket in Low Field (LF) region

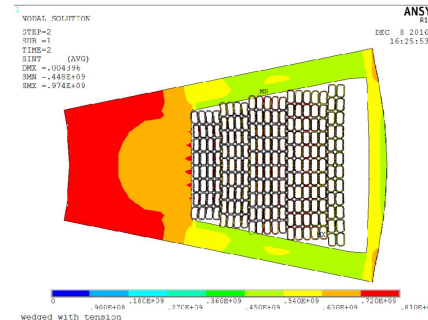


- Magnet system is an integral part of reactor design
 - Equilibrium scenarios / plasma operations
- In-board radial build & engineering design analysis
 - TF-CS structural interaction (bucked or wedged)

Surface contours: BMOD
 1.898159E+01
 1.800000E+01
 1.600000E+01
 1.400000E+01
 1.200000E+01
 1.000000E+01
 8.000000E+00
 6.000000E+00
 4.000000E+00
 2.000000E+00
 3.337700E-01



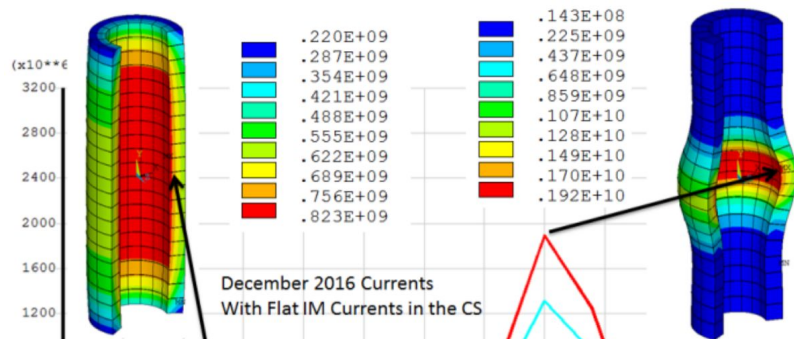
TF winding pack stress



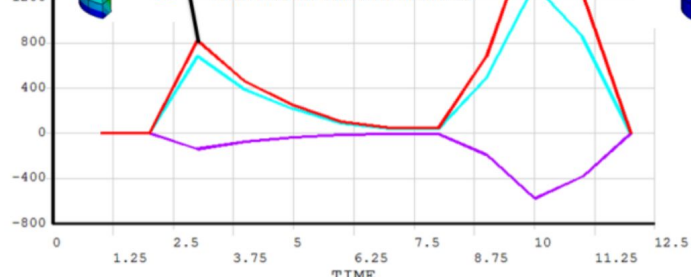


FNSF Central Solenoid Operations

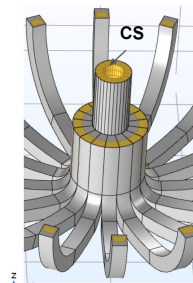
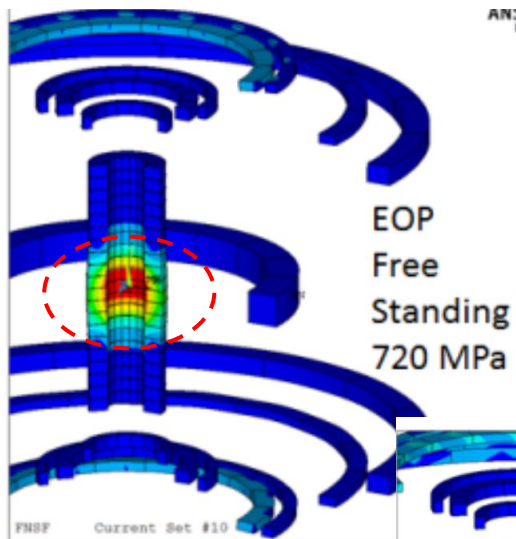
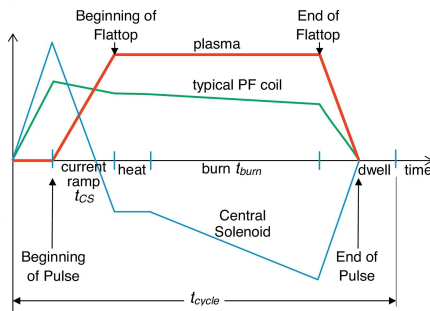
Stand alone solenoid



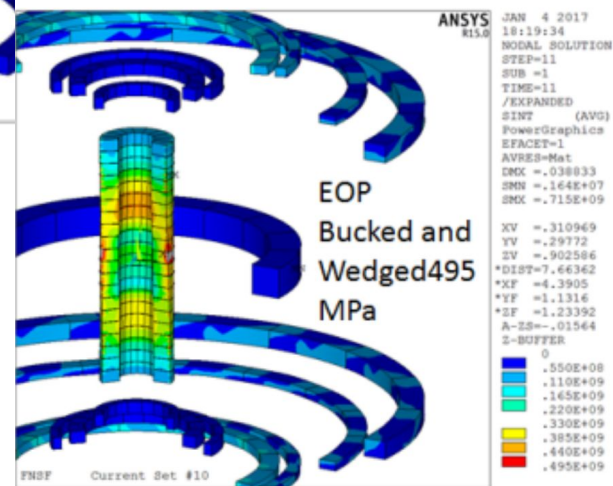
December 2016 Currents
With Flat IM Currents in the CS

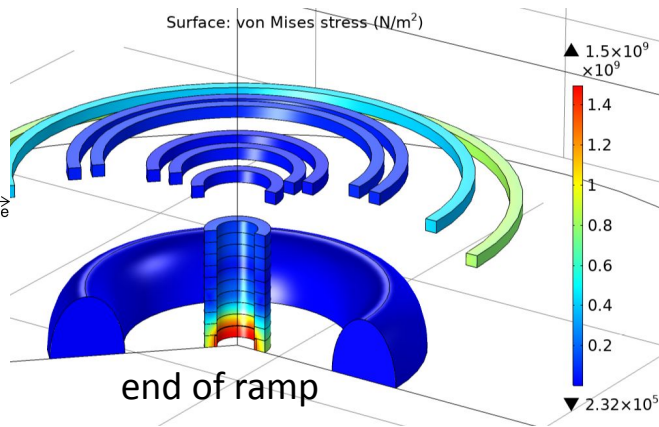
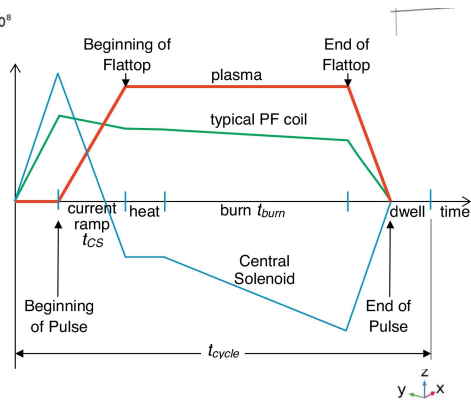
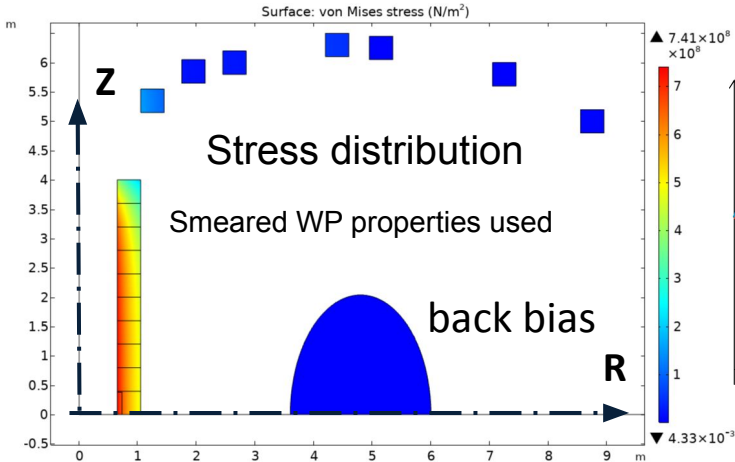
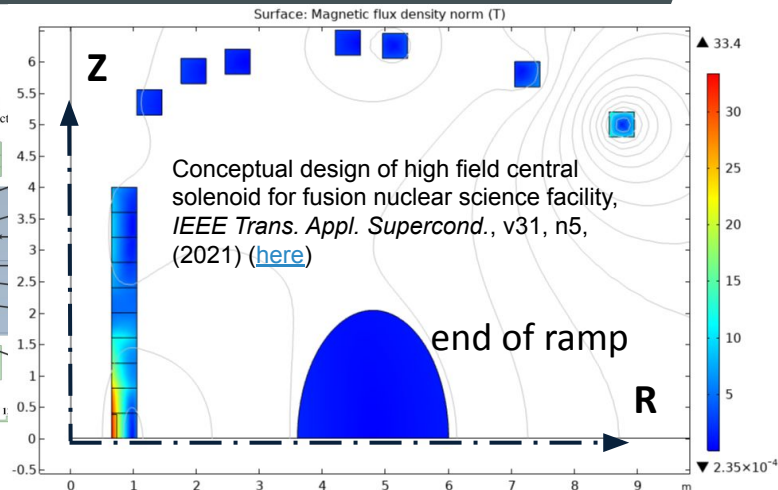
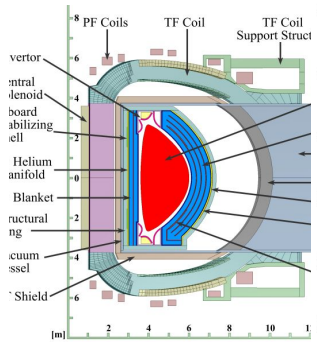
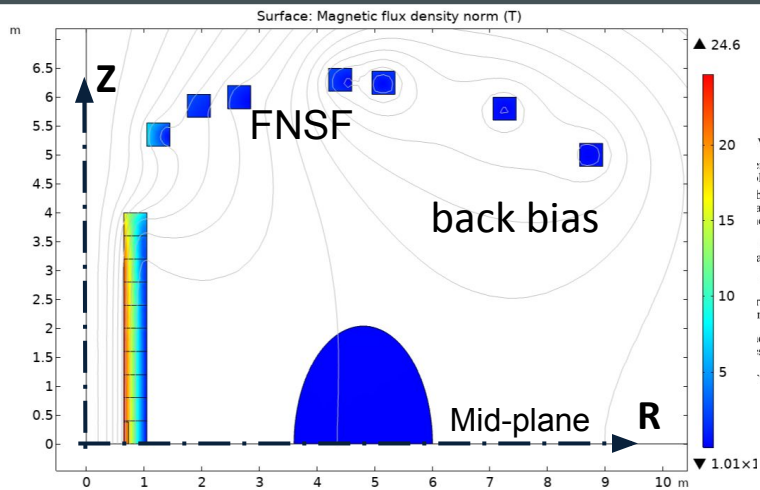


Kessel, Titus, PPPL



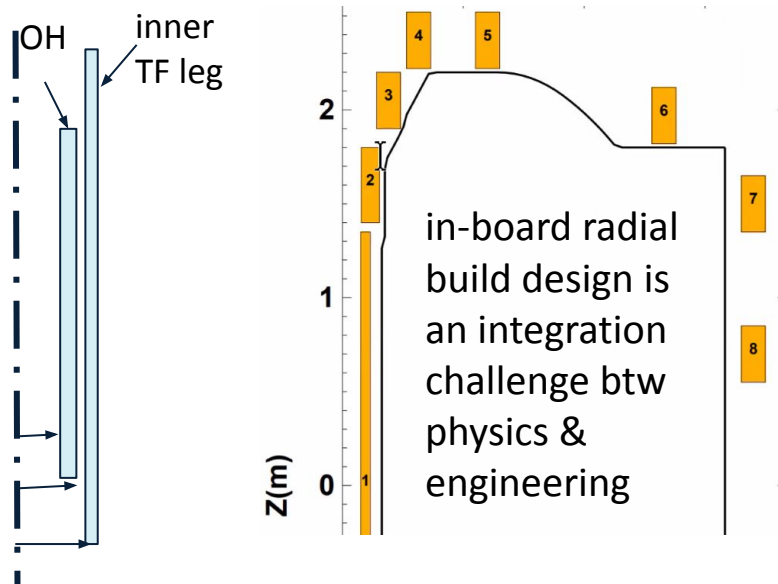
Bucked and Wedged







- Challenge in-board radial build



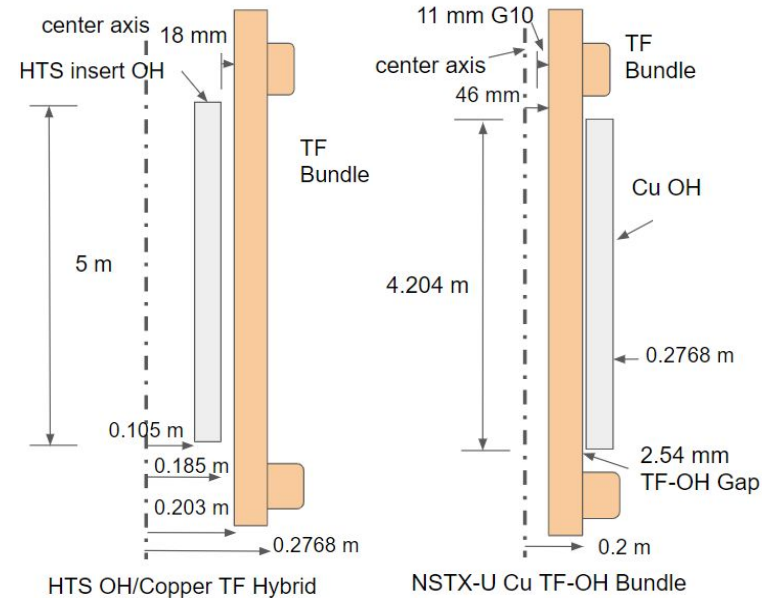
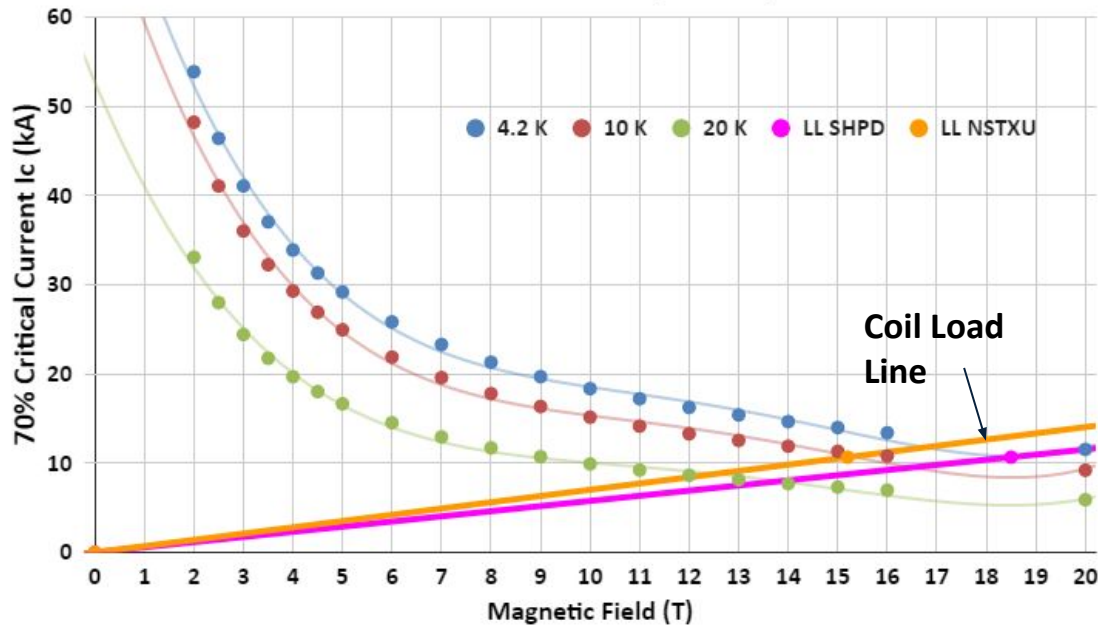
Gap (mm)	NSTX-U	SHPD
TF-CS	2.5	5-8

Parameters	SHPD
Major radius (m)	1.2
Minor radius (m)	0.6
Plasma current (MA)	4.5
Plasma center B (T)	5.5
TF current / coil (MA)	3.6
J_{wp} (A/mm ²)	80
TF coil B_{max} (T)	13
No. of TF coils	10



- HTS solenoids for plasma startups - fast ramping (kA/s), high field & high winding pack current density

CORC Cable Critical Current (70% I_c) vs. B Fields



Cabled coated conductor OH solenoid to decouple TF inner legs from OH solenoid NSTXU, SHPD/FPP

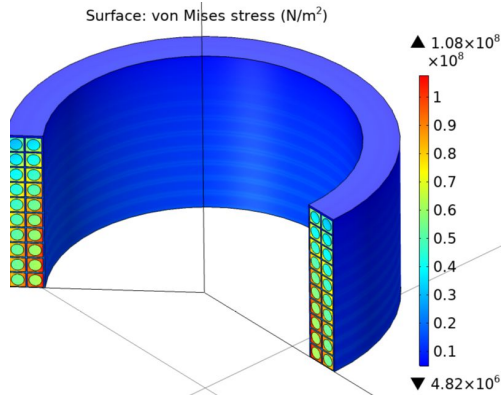


- Mature design concept and address critical issues by subscale coil testing
- Test coils in a unique large bore magnet at ASC-NHMFL to validate design

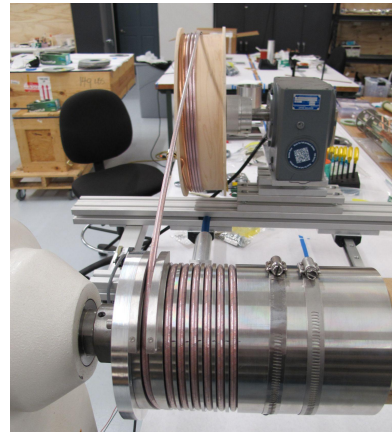
2 layer CORC® model coil

Winding at ACT (DOE SBIR)

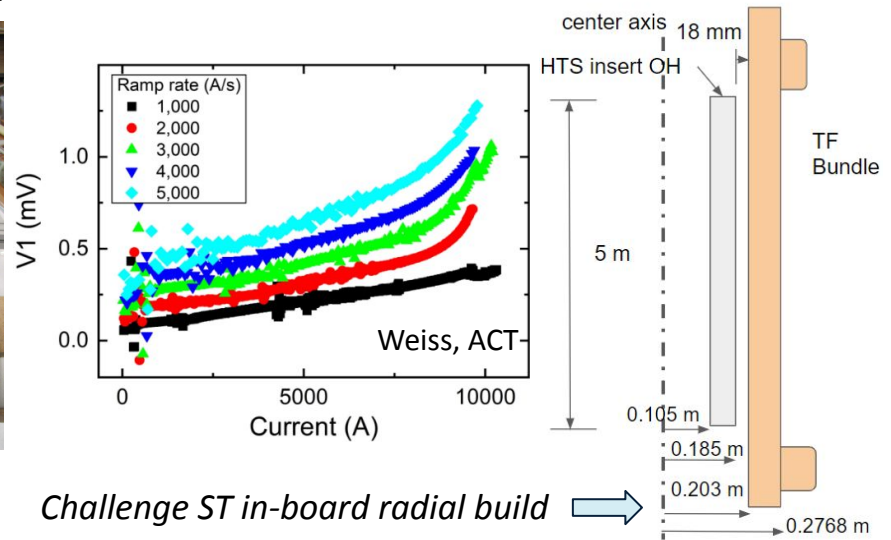
Stable behavior at 4 K self-field, kA/s ramp rate



Design & tested in ST relevant operating parameters



no impregnation



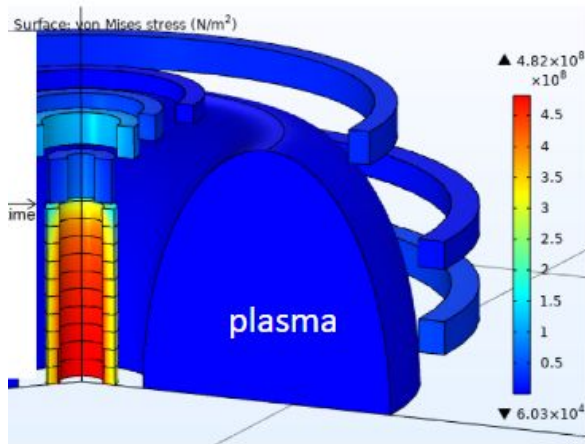
Challenge ST in-board radial build

No degradation after fast ramping on cabled model coil static test (PPPL-ACT-NHMFL)

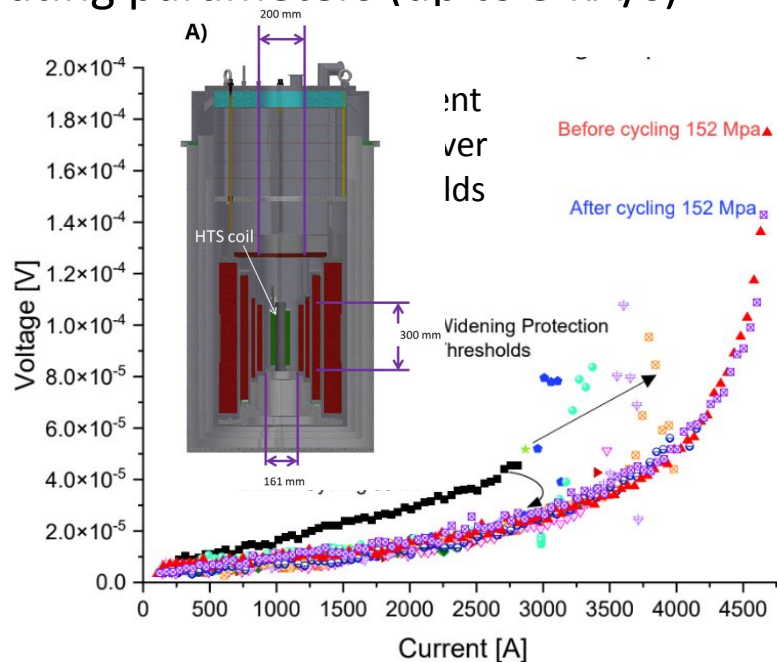


- No signs of degradation from the high field low-cycle fatigue of CORC insert solenoid tested with SHPD-FPP relevant operating parameters (up to 5 kA/s)

Parameters	SHPD
Major radius (m)	1.2
Minor radius (m)	0.6
Plasma current (MA)	4.5
Plasma center B (T)	5.5
TF current / coil (MA)	3.6
J_{wp} (A/mm ²)	80
TF coil B_{max} (T)	13
No. of TF coils	10



Tens of thousands of cyclic load fatigue test may be needed for pulsed machine



High field low-cycle fatigue testing of HTS insert solenoid with ST-FPP parameters, Davis [ASC'22](#)

Model coil has ~40% diameter of a central solenoid needed for SHPD - tested 1-3 T/s ramp rates, 12 T (higher than the ITER CS)



- Exploring reliable coated conductor & cable options is vital
- Leverage R&D capabilities in high field magnet and fusion to de-risk fusion pilot plants; differences in requirements
- Integration challenges vs. CS cyclic fatigue for pulsed machine operations to close R&D gaps
- Coated conductor for a broad range Fusion Pilot Plant configs.
 - R&D on design, testing, prototyping subscale solenoids
 - Test program to validate cables & CICC for FPP relevant coils